ASX Release

28 September 2026

Nova Scotia Exploration Acceleration Update

Highlights

- Exploration targets at Old Austen Mine Down-Plunge Prospect and along strike at the Mill Shaft West Prospect have been prioritised for assessment with intention of drill testing in Q4 June FY27 to Q1 September FY28.
- Two primary factors driving the prioritised assessment of down-plunge potential that might be able to be mined by underground mining extraction have been:
  - The Old Austen Mine Open Pit design depth has been constrained to minimise surface area disturbance and to achieve appropriate setbacks from waterways and this has left known mineralisation outside of the Open Pit Ore Reserve; and
  - Recent quality assurance work on the significant historic drilling program has enabled an updated geological model for down-plunge from the Old Austen Mine Open Pit Ore Reserve.
- Significant historical intercepts confirmed for inclusion in the updated geological model for the Old Austen Mine Down-Plunge Prospect (i.e. below the Open Pit Ore Reserve depth limitations) include:
  - **BD85-043: 1.84 m (true width) @ 163.7 g/t Au from 123.6 m;**
  - **BD86-003: 1.89 m (true width) @ 50.1 g/t Au from 141.7 m;**
  - **BD86-011: 3.20 m (true width) @ 10.3 g/t Au from 288.2 m;**
  - **BD86-015: 5.23 m (true width) @ 12.5 g/t Au from 206.3 m;**
  - **BD86-020: 3.70 m (true width) @ 66.1 g/t Au from 298.4 m; and**
  - **BD86-053C: 12.80 m (true width) @ 3.3 g/t Au from 524.2 m.**
- A drill program is now being planned to specifically test the Old Austen Mine Down-Plunge Prospect and along strike at the Mill Shaft West Prospect.
- High-resolution UAV magnetic survey across 22 km^2 around the Old Austen Mine will be completed in early October with a comprehensive structural review scheduled to follow in H2 June FY27 to refine drill targets.

St Barbara Limited ("**St Barbara**" or the "**Company**") (ASX: SBM) is pleased to provide this update on the acceleration of exploration across its Nova Scotia exploration portfolio, with a priority assessment of down-plunge underground mining potential below Old Austen Mine Open Pit Ore Reserve depth limitations and along strike at Mill Shaft West.

St Barbara Limited Managing Director and CEO Andrew Strelein said:

"*The updated Mineral Resource Estimate announced in July 2026 marked a major step forward for the 15-Mile Processing Hub Project.*"

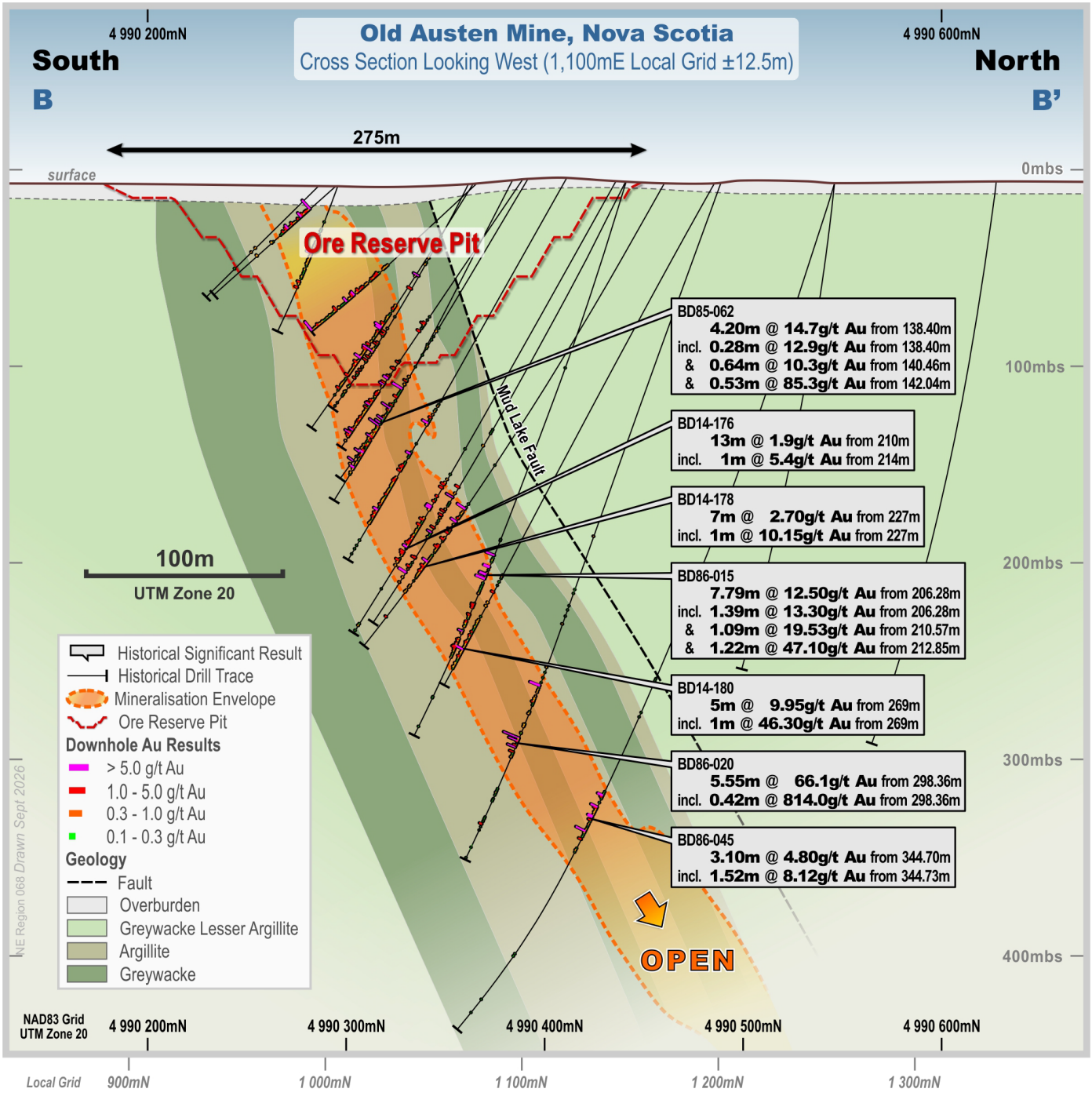
"We continue to accelerate our exploration across our extensive pipeline of targets and in particular wish to note that we are assessing, as a priority, the underground potential down-plunge and along strike from the Old Austen Mine Open Pit Ore Reserve limitations. We think this is an attractive opportunity for further resource growth."

"We are advancing plans for a major drill program to test these targets in the Nova Scotia spring and summer of 2027. Initial work will include a high-resolution UAV magnetic survey and comprehensive structural analysis to refine drill targets."

Figure 1 below is a cross section looking west at 1,100 m E showing drilling and significant intercepts down-plunge from the Old Austen Mine Open Pit Ore Reserve. The location of the Open Pit Ore Reserve shell and the +0.3 g/t Au mineralisation envelope are shown with mineralisation open down-plunge from current drilling. Mineralisation dips -70° to the north, mainly hosted by the argillite and greywacke located in the southern over-turned limb of the anticline and partially bound to the north by the late-stage Mud Lake Fault.

Drilling on cross section 1,100 m E extends up to approximately 335 m below surface and approximately 250 m down dip (or 225 m vertically) below the limits of the Open Pit Ore Reserve shell (between 110 mbs and 325 mbs). The location of the cross section is shown in the Figure 4 Long Section (page 5), which highlights high-grade 'gram-metre' gold contours of ≥30 gram-metres located below the Open Pit Ore Reserve shell. These contours, which include the BD86-202 intercept of 5.55 m @ 66.1 g/t Au from 298.36 m, define a semi-continuous domain with an interpreted down-plunge extent of approximately 450 m. The domain plunges approximately -40° to the east within the plane of section (looking north) and remains open down plunge.

Figure 1. Old Austen Mine Down-Plunge Prospect Cross Section (equivalent to 1,100 m E Mine Grid), Nova Scotia, Canada



Significant drill intercepts (quoted in down-hole lengths in metres) located on Cross Section 1,100 m E include:

- **BD86-015: 7.79 m @ 12.5 g/t Au from 206.28 m including 1.39 m @ 13.3 g/t Au from 206.28 m, 1.09 m @ 19.53 g/t Au from 210.57 m and 1.22 m @ 47.1 g/t Au from 212.85 m;**
- **BD86-020: 5.55 m @ 66.1 g/t Au from 298.36 m including 0.42 m @ 814.0 g/t Au from 298.36 m; and**
- **BD85-062: 4.20 m @ 14.7 g/t Au from 138.40 m including 0.28 m @ 12.9 g/t Au from 138.4 m, 0.64 m @ 10.3 g/t Au from 140.46 m and 0.53 m @ 85.3 g/t Au from 142.04 m.**

True widths for the same intercepts are presented in Table 2.

Old Austen Down-Plunge Prospect and Mill Shaft West Prospect

Old Austen Down-Plunge Prospect

Figure 2 below shows the local geology in relation to the location of the Old Austen Mine Open Pit Ore Reserve shell perimeter and of the +0.3 g/t Au mineralisation envelope. The Old Austen Mine Down-Plunge Prospect mineralisation is hosted in the southern limb of a north dipping overturned east - southeast striking isoclinal fold. The ore body strikes approximately 105°-285° and dips at -70° towards 15°. The mineralisation is hosted within the Moose River Formation located at the base of the Goldenville Group which consists of highly interbedded greywacke and argillite beds. The east - west striking anticline is locally offset by late-stage northwest – southeast striking late faults (i.e. the Cameron Flowage and Mud Lake Faults).

Figure 2. Old Austen Mine Down-Plunge and Mill Shaft West Geology, Nova Scotia, Canada

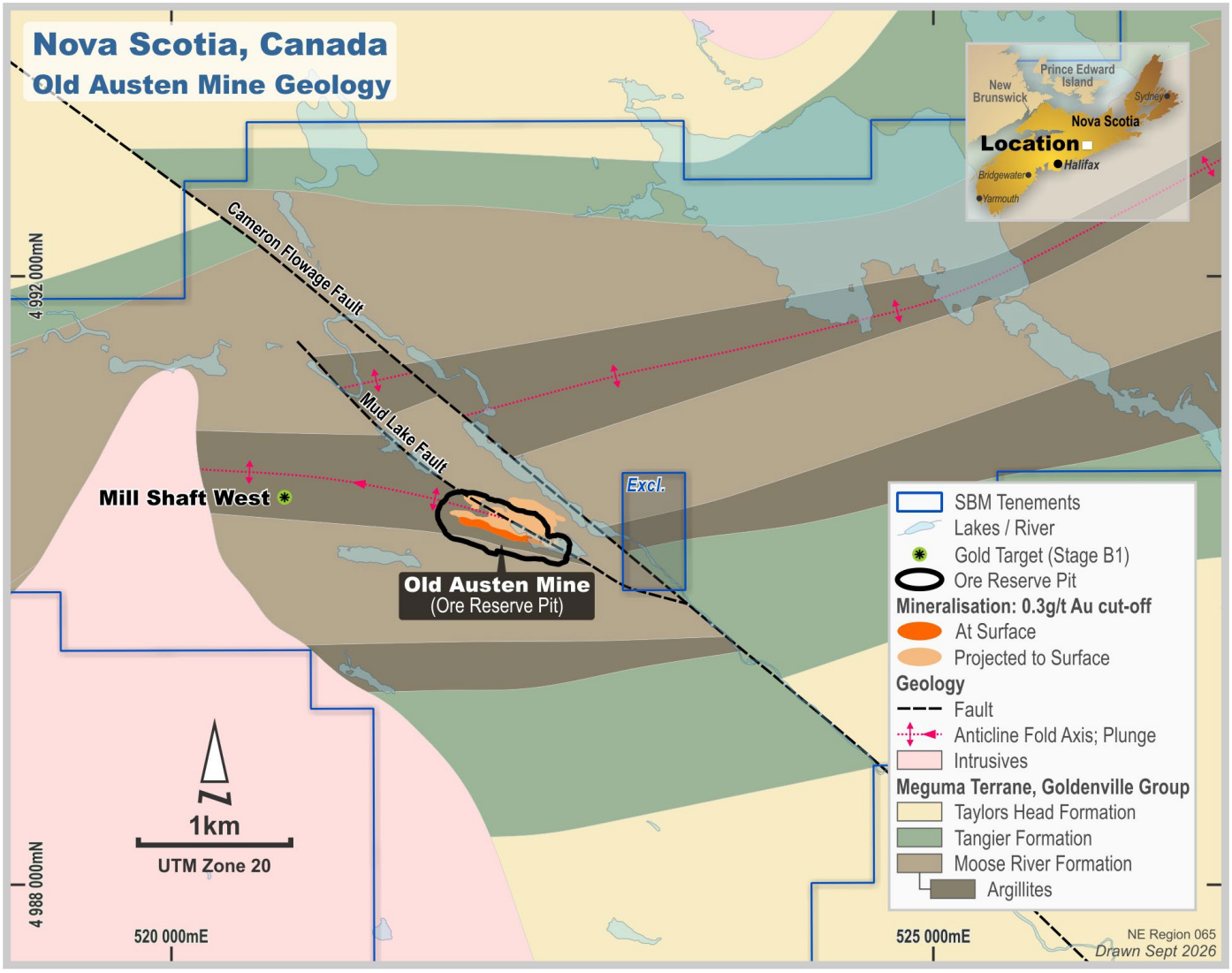


Figure 3 below zooms in on the local geology surrounding the Old Austen Mine Open Pit Ore Reserve shell and of the +0.3 g/t Au mineralisation envelope. Figure 3 shows the location of the long section shown in Figure 4 and the cross section shown in Figure 1 across the Old Austen Mine Open Pit Ore Reserve shell and the Old Austen Mine Down-Plunge Prospect.

