

ASX RELEASE | 10 June 2026

OUTSTANDING K9 TRENCHING RESULTS HIGHLIGHT BREAKOUT POLYMETALLIC POTENTIAL AT UIS PROJECT, NAMIBIA



HIGHLIGHTS

- **100%-owned Uis Project sits next to the operating Uis Tin Mine**, placing Askari in the heart of a proven, globally significant tin-lithium-tantalum district.
- **Phase 1 trenching at K9 confirms a continuous, high-grade polymetallic system**, with standout results including:
 - o 4050 ppm Tin (Sn)
 - o 0.29% Lithium Oxide (Li₂O)
 - o 215 ppm Tantalum (Ta)
 - o 2380 ppm Rubidium (Rb)
 - o 479 ppm Caesium (Cs)
- **Systematic ~40m-spaced trenching has delivered a strong targeting dataset**, materially de-risking drill planning and future resource definition.
- **K9 is emerging as a substantial mineralised system**, extending over **950m of strike** with typical widths of **4m to 6m**.
- **Previous work at K9 also delivered high-grade surface results**, including up to 0.27% SnO₂, 216ppm Ta₂O₅ and 0.49% Rb₂O, reinforcing the scale and tenor of the target.
- **Results validate historical exploration and significantly boost drill confidence**, with RC drilling planned for H2 2026.
- **Historic RC drilling has already returned high-grade hits**, including **4m @ 0.16% SnO₂** (incl. 1m @ 0.26%), **4m @ 314 ppm Ta₂O₅** (incl. 1m @ 695 ppm), and **2m @ 0.30% Rb** (incl. 1m @ 0.38%).
- **More near-term newsflow is pending**, with the Company focused on resource definition drilling in H2 2026.
- **The Uis Project is rapidly emerging as a compelling polymetallic critical minerals opportunity**, with exposure to **Tin, Lithium, Tantalum, Rubidium and Caesium** in a proven mining district just **<230km** by sealed road from the Walvis Bay Deepwater Port.



Askari Metals Limited (**ASX: AS2**) ("Askari Metals" or the "Company") is pleased to report outstanding Phase I trenching assay results from the K9 Pegmatite Target at its 100%-owned Uis Project in Namibia, further underscoring the project's breakout polymetallic potential. The results confirm extensive mineralisation across tin, lithium, tantalum, rubidium and caesium, strengthening confidence in K9 as a high-priority drill target within a rapidly emerging critical minerals district.

Strategically located on EPL 7345, Askari's Uis Project sits immediately southwest of the operating Uis Tin Mine, placing the Company in the heart of one of the world's premier hard-rock tin-lithium-tantalum districts. The neighbouring Uis Mine hosts a substantial JORC (2012) Mineral Resource Estimate of 77.51Mt @ 0.79% Li₂O, 0.15% Sn and 82 ppm Ta*, highlighting the scale, fertility and proven endowment of the mineralised corridor and reinforcing the significant discovery upside emerging across Askari's ground.

The K9 Target sits directly along strike from the B1 / C1 pegmatite targets on the adjacent ML129, previously owned by Andrada Mining Ltd (*now Uis Small Miners Association*), underscoring its strategic position within a highly prospective and already mineralised corridor. Importantly, previous drilling completed by Andrada in 2023 returned standout pegmatite intersections, including drill hole B1_01, which intersected 14.52m from 15.48m to 30m grading 1.38% Li₂O, 285 ppm tantalum and 0.131% tin, with higher-grade lithium zones of 5m @ 2.32% Li₂O from 18m and 2.5m @ 2.04% Li₂O from 25.5m to 28m. Additional strong results included 12.78m @ 0.74% Li₂O, 181 ppm tantalum and 0.052% tin in B1_09, and 11.06m @ 0.81% Li₂O, 1101 ppm tantalum and 0.033% tin in C1_04.

(refer to: polaris.brighterir.com/public/andrada_mining/news/rns/story/x5vyg8w for further information).

For investors, this nearby drilling provides a compelling analogue and materially strengthens the view that K9 is emerging within the same fertile pegmatite trend capable of delivering meaningful polymetallic scale and grade. These results further highlight K9's growing polymetallic potential, with planned RC and Diamond drilling in H2 2026 set to test the scale, continuity and broader discovery upside of the system.

Exploration across EPL 7345 has already highlighted the scale and quality of the opportunity, with historical mapping, rock chip sampling and two phases of RC drilling returning encouraging tin, tantalum, lithium and rubidium results. Across the licence, four key pegmatite targets – OP, PS, DP and K9 – have been identified and advanced through detailed exploration, while additional mapped pegmatite zones remain untested and provide further upside as the Company continues to build momentum across the broader Uis Project.

Commenting on the assay results from the K9 Target, Executive Director, Mr. Gino D'Anna, stated:

"K9 is shaping up as a standout polymetallic discovery at Uis. Phase I trenching has confirmed broad, continuous mineralisation over a 950m strike, with standout results including up to 4,050ppm tin, 0.29% Li₂O, 215ppm tantalum, 2,380ppm rubidium and 479ppm caesium. These results materially de-risk drilling and strengthen our conviction that K9 sits within a fertile, high-quality mineralised corridor with the scale and commodity mix to capture strong investor attention. With drilling planned for H2 2026 and more results still to come, we see strong potential for continued newsflow as we unlock the broader upside at Uis. In a strong tin and critical minerals market, we believe Uis is increasingly well positioned to deliver meaningful value as exploration momentum builds."

* For further information, refer to: [Uis - Andrada Mining - Lithium Mine - Namibia](https://polaris.brighterir.com/public/andrada_mining/news/rns/story/x5vyg8w)



Details of Phase I Trenching Campaign

The Phase I trenching program was designed to systematically test four high-priority pegmatite targets – OP, PS, DP and K9 – within a defined corridor of interest on EPL 7345 at the Uis Project in Namibia. These pegmatites display key characteristics of fertile LCT systems, including strong fractionation and zonation, along with lithium-associated minerals such as sugary and cleavelandite albite, coloured tourmaline and green mica.

A total of 135 trenches for 7,269m were completed, generating 2,098 channel samples. Trenching was carried out on a systematic 40m spacing across DP, PS and K9, while the OP target was initially tested at 80m spacing before being infilled to 40m to improve targeting confidence and geological resolution.

Importantly, three of the four high-priority pegmatite targets had seen only limited historical sampling, while K9 had never previously been sampled or drill tested. This underscores the significance of the Phase I dataset, which has materially advanced target definition and strengthened the foundation for follow-up drilling.

Detailed mapping and channel sampling from the trenches will provide critical information on surface extent, geometry and mineralisation potential across the pegmatite corridor. This dataset will directly inform follow-up infill trenching, RC drilling and potential diamond drilling as the Company advances its next phase of exploration at Uis. **RC drilling is planned to recommence at the Uis Project in H2 2026.**