Figure 3. Old Austen Mine Geology, Nova Scotia, Canada

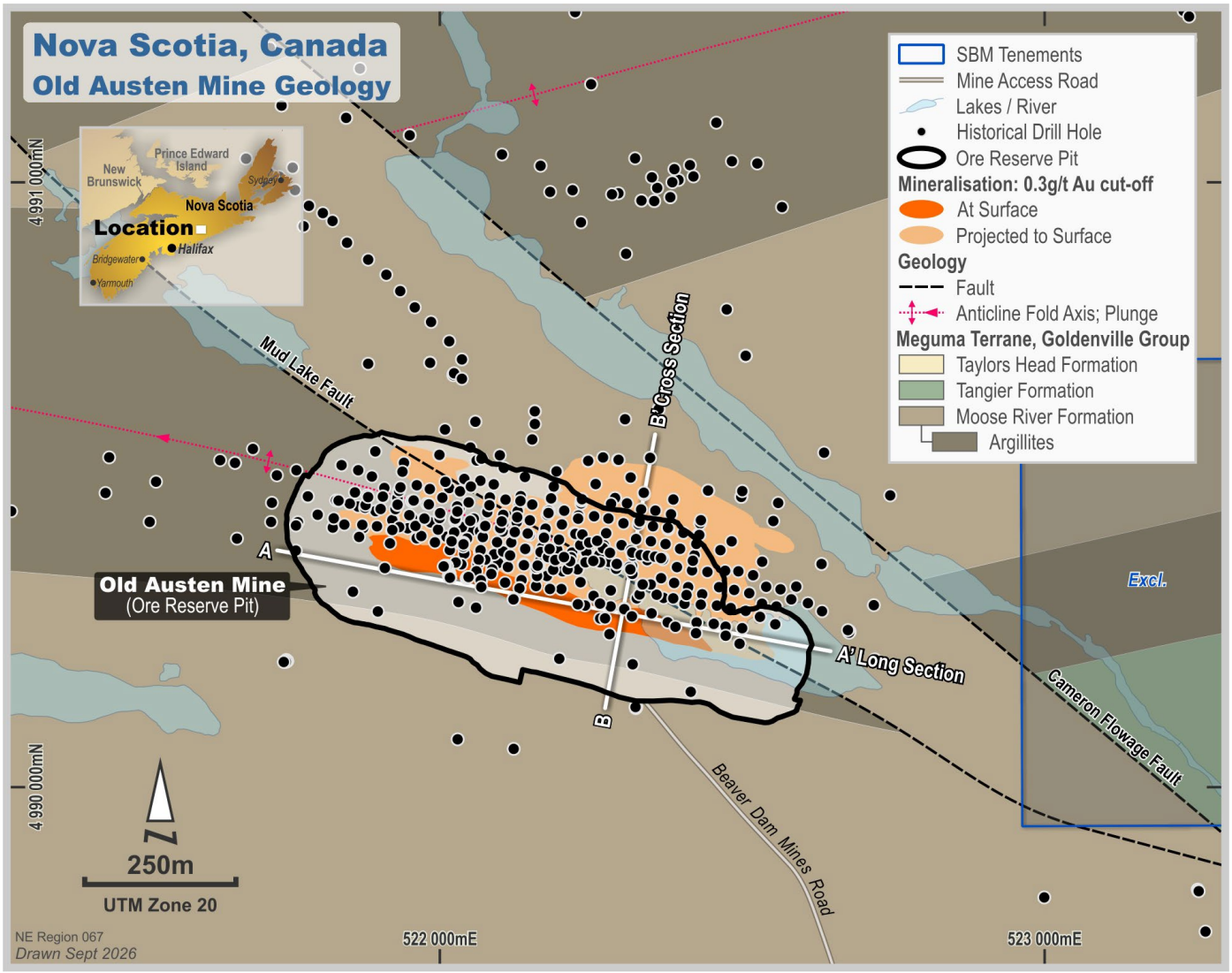
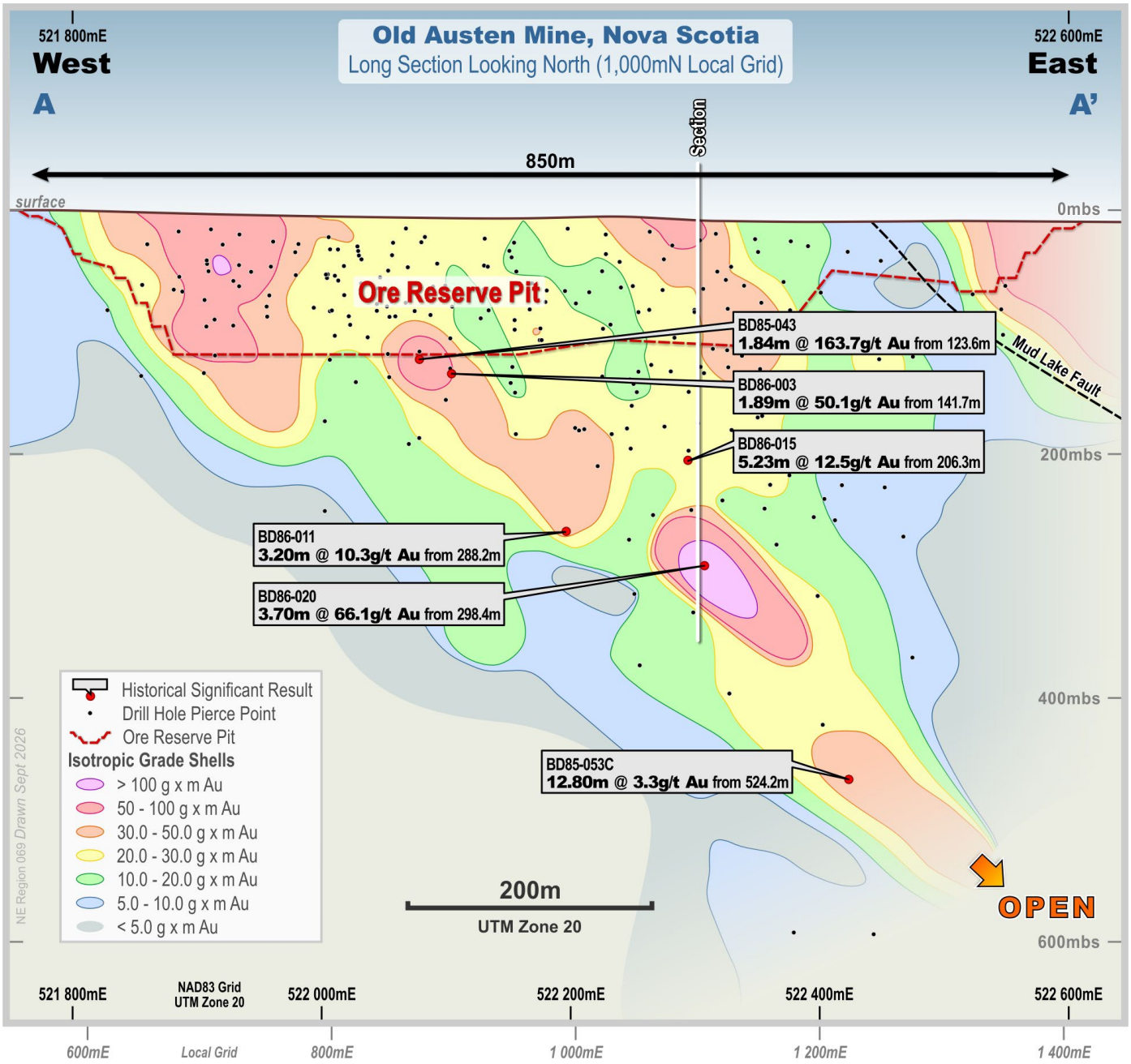


Figure 4 below is a contoured long section of gold mineralisation in 'gram-metres' for all drilling at the Old Austen Mine Down-Plunge Prospect after incorporation of the most recent additional historical data set. The location of the Old Austen Mine Open Pit Ore Reserve shell is overlain and the mid-point of the most significant drill intercept for each hole is shown as a black dot. Drilling extends up to approximately 575 m below surface and approximately 460 m vertically below the limits of the Open Pit Ore Reserve shell (between 115 mbs and 575 mbs). The high-grade 'gram-metre' gold contours of ≥30 gram-metres located below the Open Pit Ore Reserve shell define a semi-continuous domain that is 450 m long and plunges approximately -40° to the east within the plane (looking north). Gold grade is composited assuming a cut-off grade of 1 g/t Au, a minimum width of 2 m and a maximum internal dilution of 3 m. True widths have been used in the long section and calculated based on an average dip of -70° to the north and are recorded in Table 1.

Figure 4. Old Austen Mine Down-Plunge Prospect Long Section, Nova Scotia, Canada



Significant historical drill intercepts located on the Long Section for the Old Austen Mine Down-Plunge Prospect include:

- **BD85-043: 1.84 m (true width) @ 163.7 g/t Au from 123.6 m;**
- **BD86-003: 1.89 m (true width) @ 50.1 g/t Au from 141.7 m;**
- **BD86-011: 3.20 m (true width) @ 10.3 g/t Au from 288.2 m;**
- **BD86-015: 5.23 m (true width) @ 12.5 g/t Au from 206.3 m;**
- **BD86-020: 3.70 m (true width) @ 66.1 g/t Au from 298.4 m; and**
- **BD86-053C: 12.80 m (true width) @ 3.3 g/t Au from 524.2 m.**

FY26 and FY27 Exploration Work Program

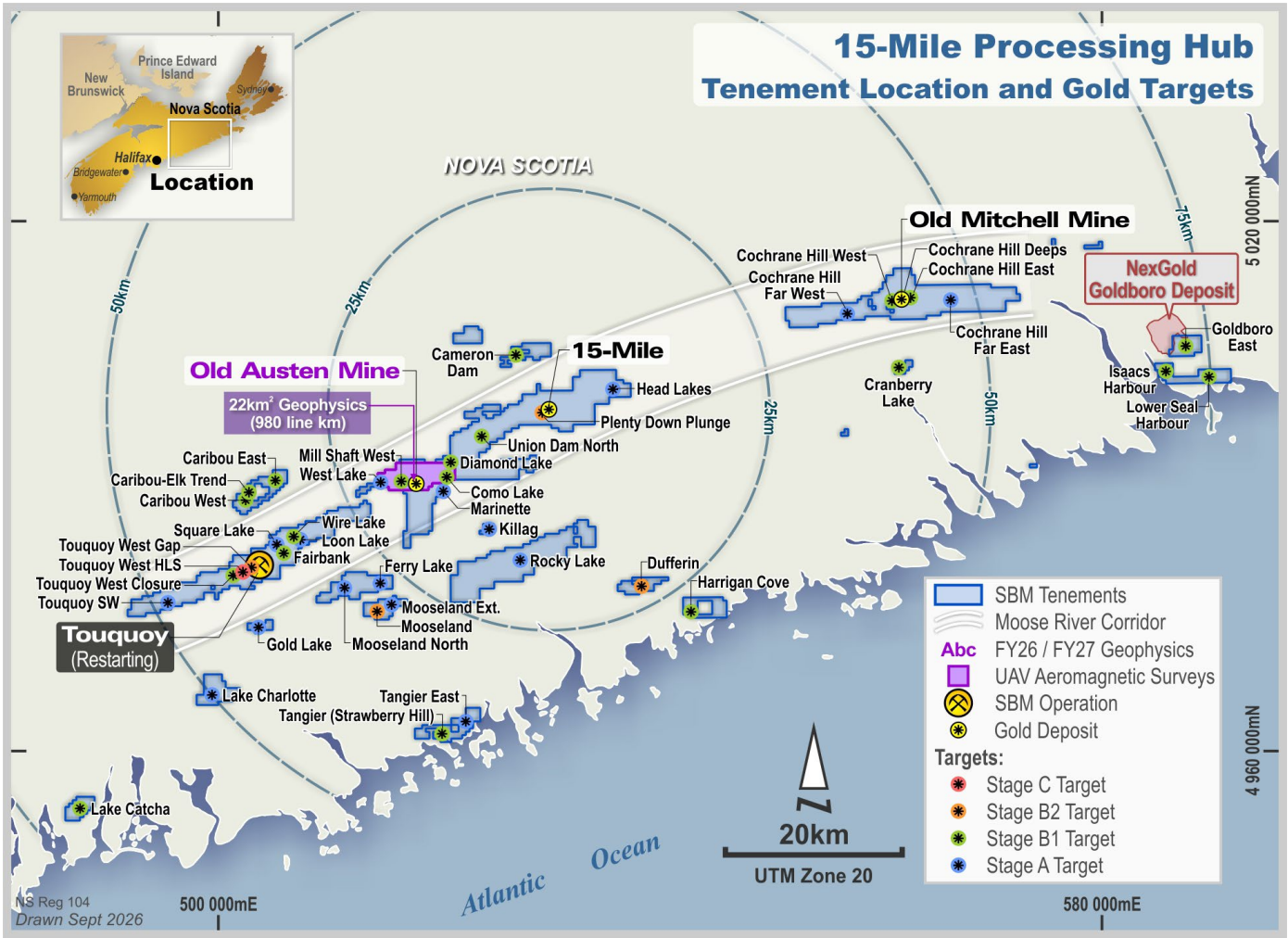
The recent ASX release dated 5 August 2026 titled "*Accelerating Nova Scotia Gold Exploration Activity*" outlined deposit and near-mine geophysical surveys as well as structural studies to advance drill targeting in the brownfield environment.

The accelerated work program in the region around the Old Austen Mine location includes:

- Acquisition of approximately 22 km^2 of high-resolution UAV magnetic survey data, comprising approximately 980 line-kilometres, across the Old Austen Mine location and the immediate surroundings;
- Generation of detailed magnetic images and a 3D magnetic inversion model; and
- A detailed structural review of all diamond drilling available for the Old Austen Mine location and surrounds with the aim of completing a structural model to support drill targeting to test the potential for the Old Austen Mine Down-Plunge Prospect.

Figure 5 below shows the tenement holdings within 75 km of the proposed 15-Mile Processing Hub Project and the proximity to the Touquoy Mine (planned to restart by December 2026), 15-Mile, Old Austen Mine and Old Mitchell Mine deposits. The Old Austen Mine is located 17 km west-southwest of the planned 15-Mile Processing Hub Project. The location of the planned 22 km^2 (980 line-kilometres) high-resolution UAV magnetic survey and 3D inversion modelling around the Old Austen Mine location is highlighted in purple. The UAV magnetic survey will be completed in early October with the detailed structural review to be completed early H2 June FY27.

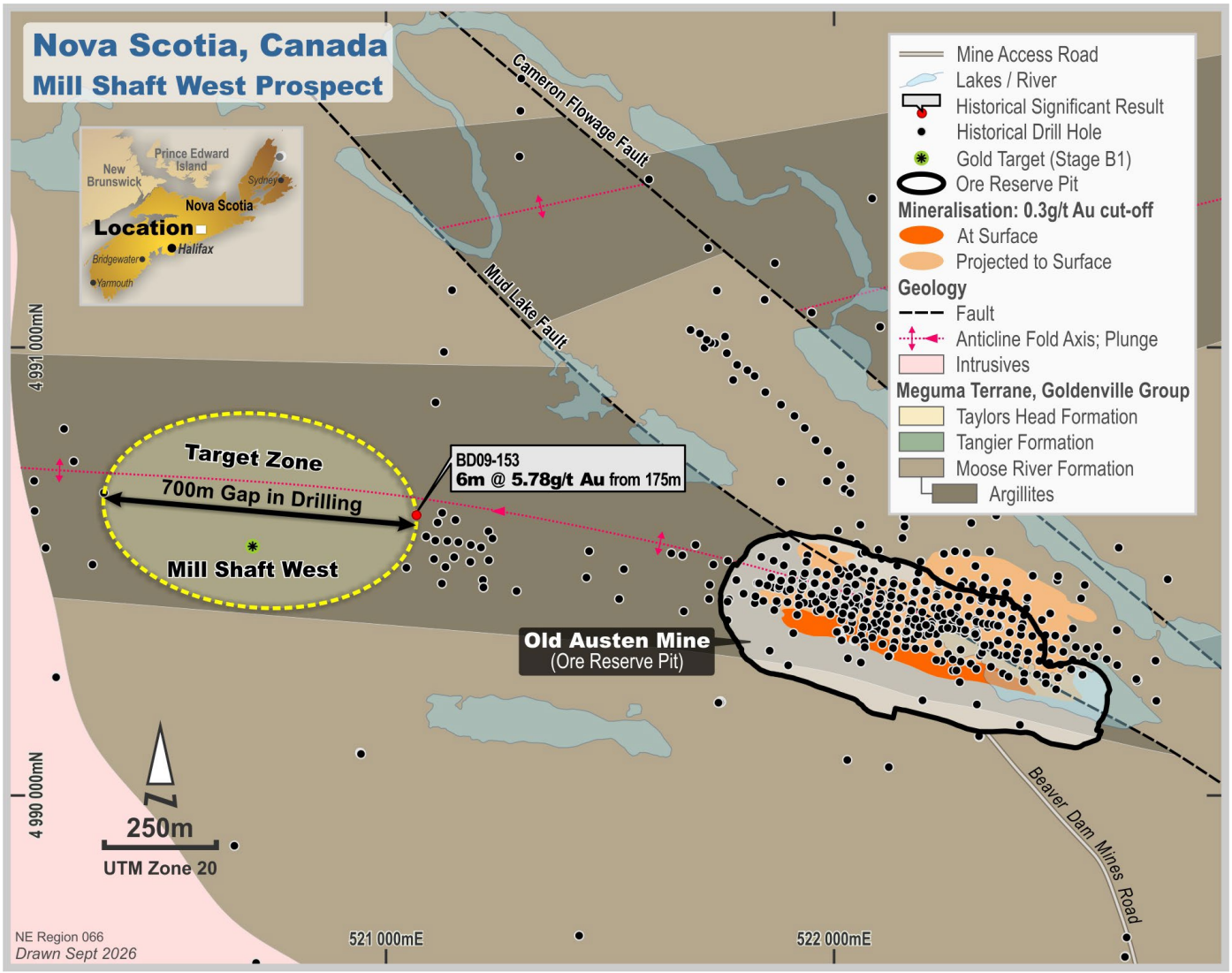
Figure 5. 15-Mile Processing Hub Exploration Targets and Old Austen Mine Down-Plunge Prospect and Mill Shaft West Prospect Locations, Nova Scotia, Canada



Mill Shaft West Prospect

Figure 6 below shows the Mill Shaft West zone, which is located west of the Old Austen Mine Open Pit Ore Reserve. The Mill Shaft West area has historical workings and past drilling targeting the western extension of the anticline. A significant intercept of **BD09-153: 6 m @ 5.78 g/t Au from 175 m** is reported from the western-most historical hole adjacent to a 700 m gap in both drilling and surface sampling along the anticline. Like Old Austen Mine Down-Plunge Prospect any discovery at Mill Shaft West would be an underground target and not an open pit possibility. The lack of surface geochemistry or drilling for 700 m to the west of this significant intercept presents an attractive immediate target for drill testing commencing Q4 June FY27 or Q1 September FY28. All drilling data and significant assay results from the Mill Shaft West area are outlined in Table 3.

Figure 6. Mill Shaft West Prospect, Nova Scotia, Canada



The Old Austen Mine Down-Plunge Prospect and along strike at Mill Shaft West Prospect were already identified respectively as Stage D (Feasibility Ready) and as Stage B1 (Drill Target) as shown in Figure 7 below.

Figure 7. 15-Mile Processing Hub Exploration Pipeline, Nova Scotia, Canada

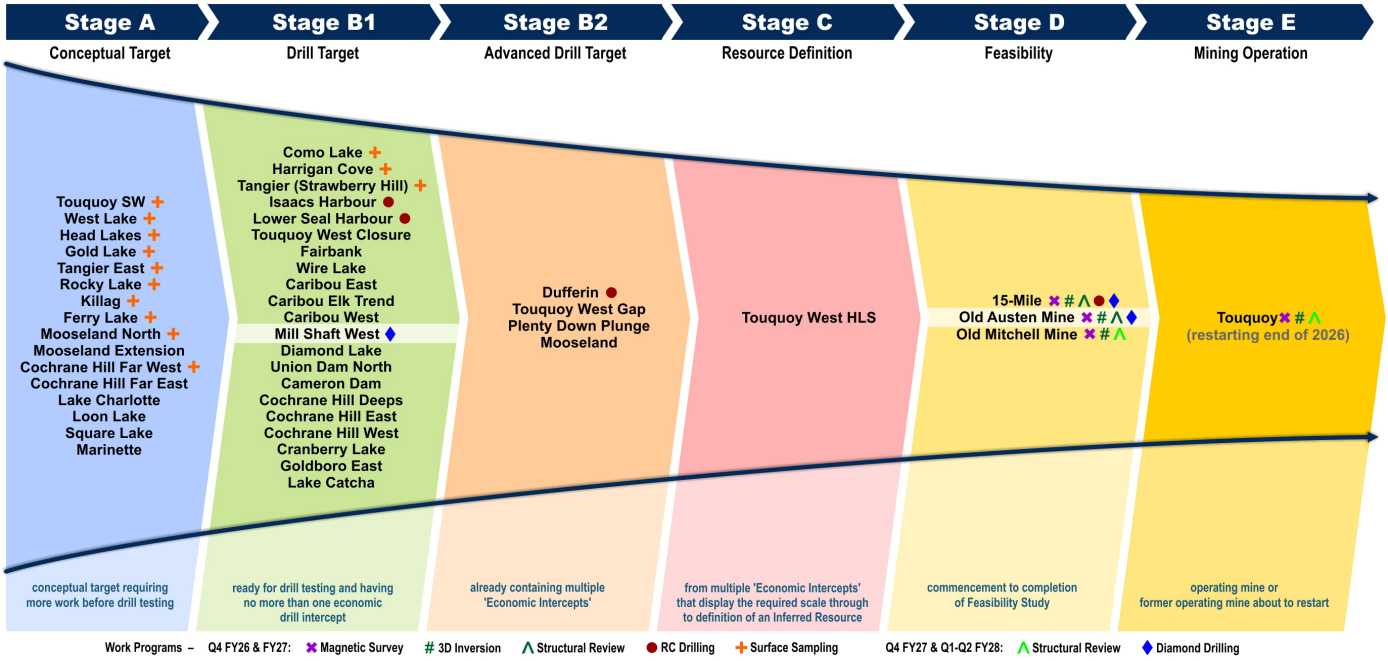


Table 1: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD05-001*	521997.15	4990425.7	133.5	-45/199.5	82	521987.0	4990397.4	104.8	38	45	7	6.39	5.1	32.6
BD05-001						521984.3	4990390.2	97.7	49	55	6	5.48	3.9	21.4
BD05-002	522071.23	4990413.4	133.7	-55/190	107	522063.7	4990376.8	80.5	64	66	2	1.65	1.7	2.8
BD05-002						522063.0	4990373.4	75.6	70	72	2	1.65	1.6	2.6
BD05-002*						522061.3	4990365.4	64.3	79	91	12	9.94	2.8	27.8
BD05-003*	522089.88	4990384.9	133.2	-45/190	73.2	522086.1	4990365.1	113.0	26	31	5	4.54	2.3	10.4
BD05-003						522085.2	4990360.5	108.5	34	36	2	1.82	1.2	2.2
BD05-006	522254.33	4990316.1	131.2	-70/194.1	110.2	522252.3	4990308.0	109.8	22	24	2	1.35	2.4	3.2
BD05-006*						522249.0	4990293.2	77.1	57	61	4	2.93	4	11.7
BD05-008*	522305.1	4990294.1	130.9	-41.7/190	83	522301.8	4990276.1	114.6	15	34	19	17.65	7.3	128.8
BD05-009*	522282.49	4990298.6	130.8	-42.2/189.1	80	522278.8	4990276.3	110.4	26	35	9	8.35	1.6	13.4
BD05-010	522318.1	4990364.7	132.3	-42.9/187.3	113	522311.1	4990314.0	85.3	68	71	3	2.78	1.6	4.4
BD05-010						522310.0	4990307.0	79.0	78	80	2	1.86	1.1	2.0
BD05-010*						522309.3	4990302.1	74.8	81	90	9	8.41	2.3	19.3
BD05-011	522366.03	4990345.4	134.4	-46.1/190.5	140	522356.1	4990293.1	80.3	74	78	4	3.65	2.2	8.0
BD05-011*						522352.9	4990275.6	63.4	92	109	17	15.67	5.8	90.9
BD05-013*	521969.51	4990415.1	132.8	-41.8/184.1	121	521967.8	4990393.5	113.5	21	37	16	14.89	10.9	162.3
BD05-017	521921.53	4990441.5	133.4	-45/190	120	521918.0	4990422.0	113.6	26	30	4	3.63	2	7.3
BD05-017						521917.4	4990418.5	110.1	32	34	2	1.81	1.6	2.9
BD05-017*						521914.7	4990403.9	95.2	52	56	4	3.63	129.9	471.5
BD05-017						521912.9	4990394.2	85.3	67	69	2	1.81	2.4	4.3
BD05-018	521949.65	4990449.5	133.9	-45/190	129	521943.6	4990416.5	100.3	46	49	3	2.72	5.2	14.1
BD05-018*						521942.6	4990410.6	94.3	54	58	4	3.63	122.3	443.9
BD05-018						521939.5	4990393.6	76.9	79	82	3	2.72	1.7	4.6
BD05-020*	522086.8	4990360	132.9	-45/185.5	80	522085.2	4990344.6	117.3	15	29	14	12.67	4.6	58.3
BD05-021*	522103.97	4990422.5	133.8	-45/190	130	522095.8	4990365.0	76.7	78	85	7	6.41	3.1	19.9
BD05-021						522095.1	4990358.8	70.8	89	91	2	1.83	2	3.7
BD05-022*	522118.22	4990404.5	132.7	-45.1/196.1	110	522103.1	4990349.3	77.5	76	83	7	6.45	2.4	15.5
BD05-022						522101.6	4990343.2	71.7	87	89	2	1.85	1.7	3.1
BD05-023*	521973.77	4990443.6	133.8	-46.2/188.1	110	521967.9	4990404.1	93.0	53	61	8	7.26	3.5	25.4
BD05-023						521965.4	4990387.2	76.2	80	82	2	1.82	3	5.5
BD05-024	522019.78	4990410.2	134.2	-45/192.8	100	522015.6	4990392.6	116.3	20	31	11	10.01	1.9	19
BD05-024*						522013.4	4990383.5	107.2	36	41	5	4.56	15.3	69.8
BD05-025*	522045.09	4990411.1	133.3	-46.3/190	100	522038.6	4990378.1	99.0	45	51	6	5.46	1.9	10.4
BD05-025						522037.7	4990373.6	94.5	53	56	3	2.74	1.4	3.8
BD05-026*	522138.97	4990368.5	132.7	-45/190.4	100	522131.6	4990328.8	93.9	55	57	2	1.85	1.5	2.8
BD05-028*	522159.75	4990353.09	132.4	-45/190	80	522153.0	4990320.5	100.6	45	47	2	1.84	1.2	2.2

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD05-029*	522174.26	4990423.07	131.1	-45/190	140	522157.1	4990328.7	41.3	130	133	3	2.86	12.6	36.0
BD05-030	522211.4	4990360.04	130.9	-45/198	98	522201.0	4990326.6	96.6	48	50	2	1.82	1.4	2.5
BD05-030*						522194.2	4990302.4	73.0	81	86	5	4.61	4.8	22.1
BD05-031*	522387.60	4990337.54	134.5	-45/194.7	120.5	522372.8	4990283.3	80.5	77	79	2	1.83	2	3.7
BD05-032*	522192.91	4990378.85	131.4	-46/190	97	522182.9	4990323.8	73.5	78	83	5	4.49	3.6	16.2
BD05-033*	522127.19	4990437.99	132.4	-45/192.1	150.2	522112.0	4990366.1	60.2	101	105	4	3.69	2.5	9.2
BD05-034	522066.22	4990388.39	133.6	-45.9/194.6	80	522059.7	4990364.1	107.9	35	37	2	1.81	11.1	20.1
BD05-034*						522054.9	4990346.1	89.8	60	64	4	3.66	13.1	47.9
BD05-036	522025.33	4990440.69	134.3	-42.4/193.5	120	522015.3	4990401.1	97.5	49	61	12	11.15	1.8	20.1
BD05-036*						522011.3	4990385.8	83.7	73	79	6	5.59	4.4	24.6
BD05-037*	521947.13	4990427.87	133.8	-43.6/194	80	521943.4	4990413.1	119.4	17	25	8	7.35	3.3	24.3
BD05-037						521939.7	4990397.3	104.6	42	44	2	1.85	1.9	3.5
BD05-037						521936.0	4990381.3	89.9	64	66	2	1.86	2.4	4.5
BD05-038	521920.65	4990425.05	133.6	-45.1/193.7	92	521918.0	4990414.4	122.7	13	18	5	4.52	1.8	8.1
BD05-038*						521911.8	4990390.2	98.2	49	52	3	2.75	4.1	11.3
BD05-039*	521896.26	4990431.19	134.9	-42/191	72.5	521893.4	4990417.0	121.8	18	21	3	2.78	9.6	26.7
BD05-039						521889.7	4990395.3	102.2	47	51	4	3.72	2.3	8.6
BD05-043*	522032.39	4990460.65	136.4	-45.5/190.8	91.3	522022.5	4990410.6	85.6	71	73	2	1.83	1.1	2.0
BD05-044*	522218.85	4990387.74	131.4	-46.8/190	125.2	522207.3	4990324.4	62.9	93	95	2	1.8	5.5	9.9
BD05-046*	522247.31	4990400.30	131.3	-45.1/192.3	150	522227.9	4990313.5	42.1	125	127	2	1.81	17.7	32.0
BD06-048*	522202.01	4990434.23	131.3	-42.7/192.2	200	522176.6	4990321.4	32.8	151	153	2	1.9	6.2	11.8
BD06-050*	522131.70	4990468.16	132.3	-47.2/195.2	180.1	522112.5	4990377.5	34.2	132	138	6	5.39	1.1	5.9
BD06-051	522369.14	4990378.27	134.9	-58.4/189.6	181	522357.1	4990304.1	14.5	141	143	2	1.6	1.4	2.2
BD06-051*						522356.5	4990300.6	9.0	146	151	5	4.01	1.4	5.6
BD06-051						522355.4	4990294.9	0.3	158	160	2	1.61	2.5	4.0
BD06-052*	522461.94	4990330.58	133.5	-43.7/188	170	522448.3	4990244.4	49.7	119	123	4	3.66	2.9	10.6
BD06-054*	522511.82	4990320.59	131.4	-45.3/190.8	170	522493.6	4990236.2	44.5	118	127	9	8.15	2.8	22.8
BD06-057*	522410.80	4990330.53	133.9	-43.5/190.5	172	522400.5	4990265.6	71.7	89	92	3	2.77	1.4	3.9
BD06-059*	522105.13	4990435.74	134.0	-53.1/190	152	522095.1	4990372.5	53.4	93	113	20	17.22	2.6	44.8
BD06-061*	522532.90	4990303.21	131.6	-46.2/188.6	161	522519.1	4990226.5	50.5	111	114	3	2.75	1.29	3.5
BD06-062*	522556.70	4990298.55	131.7	-43.8/191.7	170	522543.0	4990223.0	58.0	104	109	5	4.57	6.7	30.6
BD06-066*	522417.14	4990358.32	134.7	-45/190	179	522401.6	4990272.8	47.8	120	126	6	5.44	4	21.8
BD06-068*	522392.24	4990363.70	134.7	-40.1/189.7	180	522376.0	4990270.9	57.2	121	123	2	1.9	3.8	7.2
BD06-070*	522343.07	4990375.23	134.8	-45/190	170	522329.4	4990300.1	58.4	93	123	30	27.19	2.9	78.9
BD06-072	522442.61	4990355.75	134.3	-47/198	197	522413.4	4990273.4	40.8	127	129	2	1.77	1.2	2.1

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD06-072*						522411.6	4990268.6	35.3	134	137	3	2.66	1.7	4.5
BD06-074*	522255.28	4990447.81	131.7	-47/189.6	200	522229.6	4990325.6	2.9	176	183	7	6.4	3	19.2
BD06-076*	522205.82	4990456.97	131.3	-46.4/189.6	209	522185.8	4990362.5	32.8	136	140	4	3.64	7.5	27.3
BD06-076						522184.5	4990356.2	26.5	146	148	2	1.82	1.6	2.9
BD06-078	522240.26	4990300.18	134.2	-70.8/194.5	73	522238.7	4990294.1	116.3	18	20	2	1.26	8.1	10.2
BD06-078*						522237.0	4990287.5	96.9	35	44	9	5.75	2.4	13.8
BD06-079	522349.17	4990406.44	134.3	-50/190	209	522333.0	4990317.3	25.0	141	143	2	1.75	1.2	2.1
BD06-079*						522330.7	4990304.5	10.5	154	169	15	13.33	2.5	33.3
BD06-080	522232.81	4990338.73	131.3	-45/191.4	100	522228.0	4990315.5	107.0	33	35	2	1.8	1.7	3.1
BD06-080*						522224.4	4990298.3	89.2	56	62	6	5.45	2.9	15.8
BD06-081	521999.66	4990444.82	134.3	-45/190	170	521988.6	4990401.0	90.4	62	64	2	1.84	2.6	4.8
BD06-081*						521987.3	4990396.4	86.0	68	71	3	2.76	2.1	5.8
BD06-082*	522201.08	4990327.48	132.3	-45/190	116	522199.6	4990319.5	124.1	8	15	7	6.33	6.1	38.6
BD06-084*	521953.78	4990472.58	133.6	-45/194.8	161	521939.6	4990420.0	81.3	74	77	3	2.77	1.7	4.7
BD06-085*	522159.23	4990332.39	132.5	-45/195.7	102	522153.8	4990313.4	112.7	27	29	2	1.8	7.1	12.8
BD06-086*	521905.50	4990480.18	130.8	-41.6/190	153	521896.2	4990429.1	84.7	67	72	5	4.65	4.2	19.5
BD06-086						521891.6	4990403.7	61.8	102	106	4	3.72	3.4	12.6
BD06-088*	521930.02	4990477.80	132.6	-55/194.3	170	521917.7	4990431.2	65.7	79	86	7	5.86	3.5	20.5
BD06-090*	521926.85	4990459.63	133.1	-45/191	140	521918.3	4990416.7	89.2	60	64	4	3.62	15.6	56.5
BD06-090						521912.4	4990387.5	59.5	103	105	2	1.81	23.9	43.3
BD06-094	521908.37	4990494.52	130.8	-41.6/188.6	186	521899.5	4990434.5	77.2	79	83	4	3.73	1.3	4.8
BD06-094*						521898.8	4990429.3	72.6	87	89	2	1.86	3.3	6.1
BD06-095*	521865.23	4990523.85	130.8	-45/196.4	197	521839.5	4990446.2	57.3	109	111	2	1.86	2.7	5.0
BD06-095						521837.8	4990441.1	52.9	116	118	2	1.87	2.2	4.1
BD06-097*	522282.77	4990325.19	130.1	-45/193.6	101	522274.6	4990291.6	99.0	40	53	13	12.18	2.7	32.9
BD06-098*	522291.64	4990361.03	130.6	-45/195.1	129	522275.3	4990301.4	73.8	72	96	24	22.52	1.9	42.8
BD06-099	522330.44	4990318.48	130.0	-44/198.8	101	522321.6	4990293.0	104.0	36	39	3	2.71	2	5.4
BD06-099						522319.6	4990287.2	98.1	45	47	2	1.81	1.2	2.2
BD06-099*						522316.7	4990278.4	89.0	53	65	12	10.83	1.6	17.3
BD06-100*	522350.23	4990287.24	130.0	-45/191.7	89	522347.0	4990272.3	115.6	20	22	2	1.86	1.7	3.2
BD06-101*	522333.83	4990334.68	130.2	-45/183.6	122	522331.1	4990294.4	92.9	53	57	4	3.7	7.4	27.4
BD06-101						522330.3	4990280.5	80.7	72	75	3	2.79	3.6	10.0
BD06-102*	522358.70	4990318.08	130.4	-45/191.5	120	522352.8	4990289.8	105.1	37	40	3	2.86	1.7	4.9
BD06-107*	522377.02	4990272.42	129.7	-45/190	96	522373.9	4990256.8	113.8	21	24	3	2.72	4.3	11.7
BD06-108*	522228.37	4990302.28	134.1	-45/190	86	522225.4	4990287.6	119.4	20	22	2	1.82	9.7	17.7

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD06-108						522223.3	4990278.5	110.3	33	35	2	1.83	1.7	3.1
BD06-109*	522389.74	4990265.05	129.6	-45/190	68	522386.2	4990245.6	109.8	23	33	10	9.06	3.3	29.9
BD06-110*	522264.98	4990303.39	130.5	-45/190	80	522263.4	4990294.7	121.7	11	14	3	2.72	33.1	90.0
BD06-110						522261.9	4990286.7	113.5	20	28	8	7.25	3.9	28.3
BD06-110						522260.0	4990276.3	102.9	36	42	6	5.44	9.2	50.0
BD06-111*	522317.74	4990282.28	130.5	-45/198.4	80	522314.3	4990272.2	119.9	12	18	6	5.41	6.1	33.0
BD06-111						522311.8	4990264.8	112.2	24	28	4	3.62	1.6	5.8
BD06-112*	522300.61	4990400.03	134.6	-57.3/190	200	522286.8	4990326.2	7.1	146	150	4	3.06	19.2	58.8
BD06-112						522283.3	4990312.0	-17.9	172	182	10	7.72	2.4	18.5
BD06-113	522324.67	4990410.09	135.3	-60.6/190	224	522309.7	4990327.6	-12.6	168	172	4	3.07	1.8	5.5
BD06-113						522309.1	4990324.2	-18.7	176	178	2	1.54	1.5	2.3
BD06-113*						522307.3	4990314.4	-35.5	194	199	5	3.86	2.2	8.5
BD06-114	522352.61	4990431.27	133.1	-57.2/190	230	522338.8	4990341.9	-5.4	163	168	5	4.08	3.9	15.9
BD06-114*						522335.7	4990316.9	-40.9	200	218	18	14.9	2.5	37.3
BD06-115	522397.43	4990393.99	134.6	-45/190	230	522379.7	4990296.6	35.6	137	143	6	5.44	1.6	8.7
BD06-115*						522378.0	4990287.2	26.0	151	156	5	4.53	6.9	31.3
BD06-117*	522424.71	4990272.21	130.0	-45/190	90	522419.5	4990246.7	105.2	35	37	2	1.85	2.4	4.4
BD06-118*	522453.10	4990269.86	129.6	-42.5/193	81	522445.1	4990236.1	97.8	44	50	6	5.54	2.7	15.0
BD06-119*	522464.06	4990391.72	132.7	-45/190	233	522439.7	4990257.5	-3.8	192	194	2	1.81	2.4	4.3
BD06-120*	522493.83	4990356.73	132.5	-45/190	197	522474.9	4990252.7	19.2	154	156	2	1.75	1.4	2.5
BD06-121*	522518.18	4990350.25	131.3	-42/192	200	522491.2	4990239.1	31.3	151	153	2	1.87	3.2	6.0
BD06-122*	522539.77	4990331.18	133.1	-45/188	189.3	522517.3	4990235.6	36.2	136	140	4	3.63	3.6	13.1
BD06-123*	522563.44	4990326.99	133.6	-45/190	191.5	522546.1	4990231.3	37.1	136	138	2	1.82	1.1	2.0
BD06-128*	522554.80	4990269.17	130.7	-45/190	102.5	522545.3	4990216.7	77.3	73	78	5	4.53	19.3	87.4
BD06-129	522529.52	4990281.53	130.5	-45/190	110	522520.7	4990233.2	81.4	68	71	3	2.72	1.2	3.3
BD06-129*						522519.1	4990222.3	70.4	83	87	4	3.45	3.28	11.3
BD06-130*	522269.36	4990379.14	131.4	-45/190	134	522255.8	4990304.7	55.7	106	108	2	1.81	2.7	4.9
BD06-131*	522148.45	4990416.85	131.8	-45/190	122	522137.6	4990357.0	71.0	85	87	2	1.81	3	5.4
BD06-132*	522067.21	4990506.51	135.5	-45/190	167	522049.3	4990407.7	35.1	140	144	4	3.63	2.9	10.5
BD06-133*	521917.71	4990402.97	135.6	-45/190	65	521915.6	4990391.1	123.6	15	19	4	3.63	3.8	13.8
BD07-134*	522303.74	4990436.12	132.5	-60/188	250	522281.6	4990326.8	-38.1	201	207	6	4.98	13.9	69.2
BD07-135*	522356.57	4990457.10	133.2	-65/190	310	522334.8	4990353.3	-98.7	252	258	6	4.22	1.5	6.3
BD07-136*	522315.68	4990511.85	133.5	-65/190	372.5	522284.6	4990393.9	-110.7	265	281	16	11.88	1.3	15.4
BD07-137*	522105.99	4990527.76	132.1	-64/188	275	522088.4	4990433.5	-52.4	206	210	4	3	10.5	31.5
BD07-138*	522402.77	4990420.44	134.0	-65/190	275	522385.1	4990323.2	-78.1	228	240	12	8.49	2.2	18.7

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD07-139*	522257.824	4990500.994	131.6	-60/190	290	522237.0	4990386.2	-70.6	222	245	23	17.62	2.6	45.8
BD07-139						522234.0	4990369.9	-99.1	265	268	3	2.3	3.1	7.1
BD09-140	521932.9838	4990429.969	133.3	-45/190	105	521930.2	4990415.9	119.3	18	22	4	3.66	1.8	6.6
BD09-140*						521928.3	4990407.4	111.1	29	35	6	5.52	2.6	14.4
BD09-140						521923.0	4990385.8	91.0	61	63	2	1.86	1.1	2.0
BD09-141	521959.8282	4990431.779	133.4	-45/190	95	521954.5	4990407.9	109.8	31	37	6	5.52	2.4	13.2
BD09-141						521950.4	4990393.6	96.4	52	56	4	3.7	3.3	12.2
BD09-141*						521948.0	4990385.3	88.8	63	68	5	4.63	5.7	26.4
BD09-141						521946.1	4990379.2	83.2	71	77	6	5.57	1.2	6.7
BD09-142*	522075.2433	4990376.062	133.2	-45/190	47	522073.7	4990367.4	124.3	11	14	3	2.72	1.5	4.1
BD09-143*	522104.7955	4990389.433	131.4	-45/190	83	522097.0	4990352.7	95.5	51	53	2	1.85	1	1.9
BD09-144	522348.8303	4990334.996	133.0	-45/190	110	522341.9	4990295.4	94.0	54	58	4	3.67	1.4	5.1
BD09-144*						522338.9	4990277.7	77.4	77	84	7	6.47	2.8	18.1
BD09-146*	521893.4822	4990554.949	130.0	-50/190	190.5	521867.9	4990447.6	3.4	167	169	2	1.77	1.9	3.4
BD09-148*	522069.0135	4990543.006	136.0	-45/190	215	522038.7	4990404.0	-1.7	197	199	2	1.83	2	3.7
BD09-149	522107.4706	4990475.147	133.3	-70/190	215	522093.7	4990413.7	-33.1	177	179	2	1.33	1.9	2.5
BD09-149*						522092.3	4990408.1	-47.5	192	195	3	2	1.7	3.4
BD09-150	522427.2693	4990417.284	134.8	-62/190	260	522425.3	4990311.1	-70.4	230	232	2	1.48	1.2	1.8
BD09-150*						522425.0	4990302.6	-86.2	248	250	2	1.49	1.8	2.7
BD09-152*	522279.2573	4990372.568	131.4	-45/190	130.5	522262.4	4990291.5	57.6	107	115	8	7.49	3.9	29.2
BD-110-01	522016.332	4990352.653	101.0	-46/002	111.36	522019.6	4990391.4	64.2	50	57.3	7.3	3.56	6.4	22.8
BD-110-01*						522025.1	4990424.9	36.4	95.6	99.5	3.9	2.05	12.5	25.6
BD-110-02*	522015.034	4990349.14	100.8	-15/017	65.23	522024.5	4990381.2	93.5	31.4	37.2	5.8	4.98	5	24.9
BD-110-03*	522015.374	4990349.332	100.9	-42/017	90.83	522025.5	4990384.7	69.7	47.2	49.4	2.2	1.09	2.9	3.2
BD-110-04	522015.309	4990349.09	100.8	-48/017	109.73	522027.8	4990387.1	62.6	54	56.8	2.8	1.41	2.5	3.5
BD-110-04*						522032.0	4990399.3	52.3	70.2	73.6	3.4	1.77	6.2	11.0
BD-110-05*	522016.079	4990349.803	100.9	-31/035	59.44	522038.9	4990381.6	79.4	39.6	49.8	10.2	6.35	4.2	26.7
BD14-154*	521932.765	4990489.746	132.0	-58/192	161	521919.8	4990434.7	43.9	94	112	18	14.66	20.9	306.4
BD14-155	521974.608	4990443.982	133.9	-58/193	173	521968.0	4990417.1	86.0	49	55	6	4.74	1.9	9.0
BD14-155*						521963.9	4990401.2	60.3	81	84	3	2.39	3.9	9.3
BD14-156*	521979.063	4990468.521	134.4	-58/192	158	521967.8	4990420.1	52.0	89	96	7	5.61	3.8	21.3
BD14-158*	522073.907	4990430.817	134.4	-59/192	140	522062.9	4990383.5	51.9	88	96	8	6.34	3.1	19.7
BD14-158						522060.5	4990374.6	37.6	108	110	2	1.59	2.8	4.5
BD14-159A*	522025.577	4990443.78	134.3	-60/190	122	522016.6	4990401.1	56.4	83	88	5	3.91	14.7	57.5
BD14-159A						522014.7	4990393.7	44.1	99	101	2	1.57	1.6	2.5

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD14-160	522078.58	4990454.54	134.9	-59/191	170	522066.7	4990403.2	42.7	100	104	4	3.13	3.9	12.2
BD14-160*						522062.9	4990390.7	21.4	122	132	10	7.82	2.2	17.2
BD14-160						522059.8	4990380.9	4.8	145	148	3	2.35	6.4	15.0
BD14-163*	522133.94	4990481.03	132.4	-61/192	221	522112.1	4990395.3	-16.2	168	174	6	4.85	1.3	6.3
BD14-164*	522233.79	4990469.02	131.5	-61/189	251	522223.5	4990373.7	-40.3	191	200	9	7.01	2.7	18.9
BD14-165*	522174.94	4990427.31	131.4	-59/190	185	522159.8	4990353.7	10.7	138	144	6	4.84	3.6	17.4
BD14-166	522228.81	4990443.79	131.4	-62/188	221	522217.5	4990366.1	-12.8	161	165	4	3.1	1.4	4.3
BD14-166						522215.1	4990352.2	-35.8	189	191	2	1.58	1.1	1.7
BD14-166*						522214.5	4990348.8	-41.3	194	199	5	3.97	25	99.3
BD14-167*	522180.14	4990456.63	131.5	-59/192	212	522162.4	4990375.1	-2.4	155	158	3	2.42	4.1	9.9
BD14-169*	522278.95	4990444.09	131.4	-61/190	269	522260.5	4990359.8	-21.1	171	177	6	4.64	2.7	12.5
BD14-169						522259.8	4990357.1	-25.8	178	181	3	2.32	1.2	2.8
BD14-169						522255.8	4990339.2	-56.2	214	216	2	1.56	4.2	6.6
BD14-170	522263.72	4990383.67	131.4	-61/184	173	522259.0	4990326.8	26.7	117	119	2	1.52	3.1	4.7
BD14-170*						522257.8	4990315.3	6.9	140	142	2	1.55	10.3	16.0
BD14-171*	522271.56	4990399.69	131.8	-60/194	212	522252.4	4990324.4	0.5	149	153	4	3.2	3.6	11.5
BD14-172*	521938.32	4990521.48	131.3	-59/191	180.54	521919.7	4990445.2	5.8	142	152	10	8.02	2.4	19.2
BD14-173*	522275.20	4990419.72	131.8	-60/190	254	522258.9	4990343.1	-3.2	153	156	3	2.35	2.7	6.3
BD14-174*	522313.67	4990363.63	132.2	-58/192	149	522305.0	4990318.2	57.5	84	88	4	3.24	8.3	26.9
BD14-174						522304.0	4990310.9	46.8	97	101	4	3.25	1.8	5.9
BD14-174						522303.5	4990305.8	39.4	105	111	6	4.89	3.3	16.1
BD14-175*	522028.86	4990463.99	135.6	-60/190	149	522015.8	4990397.6	16.7	131	133	2	1.57	2.1	3.3
BD14-176	522328.63	4990434.78	133.5	-61/193	266	522307.0	4990349.5	-25.3	177	180	3	2.31	2.1	4.9
BD14-176						522305.4	4990343.4	-36.1	190	192	2	1.55	7.7	11.9
BD14-176						522304.3	4990338.9	-43.8	198	202	4	3.11	2	6.2
BD14-176*						522302.4	4990330.5	-57.9	210	223	13	10.16	1.9	19.3
BD14-177*	522128.85	4990456.06	132.6	-59/190	190.2	522113.4	4990382.6	9.5	139	145	6	4.76	1.3	6.2
BD14-178	522332.93	4990459.01	132.4	-61/192	281	522304.8	4990350.4	-50.9	207	219	12	9.88	1.4	13.8
BD14-178*						522302.4	4990340.4	-65.1	227	234	7	5.82	2.7	15.7
BD14-179*	522188.56	4990496.94	131.6	-59/191	248	522168.8	4990386.4	-44.3	202	213	11	9.09	2.7	24.5
BD14-179						522167.5	4990379.2	-54.5	218	222	4	3.31	4.6	15.2
BD14-180*	522337.79	4990484.01	132.4	-61/190	290	522309.8	4990358.2	-106.6	269	374	5	4.6	9.95	45.8
BD14-181*	522369.10	4990377.44	135.0	-46/191	163	522351.3	4990300.4	49.3	106	120	14	12.66	2.8	35.4
BD14-181						522345.1	4990271.4	19.5	154	156	2	1.82	1.5	2.7
BD14-182	522316.28	4990391.48	134.7	-59/189	191	522299.9	4990314.9	-0.3	150	154	4	3.12	1.4	4.4

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD14-182*						522298.6	4990309.4	-9.7	161	165	4	3.13	2.9	9.1
BD14-183	522377.87	4990426.43	133.5	-62/193	251	522352.9	4990333.5	-49.9	198	210	12	9.07	2	18.1
BD14-183*						522350.9	4990325.9	-63.8	214	226	12	9.15	2.6	23.8
BD14-183						522349.7	4990321.6	-71.6	228	230	2	1.53	1.2	1.8
BD14-184*	522289.89	4990477.92	131.3	-59/198	286	522246.8	4990376.1	-44.3	201	212	11	8.74	1.8	15.7
BD14-184						522240.9	4990364.0	-63.6	229	231	2	1.6	1.2	1.9
BD14-184						522239.9	4990362.0	-66.9	233	235	2	1.6	1.3	2.1
BD14-185	522382.38	4990451.09	134.2	-63/190	284	522367.4	4990343.8	-84.1	239	241	2	1.5	4.3	6.5
BD14-185*						522366.0	4990331.8	-105.4	261	268	7	5.35	1.8	9.6
BD14-186*	522418.52	4990374.27	134.6	-60/188	215	522404.3	4990289.7	-22.0	172	177	5	3.84	2.8	10.8
BD14-187A	522431.82	4990441.18	135.1	-60/189	278	522413.0	4990318.3	-86.3	248	251	3	2.31	1.8	4.2
BD14-187A*						522412.1	4990311.7	-97.5	260	265	5	3.86	1.3	5.0
BD14-188*	522373.34	4990401.83	134.1	-60/187	212	522359.5	4990308.0	-29.4	177	194	17	13.36	2.5	33.4
BD85-001*	522135.21	4990342.27	132.2	-45/192	38.41	522131.7	4990326.4	116.0	19.7	26.3	6.6	5.98	11	65.8
BD85-007*	522075.13	4990431.73	134.9	-66/189	129.54	522068.8	4990388.8	52.3	89	97.8	8.8	6.77	3.3	22.3
BD85-009	522067.50	4990391.70	132.6	-50/192	72.24	522062.9	4990370.7	107.4	29.3	36.9	7.6	6.67	3	20.0
BD85-009*						522061.9	4990366.4	102.4	38.1	41.4	3.3	2.91	14.8	43.1
BD85-015*	522099.97	4990428.35	133.3	-72/196	155.45	522089.3	4990390.7	23.4	115.1	118.3	3.2	2.16	2.1	4.5
BD85-015						522088.9	4990389.2	19.5	119.8	121.9	2.1	1.42	1.6	2.3
BD85-016*	522145.44	4990419.26	131.2	-61/190	133.2	522136.6	4990370.7	50.6	93.6	95.6	2	1.65	3.9	6.4
BD85-019	522038.79	4990397.65	132.7	-45/190	85.36	522036.5	4990385.4	120.3	15.5	19.8	4.3	3.9	3.6	14.0
BD85-019*						522034.6	4990374.9	109.6	25.9	39.5	13.6	12.33	4	49.3
BD85-023*	521992.08	4990404.62	133.0	-45/193	60.96	521987.0	4990383.3	111.6	27.4	33.9	6.5	5.95	3.5	20.8
BD85-025*	522047.84	4990470.72	133.1	-50/194	152.4	522031.6	4990390.8	45.3	115.2	124.5	9.3	8.41	6.1	51.3
BD85-028*	522029.06	4990455.05	135.3	-50/192	121.92	522015.7	4990387.6	57.1	100.4	107.9	7.5	6.7	1.9	12.7
BD85-033*	521981.97	4990467.38	133.8	-51/194	128.32	521968.7	4990415.3	69.4	82.8	85	2.2	1.93	6.5	12.5
BD85-035*	521956.72	4990473.26	133.3	-52/196	138.38	521936.4	4990403.1	44.7	110.9	118.9	8	7.04	6.4	45.1
BD85-036*	522082.13	4990466.02	133.9	-64/197	182.88	522065.5	4990398.5	2.4	147.8	149.9	2.1	1.62	1.3	2.1
BD85-041	521930.24	4990466.96	133.3	-70/189	174.96	521926.3	4990433.3	53.7	85.1	88.1	3	2.15	1.4	3.0
BD85-041*						521926.0	4990431.4	49.6	89.5	92.7	3.2	2.3	4.4	10.1
BD85-043*	522104.96	4990449.95	133.6	-71/197	187.45	522092.2	4990406.9	17.0	123.6	126.3	2.7	1.84	163.7	301.2
BD85-043						522090.1	4990398.8	-2.4	144.6	147.5	2.9	2	6.6	13.2
BD85-044*	521935.02	4990495.60	133.4	-68/188	237.44	521928.6	4990443.1	20.2	123.4	126.6	3.2	2.36	2.8	6.6
BD85-051*	521905.95	4990480.34	130.5	-50/196	164.59	521892.7	4990434.9	74.1	72.3	74.9	2.6	2.24	1.9	4.3
BD85-054*	522040.64	4990509.45	135.4	-72/199	320.65	522020.8	4990446.6	-33.7	180	183.4	3.4	2.47	4.3	10.6

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD85-055*	521881.56	4990479.52	130.3	-51/199	126.49	521866.9	4990437.6	78.0	67.6	69.6	2	1.76	10.6	18.7
BD85-059*	522292.81	4990368.93	129.9	-63/186	177.7	522288.3	4990318.1	34.8	104.8	111.2	6.4	4.85	3.9	18.9
BD85-061*	522064.41	4990376.16	132.6	-60/190	44.5	522062.4	4990364.5	112.6	19.2	27.3	8.1	6.29	2	12.6
BD85-062*	522319.05	4990383.01	134.0	-63/189	175.56	522309.7	4990316.4	10.8	138.4	142.6	4.2	3.64	14.7	53.5
BD85-064*	522159.60	4990362.81	131.9	-55/192	44.5	522155.7	4990345.1	106.0	27.8	35.4	7.6	6.22	1.5	9.3
BD85-065*	522183.94	4990476.56	131.0	-50/192	255.12	522161.1	4990348.5	-10.3	190.9	193.4	2.5	2.28	7.2	16.4
BD85-068*	522315.18	4990360.00	130.3	-64/190	131.68	522305.3	4990319.3	55.9	84.3	86.6	2.3	1.82	2.2	4.0
BD85-071*	522335.53	4990335.09	129.6	-52/192	120.09	522327.4	4990297.8	82.1	59.4	62.5	3.1	2.68	5.1	13.7
BD85-072*	521866.64	4990413.61	132.5	-70/190	37.49	521865.3	4990406.1	111.4	20.3	24.6	4.3	2.76	5.5	15.2
BD85-078*	521781.96	4990480.62	135.8	-71/202	145.08	521772.5	4990458.4	70.8	68.3	70.4	2.1	1.4	4.3	6.0
BD85-079*	522471.91	4990357.66	133.5	-46/196	166.48	522446.5	4990251.2	17.1	158.7	161	2.3	2.05	34.8	71.3
BD85-082*	522269.93	4990395.15	131.6	-64/190	214.88	522257.8	4990322.5	-9.9	158.5	160.6	2.1	1.61	5.8	9.3
BD85-088*	522039.37	4990403.97	133.1	-50/186	83.84	522037.8	4990389.4	116.0	19.5	25.5	6	5.22	2.6	13.6
BD85-088						522036.3	4990377.3	102.2	32.2	49.8	17.6	15.6	2.6	40.6
BD86-001*	522235.08	4990475.96	130.6	-62/190	308.76	522216.7	4990378.3	-39.3	193.2	200.6	7.4	6.01	2.2	13.2
BD86-002*	522283.24	4990468.36	130.8	-61/190	318.52	522259.4	4990375.3	-39.7	193.7	197.8	4.1	3.23	10.1	32.6
BD86-002						522258.4	4990371.6	-45.7	201.2	204.5	3.3	2.61	5.3	13.8
BD86-003	522128.05	4990446.22	132.6	-65/192	181.97	522115.3	4990385.9	10.8	134.9	138.2	3.3	2.49	1.2	3.0
BD86-003*						522114.6	4990382.9	5.2	141.7	144.2	2.5	1.89	50.1	94.7
BD86-004*	522294.45	4990540.71	133.2	-63/190	382.83	522267.1	4990407.5	-130.9	292.3	302	9.7	7.38	2.5	18.5
BD86-004						522265.6	4990400.8	-142.9	309.8	312.1	2.3	1.76	6.8	12.0
BD86-005*	522102.47	4990439.25	133.9	-54/198	157.58	522083.9	4990383.5	56.6	96	98.2	2.2	1.88	3.5	6.6
BD86-006*	522295.73	4990541.10	133.5	-73/190	462.99	522275.1	4990426.9	-175.4	328.7	332.3	3.6	2.65	1.8	4.8
BD86-011*	522245.50	4990539.05	132.2	-63/193	405.08	522214.5	4990406.6	-124.1	288.2	292.3	4.1	3.2	10.3	33.0
BD86-015*	522330.47	4990439.31	132.0	-73/194	349.27	522309.6	4990371.8	-65.8	206.3	214.1	7.8	5.23	12.5	65.4
BD86-015						522307.1	4990365.0	-82.8	227.3	230	2.7	1.84	1.8	3.3
BD86-015						522303.9	4990356.4	-103.9	250.6	252.7	2.1	1.45	2.6	3.8
BD86-017*	522039.22	4990401.46	133.4	-50/188	70.1	522035.9	4990378.3	105.9	32	40.2	8.2	7.18	3.2	23.0
BD86-018*	522019.57	4990406.32	133.3	-46/201	70.83	522013.7	4990391.1	117.2	21.9	23.9	2	1.8	1.1	2.0
BD86-019*	522306.43	4990608.16	130.3	-70/193	527.3	522285.2	4990457.2	-233.9	390.4	400.4	10	7.5	1.7	12.8
BD86-020*	522337.40	4990486.68	130.6	-70/192	412.4	522325.7	4990384.3	-152.2	298.4	303.9	5.5	3.7	66.1	244.6
BD86-021*	522386.25	4990475.52	132.2	-74/191	390.75	522385.7	4990384.3	-134.9	280.2	284.7	4.5	2.88	2.4	6.9
BD86-021						522386.1	4990371.9	-167.1	314	319.8	5.8	3.9	1.5	5.9
BD86-024	522377.41	4990428.77	131.8	-64/190	325.91	522370.6	4990340.8	-59.8	210	212.1	2.1	1.46	3.3	4.8
BD86-024*						522370.1	4990328.6	-85.9	237.6	242.1	4.5	3.22	12.3	39.6

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD86-028*	522429.19	4990416.87	133.5	-76/192	300.53	522425.5	4990336.3	-114.9	260.2	262.6	2.4	1.56	1.8	2.8
BD86-033	522369.08	4990376.88	134.4	-70/190	237.74	522358.1	4990321.7	-10.7	153.4	157.9	4.5	3.05	3.3	10.1
BD86-033						522357.6	4990318.6	-18.2	162.7	164.9	2.2	1.5	4.1	6.2
BD86-033						522357.3	4990316.8	-22.6	167.3	169.8	2.5	1.71	1.4	2.4
BD86-033*						522356.8	4990313.3	-30.7	174	180.6	6.6	4.54	3.6	16.3
BD86-038*	522482.66	4990406.29	132.8	-68/193	309.98	522462.2	4990310.8	-88.0	240.5	242.5	2	1.4	8	11.2
BD86-041*	522443.73	4990490.28	129.9	-77/198	457.5	522425.3	4990412.9	-177.0	308.8	325.4	16.6	9.9	2.4	23.8
BD86-045*	522347.88	4990544.33	132.5	-74/190	474.27	522323.5	4990423.4	-190.6	344.7	347.8	3.1	2.24	4.8	10.8
BD86-048*	522443.73	4990490.28	129.9	-68/197	398.37	522417.6	4990389.0	-112.4	258.5	269.3	10.8	7.54	2.3	17.3
BD86-048						522415.5	4990381.3	-129.8	281.6	284.5	2.9	2.04	2.3	4.7
BD86-049*	522347.88	4990544.33	132.5	-84/195	526.4	522358.0	4990447.1	-257.1	398.5	407.5	9	5.92	3.5	20.7
BD86-050	522443.73	4990490.28	129.9	-86/214	534.92	522434.2	4990438.8	-271.0	399.2	410.1	10.9	5.76	1.6	9.2
BD86-050*						522433.9	4990436.3	-282.7	415	418.2	3.2	1.71	15.4	26.3
BD86-051*	522362.04	4990624.86	128.4	-82/177	558.7	522368.7	4990494.6	-308.2	261	268	7	5.35	1.8	9.63
BD86-052*	522152.92	4990574.78	133.7	-68/194	372.5	522124.3	4990456.3	-123.3	282.2	287.2	5	3.83	4	15.3
BD86-053	522505.94	4990713.11	132.0	-81/190	769.01	522491.6	4990524.0	-426.3	591.6	594.4	2.8	2.08	3.4	7.1
BD86-053*						522489.8	4990508.7	-454.5	623.7	626.5	2.8	2.12	5.1	10.8
BD86-053C*	522505.94	4990713.11	131.7	-65/190	617.22	522458.4	4990451.3	-327.5	524.2	539.3	15.1	12.8	3.3	42.2
BD86-059*	522474.53	4990789.67	132.0	-80/190	763.22	522438.0	4990588.7	-453.0	621.8	625	3.2	2.41	2.4	5.8
BD87-001*	522308.15	4990881.68	127.8	-62/190	699.82	522286.4	4990579.7	-335.5	552.9	555.1	2.2	1.83	2.2	4.0
BD87-064*	522058.97	4990604.09	130.9	-76/190	424.4	522036.5	4990531.5	-107.4	249.3	251.4	2.1	1.39	2.5	3.5
BD87-065*	522498.5584	4990479.80	128.7	-62/190	331.14	522482.1	4990334.1	-128.4	294.4	297.6	3.2	2.5	1.9	4.8
BD87-067A*	522500.25	4990489.35	128.7	-76/190	409.35	522497.1	4990374.4	-227.6	371.5	377.8	6.3	4.29	2.1	9.0
BD87-1012.5B*	522232.27	4990400.14	129.8	-45/190	98	522221.9	4990343.3	72.0	80.5	83	2.5	2.27	7.6	17.3
BD87-1025A*	522241.05	4990371.62	129.4	-50/190	79.2	522237.1	4990350.1	103.3	33	35	2	1.73	13.8	23.9
BD87-1037.5A*	522253.87	4990373.86	129.5	-45/190	123.44	522244.3	4990321.2	75.9	72.5	79	6.5	5.89	2.7	15.9
BD87-1037.5A						522242.0	4990308.4	63.0	90.2	98	7.8	7.07	1.7	12.0
BD87-1037.5A						522240.2	4990298.7	53.1	106.5	109.5	3	2.72	2.6	7.1
BD87-1037.5C*	522260.26	4990407.13	130.7	-45/196	160.02	522236.4	4990325.4	45.5	119	122	3	2.71	7.2	19.5
BD87-1062.5A*	522281.48	4990387.32	130.6	-52/190	163.82	522265.0	4990296.5	12.4	148	152	4	3.39	2	6.8
BD87-1100A	522318.32	4990387.80	133.5	-56/185	163.67	522311.6	4990319.2	32.0	120	125.5	5.5	4.45	2.3	10.2
BD87-1100A						522311.1	4990314.5	25.2	130	132	2	1.62	1.3	2.1
BD87-1100A						522310.8	4990310.9	19.8	135	140	5	4.05	2.1	8.5
BD87-1100A*						522309.8	4990301.4	5.7	152.1	157	4.9	3.97	3.3	13.1
BD87-1112.5A*	522332.25	4990383.73	133.0	-56/190	152	522319.3	4990312.5	25.6	124	135	11	8.9	2.2	19.6

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD87-1112.5A						522317.8	4990304.3	13.2	142	147	5	4.05	4.2	17.0
BD87-1125A*	522343.96	4990382.56	134.0	-56/190	152.4	522330.8	4990309.9	24.5	115.5	148.6	33.1	26.78	2.3	61.6
BD87-1137.5A	522355.99	4990380.99	133.7	-56/190	152.4	522345.3	4990322.2	45.1	105	108.7	3.7	2.99	1.3	3.9
BD87-1137.5A						522344.3	4990316.6	36.7	116	118	2	1.62	8.7	14.1
BD87-1137.5A*						522342.3	4990305.5	19.9	124	150.5	26.5	21.44	2.6	55.7
BD87-1150A	522365.93	4990378.60	133.9	-56/190	179	522354.7	4990317.0	41.1	111	113	2	1.62	1.5	2.4
BD87-1150A*						522353.2	4990308.3	28.0	115.2	140.4	25.2	20.39	2.9	59.1
BD87-1150A						522351.7	4990300.1	15.6	141.3	144	2.7	2.18	1.3	2.8
BD87-950A*	522166.71	4990388.63	130.5	-57/184	77.7	522164.6	4990361.8	89.0	48	51	3	2.39	1.2	2.9
BD87-950B*	522172.39	4990412.40	130.3	-55/190	105.15	522162.2	4990356.5	49.2	98	100	2	1.64	1.8	3.0
BD87-962.5A*	522179.02	4990380.38	130.0	-50/190	105.16	522168.2	4990321.0	58.0	88	100	12	10.39	5.1	53.0
BD87-962.5B*	522181.43	4990393.78	129.9	-51/187	100	522176.1	4990352.8	79.4	60.5	70	9.5	8.16	4.4	35.9
BD87-975A	522191.16	4990375.48	130.2	-46/190	100	522185.5	4990344.4	97.5	44	47	3	2.7	3.2	8.6
BD87-975A*						522179.7	4990312.6	64.0	91	93	2	1.8	6.2	11.2
BD87-975B	522197.20	4990409.04	130.4	-44/193	135.03	522183.8	4990350.2	72.7	80	87	7	6.41	6.3	40.4
BD87-975B						522181.5	4990340.0	62.7	97	99	2	1.83	1.5	2.7
BD87-975B*						522176.8	4990319.2	42.3	126	129	3	2.75	25.7	70.7
BD-88-12U*	522017.16	4990347.07	100.8	-29/004	65.84	522020.2	4990383.3	81.6	36.2	46	9.8	6.68	4.7	31.4
BD-88-14U*	522017.09	4990346.54	102.4	-9/003	55.47	522018.9	4990377.7	107.1	27.5	35.7	8.2	7.99	4.2	33.6
BD-88-3U*	522011.52	4990365.38	70.1	-40/002	49.99	522011.8	4990385.2	86.7	23	28.7	5.7	5.29	2.9	15.3
BD-88-4U*	522011.55	4990365.58	69.8	-31/002	45.42	522012.0	4990394.1	86.6	31.4	34.9	3.5	3.4	2.2	7.5
BD-R1*	522046.30	4990347.40	97.8	-19/013	54.86	522056.6	4990391.5	84.2	46.3	48.3	2	1.65	9.6	15.8
BD-R10	522068.65	4990341.89	75.6	-20/010	70.1	522072.9	4990365.2	68.1	23.4	26.3	2.9	2.33	2.5	5.8
BD-R10*						522076.0	4990380.8	63.4	34.5	48.5	14	11.3	1.5	17.0
BD-R11*	522067.81	4990341.86	75.4	-23/348	70.1	522060.8	4990383.2	60.4	43	46.2	3.2	2.38	4.6	10.9
BD-R12*	522044.70	4990345.59	71.3	-16/010	60.96	522052.0	4990381.2	62.4	33.7	41.2	7.5	6.38	1.7	10.8
BD-R13A*	522044.65	4990345.37	71.0	-22/010	76.2	522052.8	4990385.6	56.8	41.6	45.3	3.7	2.99	2.7	8.1
BD-R15*	522008.74	4990366.25	67.7	-21/339	50.29	522000.6	4990387.8	59.3	22.6	26.5	3.9	2.56	2	5.1
BD-R2	522046.11	4990346.06	97.6	-36/010	65.53	522048.9	4990360.6	87.4	17	19	2	1.19	8	9.5
BD-R2						522050.8	4990369.3	81.7	27.5	29.6	2.1	1.29	1.5	1.9
BD-R2*						522053.0	4990379.7	75.3	37.9	44	6.1	3.89	3	11.7
BD-R4	522068.64	4990330.74	94.4	-2/010	65.67	522072.5	4990352.3	93.6	18.6	25.3	6.7	6.21	1.9	11.8
BD-R4						522075.8	4990370.1	93.0	35	45.1	10.1	9.36	2.9	27.1
BD-R4*						522078.1	4990383.1	92.5	52.3	54.3	2	1.85	22.7	42.0
BD-R6	522122.61	4990311.48	85.7	-18/033	70.1	522131.1	4990324.4	90.7	14.3	18.3	4	3.71	1.9	7.0

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 1 Continued: Down-hole Composite Significant Intercepts, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mid-Point (NAD83 Z20)			Mineralised Interval				Composite Gold Grade (g/t Au)	Gram*Metres (True Width)
						Easting (m)	Northing (m)	RL (m)	From (m)	To (m)	Interval (m)	True Width		
BD-R6*						522135.0	4990330.5	93.0	21.6	26.2	4.6	4.29	5.5	23.6
BD-R6						522150.9	4990356.4	103.0	53.3	58.4	5.1	4.83	4.7	22.7
BD-R8*	522122.60	4990311.43	83.2	-29/029	94.49	522130.7	4990325.3	74.5	16.8	19.7	2.9	1.78	35	62.3
BD-R8						522136.1	4990334.1	69.0	27.1	32.9	5.8	3.59	8.7	31.2
BD-R9*	522121.94	4990310.34	83.2	-43/029	49.68	522136.7	4990335.8	57.2	36.4	42.2	5.8	2.53	2.8	7.1

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 2: Significant Intercepts Cross Section (equivalent to 1,100 m E Mine Grid), Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Mineralised Intersection				
						From (m)	To (m)	Interval (m)	True Width (m)	Gold Grade (g/t Au)
BD85-062	522193.2	4990522.0	131.5	-63/189	95.69	138.4	142.6	4.2	3.64	14.7
including						138.4	138.68	0.28	0.24	12.9
and						140.46	141.1	0.64	0.55	10.3
and						142.04	142.57	0.53	0.46	85.3
BD86-015	522330.5	4990439.3	132.0	-73/194	349.27	206.28	214.07	7.79	5.23	12.5
including						206.28	207.67	1.39	0.93	13.3
and						210.57	211.66	1.09	0.73	19.53
and						212.85	214.07	1.22	0.82	47.1
BD86-020	522337.4	4990486.7	130.6	-70/192	412.4	298.36	303.91	5.55	3.7	66.1
including						298.36	298.78	0.42	0.28	814
BD86-045	522347.9	4990544.3	132.5	-74/190	474.27	344.7	347.8	3.1	2.24	4.8
including						344.73	346.25	1.52	1.10	8.12
BD14-176	522328.6	4990434.8	133.5	-60.8/192.7	266	210	223	13	10.16	1.9
including						214	215	1	0.78	5.4
BD14-178	522332.9	4990459.0	132.4	-60.6/192.2	281	227	234	7	5.82	2.7
including						227	228	1	0.83	10.15
BD14-180	522337.8	4990484.0	132.4	-60.7/189.8	290	269	274	5	4.6	9.95
including						269	270	1	0.92	46.3

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

Table 3: Significant Intercepts Mill Shaft West, Old Austen Mine, Nova Scotia

Hole ID	Easting (m)	Northing (m)	RL (m)	Dip/ Azimuth degrees	Total Depth (m)	Downhole Mineralised Intersection			
						From (m)	To (m)	Interval (m)	Gold Grade (g/t Au)
BD80-010	521125.5	4990630.7	132.0	-50/192	108	No Significant Intercept			
BD80-011	521115.2	4990609.1	132.0	-51/192	178	No Significant Intercept			
CX86-001	521110.1	4990568.8	137.7	-48/182	178.74	No Significant Intercept			
CX86-002	521107.1	4990527.5	137.8	-46/192	136.25	39.78	42.69	2.91	1.65
CX86-003	521124.7	4990472.9	137.9	-55/192	159.3	38.83	42.9	4.07	19.75
including						38.83	39.04	0.21	24.00
and						42	42.5	0.5	141.60
CX86-004	521211.9	4990553.4	138.1	-55/194	121	No Significant Intercept			
CX86-005	521136.8	4990567.8	137.8	-54/192	163.36	No Significant Intercept			
CX86-006	521161.5	4990565.2	137.9	-52/193	185	No Significant Intercept			
CX86-007	521189.3	4990559.0	138.0	-54/194	163.72	No Significant Intercept			
CX86-008	521089.6	4990578.0	137.6	-50/192	157.28	No Significant Intercept			
CX86-009	521217.5	4990464.3	137.7	-54/193	109.4	No Significant Intercept			
CX86-010	521229.5	4990524.9	138.3	-45/192	152.4	No Significant Intercept			
CX86-011	521237.7	4990573.5	138.1	-46/193	94.49	No Significant Intercept			
BD06-067	521132.7	4990509.8	138.0	-45/191	151	No Significant Intercept			
BD06-069	521152.1	4990531.7	138.0	-43/193	150	46	49	3	1.11
BD06-071	521188.2	4990521.3	138.2	-45/190	131	68	73	5	4.88
including						68	69	1	18.45
BD09-153	521068.0	4990625.6	137.3	-45/190	260	175	181	6	5.78
including						176	177	1	14.35
including						178	179	1	15.25
MS-18-004	521122.0	4990687.0	134.0	-45/190	191	No Significant Intercept			
MS-19-005	521291.3	4990456.1	138.5	-46/190	110	No Significant Intercept			
MS-19-006	521228.6	4990589.5	133.4	-46/190	212	No Significant Intercept			
MS-19-007	521216.1	4990480.9	137.2	-46/190	152	No Significant Intercept			
MS-19-008	521155.0	4990614.7	134.1	-45/189	218.41	No Significant Intercept			
MS-19-009	521045.5	4990508.2	137.3	-46/190	152	No Significant Intercept			

NOTES: Assumptions include: Cut Off Grade is 1 g/t Au, Minimum width is 2 m down hole, Maximum internal dilution is 3 m. Coordinates quoted in NAD83/ UTM Zone 20N.

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Gold Mineral Resources July 2026 – 15-Mile Processing Hub Project

Deposit	Measured			Indicated			Inferred			Total			31 December 2025		
	Tonnes (Mt)	Gold (g/t)	Ounces ('000)	Tonnes (Mt)	Gold (g/t)	Ounces ('000)	Tonnes (Mt)	Gold (g/t)	Ounces ('000)	Tonnes (Mt)	Gold (g/t)	Ounces ('000)	Tonnes (Mt)	Gold (g/t)	Ounces ('000)
15-Mile Mine	-	-	-	30.2	1.2	1,190	5.5	1.1	200	**35.7**	**1.2**	**1,390**	26.5	1.0	860
Old Mitchell Mine	13.2	1.2	510	3.3	1.4	150	-	-	-	**16.5**	**1.2**	**660**	20.9	1.1	690
Old Austen Mine	4.4	1.4	190	5.2	1.4	230	0.6	1.9	40	**10.2**	**1.4**	**460**	12.0	1.2	470
Total Project	17.6	1.2	700	38.7	1.3	1,570	6.1	1.2	240	**62.4**	**1.2**	**2,510**	**59.4**	**1.1**	**2,020**

Notes

1. Cut-off Grade 0.3 g/t Au
2. Mineral Resources are reported constrained by a US$2,500/oz pit shell.
3. Rounding may result in apparent summation differences between tonnes, grade and contained metal.

Competent Persons Statement

Exploration results

The information in this report that relates to Exploration Results is based on, and fairly represents information compiled by Dr Roger Mustard, who is a Member of The Australasian Institute of Mining and Metallurgy. Dr Mustard is a full-time employee of St Barbara and has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'. Dr Mustard consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

The information in this report that relates to previously reported Mineral Resources for Old Austen is extracted from the ASX announcement entitled '*15-Mile Processing Hub Mineral Resources Estimate Increases 24% to 2.5 Moz*' dated 28 July 2026, which is available to view on the Company's website. The Company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcement and that all material assumptions and technical parameters underpinning the estimates in the relevant market announcement continue to apply and have not materially changed. The Company confirms that the form and context in which the Competent Person's findings are presented have not been materially modified from the original market announcement.

JORC Code, 2012 Edition – Table 1 Old Austen Mine

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.*	• Sampling is based on diamond drilling completed by five exploration campaigns between 1985 and 2021, totalling approximately 70 km of drilling. • Historical sampling (1985–1988) was undertaken using geological boundaries defined by lithology and quartz vein contacts, while modern drilling generally utilised continuous nominal 1 m sample intervals or geology-based intervals. • Modern drilling employed diamond-sawn half-core sampling, with limited whole-core sampling undertaken in selected programs to improve representativity in coarse gold mineralisation. • Samples were prepared by accredited commercial laboratories using industry-standard crushing and pulverisation protocols, typically to approximately 85% passing 75 µm prior to analysis. • Gold analyses were completed predominantly by Fire Assay with Atomic Absorption Spectroscopy (AAS) finish, with Screen Fire Assay routinely applied where coarse or visible gold was present, or for entire sampling programs where appropriate. • Sampling protocols, sample preparation procedures and analytical methods are considered appropriate for the Meguma-style orogenic gold mineralisation.
Drilling techniques	• *Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• Drilling is exclusively surface and underground diamond drilling completed by Seabright Resources (1985–1988), Acadian Gold Corporation (2005–2009) and Atlantic Gold (2014–2015). • Drilling comprised predominantly NQ-size diamond core, which is considered appropriate for the style and geometry of the mineralisation. • Drill core orientation was referenced to the interpreted regional cleavage fabric. The consistent orientation of the regional cleavage across the deposit provided an appropriate structural framework for orienting core and supporting structural and geological interpretation. • The drilling methods and core sizes are considered appropriate for the style of mineralisation and have provided data of sufficient quality for geological interpretation and Mineral Resource estimation.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of*	• Seabright and Acadian drilling did not routinely record quantitative core recovery; however, geological logs indicate no evidence of significant or systematic core loss. • Review of Atlantic drilling demonstrates good core recovery within mineralised intervals, with an average recovery of 93%.

Criteria	JORC Code explanation	Commentary
	fine/coarse material.	• No evidence of recovery-related sampling bias has been identified. • Core recovery is considered adequate for the style of mineralisation and supports the reliability of the geological interpretation.
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• All diamond drill core was geologically logged using standard industry procedures, recording lithology, alteration, mineralogy, quartz veining, sulphide content and structural features. • Structural measurements, including bedding, cleavage and vein orientations, were routinely collected to support geological interpretation and mineralisation modelling. • The level of geological logging is considered qualitative and quantitative in nature.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• Historical sampling was undertaken using geological boundaries, with sample intervals defined by lithological contacts, alteration and quartz vein margins, while modern drilling generally utilised continuous nominal 1 m intervals. • Core was predominantly diamond-sawn half-core, with limited whole-core sampling undertaken in selected programs to improve representativity in coarse gold mineralisation. • Samples were prepared at accredited commercial laboratories using industry-standard protocols involving drying, crushing and pulverising to approximately 85% passing 75 µm. • Gold was analysed predominantly by Fire Assay with an Atomic Absorption Spectroscopy (AAS) finish, with Screen Fire Assay routinely employed where coarse or visible gold was present to better account for the nugget effect. • Sampling, sub-sampling and sample preparation procedures are considered appropriate for the style of mineralisation.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.*	• Gold analyses were completed by accredited commercial laboratories using Fire Assay with an Atomic Absorption Spectroscopy (AAS) finish, with Screen Fire Assay routinely applied where coarse or visible gold was present or anticipated. • Sample preparation and analytical methods are considered appropriate for the coarse gold style of mineralisation and are consistent with industry best practice. • Modern drilling programs incorporated comprehensive QA/QC procedures, including the routine insertion of certified reference materials, blanks and field duplicates, with results demonstrating acceptable analytical accuracy and precision. • Historical drilling pre-dated routine QA/QC protocols; however, validation through database audits, twin-hole comparisons and subsequent infill drilling

Criteria	JORC Code explanation	Commentary
		confirms the historical assay data are reliable. • No material analytical bias has been identified.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• Historical drilling, sampling and assay data were verified through review of original assessment reports, validation of legacy digital databases and reconciliation with the current SQL database. • Multiple generations of modern infill and twin drilling demonstrate good agreement with historical drilling in terms of geology, mineralisation thickness and gold grade, providing confidence in the historical dataset. • Drilling, logging and assay data are maintained within a secure relational SQL database incorporating validation rules, audit trails and controlled user access. • No material transcription errors or analytical bias were identified during database validation, and no adjustments were applied to assay data other than assignment of half the detection limit to below-detection results. • The historical and modern datasets are considered adequately verified.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• Drill hole collars were surveyed using licensed surveyors and a combination of historical local mine grids and modern NAD83(CSRS) UTM Zone 20N survey control. • Historical local grids were validated and transformed to the modern coordinate system using surveyed control points, with transformation accuracy considered appropriate. • Down-hole surveys were completed using industry-standard methods appropriate to the period of drilling, with modern drilling utilising electronic digital survey instruments to record both dip and azimuth. • Topographic control is based on a 1 m resolution LiDAR-derived Digital Elevation Model referenced to NAD83(CSRS) and CGVD2013. • Survey control and spatial accuracy are considered appropriate.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Drill spacing is generally approximately 25 m × 25 m across the principal mineralised zones, with closer spacing around underground workings and spacing increasing progressively at depth. • The drilling density is sufficient to establish geological and grade continuity • Samples were retained at their original sampled lengths, with no compositing applied to the primary assay database. •
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Drill holes were planned to intersect the principal mineralised lodes at high angles and provide representative sampling of the mineralisation. • The range of drill hole orientations is appropriate for the lode geometries and structural controls recognised across the deposit. • No orientation-related sampling bias has been identified, and drill hole

Criteria	JORC Code explanation	Commentary
		orientations are considered appropriate to support geological interpretation. • The relationship between drill hole orientation and the interpreted geometry of the mineralisation is well understood.
Sample security	• *The measures taken to ensure sample security.*	• Drill core was transported from the drill rig to secure logging facilities where logging, sampling and core cutting were completed prior to dispatch. • Samples were placed in uniquely identified sample bags, secured and transported to independent commercial laboratories by company personnel or commercial freight carriers. • Historical sample handling and chain-of-custody procedures are consistent with industry practice, with no material sample security issues identified. • Review of historical documentation, QA/QC performance and database validation provides confidence that sample security was adequate to support the integrity of the assay database.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• Historical drilling, sampling and assay data have been reviewed against original assessment reports and validated during compilation of the current geological database. • Database audits, validation checks and twin-hole comparisons confirm the integrity and reliability of the historical and modern datasets. • Sampling, analytical and QA/QC procedures have been reviewed and are considered appropriate for the style of mineralisation. • No material issues were identified that would adversely affect the quality of the data.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The Old Austen Mine is held under five Exploration Licences owned by 15-Mile Minerals and Renewables Limited, a wholly owned subsidiary of St Barbara Limited, with all licences in good standing at the effective date of the Mineral Resource estimate. • Mineral tenure is administered by the Nova Scotia Department of Natural Resources under the Mineral Resources Act (2016). Exploration licences are renewable subject to statutory expenditure requirements. • The Mineral Resource is located on a combination of St Barbara-owned freehold land and Crown land. No material land access issues have been identified, and no private land acquisitions are currently anticipated. • An application for Mineral Lease MLE54321 has been submitted over part of the project area and was under assessment at the effective date. No material issues are known that are expected to prevent the granting of the

Criteria	JORC Code explanation	Commentary
		lease. • Certain licences are subject to Net Smelter Return (NSR) royalty agreements; however, no tenure, royalty, environmental or permitting matters are considered material to the reported Mineral Resource or ongoing exploration activities. • The Competent Person is not aware of any material legal, tenure, environmental, permitting, royalty, native title or land access issues that would materially affect the reported Mineral Resource or ongoing exploration activities.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• Gold was first discovered in the Old Austen Mine area in 1868, with early underground development and small-scale production occurring intermittently between 1871 and 1935, including shaft sinking, limited mining and installation of early processing infrastructure. • Exploration in the 1950s included trenching by the Lawrence Construction Company, returning locally high-grade surface gold assays. • Modern systematic exploration commenced in the 1970s with M.E.X. Explorations, including mapping, geophysics, geochemistry, trenching and diamond drilling, identifying multiple narrow quartz vein systems with limited continuity. • Acadia Mineral Ventures (1983) and Seabright (1985–1988) completed extensive exploration including drilling, geophysical and geochemical surveys, underground development, bulk sampling, and trial mining, supporting early resource and feasibility studies. • Westminer subsequently re-evaluated the project in the early 1990s and withdrew following reassessment of economic viability. • Between 2002 and 2013, Tempus/Acadian Gold completed airborne geophysics, drilling and updated Mineral Resource estimates. • Atlantic Gold (2014–2019) advanced modern development through updated resource and reserve models, metallurgical and geotechnical studies, permitting and mine planning. • St Barbara (2019–2026) completed further technical studies and integrated district-scale development planning, including optimisation studies incorporating Old Austen Mine and adjacent deposits.
Geology	• *Deposit type, geological setting and style of mineralisation.*	• The Old Austen Mine deposit is a Meguma-style orogenic gold deposits hosted within metasedimentary rocks of the Moose River Formation, Goldenville Group, in the Meguma Terrane of Nova Scotia. • Mineralisation is hosted within the overturned southern limb of the east-west trending Beaver Dam Anticline, where stratigraphy dips moderately to steeply north and is locally offset by late faults.

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		• Gold occurs in bedding-parallel quartz veins, disseminated within surrounding argillite and greywacke, and subordinate cross-cutting quartz veins, with mineralisation commonly associated with arsenopyrite and pyrite. • Hydrothermal alteration includes silicification, carbonatisation, chlorite, sulphidisation and albite, with metamorphic grade generally greenschist facies and locally overprinted by contact metamorphism from nearby Devonian intrusions. • The mineralised system extends approximately 1.4 km along strike and to depths exceeding 600 m, with true widths typically 15–40 m containing narrower high-grade quartz vein sets.

Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:*
	  ○ *easting and northing of the drill hole collar*
	  ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar*
	  ○ *dip and azimuth of the hole*
	  ○ *down-hole length and interception depth*
	  ○ *hole length.*
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*
		• A tabulation of all material drill hole data – including collar coordinates, elevation, dip, azimuth and hole depth – is provided in Tables 1 to 3 in this announcement. Drill hole spacing, distribution and data density, are described under the 'Data Spacing and Distribution' criterion.

Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Down-hole Composite Significant Intercepts are reported as length weighted averages using a cut-off of 1.0 g/t Au and minimum width of 2 m. Such intercepts may include material below cut-off but no more than three sequential metres of such material and except where the average drops below the cut-off. • No top-cutting has been applied.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down-hole lengths are reported, there should be a clear statement to this effect (eg 'down-hole length, true width not known').*	• The orientation of the mineralised structures is well understood for Old Austen Mine and drilling has been designed to intersect these structures as close to perpendicular as possible. Both down-hole lengths and calculated true widths – along with average grade, gram-metres and intercept mid-points - are detailed for Old Austen drill holes in Table 2 contained in this release. • True width for Old Austen has been calculated assuming mineralisation dips at 70° to the north • For drilling at the Mill Shaft West Prospect down-hole length reported as there is low confidence in the orientation of the mineralisation.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and*	• Appropriate plans and sections with scales and headings are included in the body of this release. • The cross section is a conventional cross section constructed perpendicular

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	appropriate sectional views.	to strike using the local mine grid. It is presented in NAT grid coordinates for consistency with the other figures.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• The long-section view is a projected longitudinal section and is balanced and representative of the currently modelled Old Austen mineralised structure. Significant historical intersections relevant to this specific geological model are displayed. Historical intersections from parallel structures, unmodelled footwall/hanging wall zones, or isolated anomalies have been omitted from this specific diagram to maintain geological clarity and avoid misrepresentation of the target lode. Full details of all historical drilling are provided in Table 2 contained in the release.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• No other substantive exploration data or geological observations have been collected or are considered material to this release. All available historical drilling data relevant to the Old Austen prospect has been reviewed and reported in a balanced manner within this announcement.
Further work	• *The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).* • *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Details of the planned further work program are outlined in the body of this release. Future activities at Old Austen may include diamond drilling and a comprehensive review of the structural geology.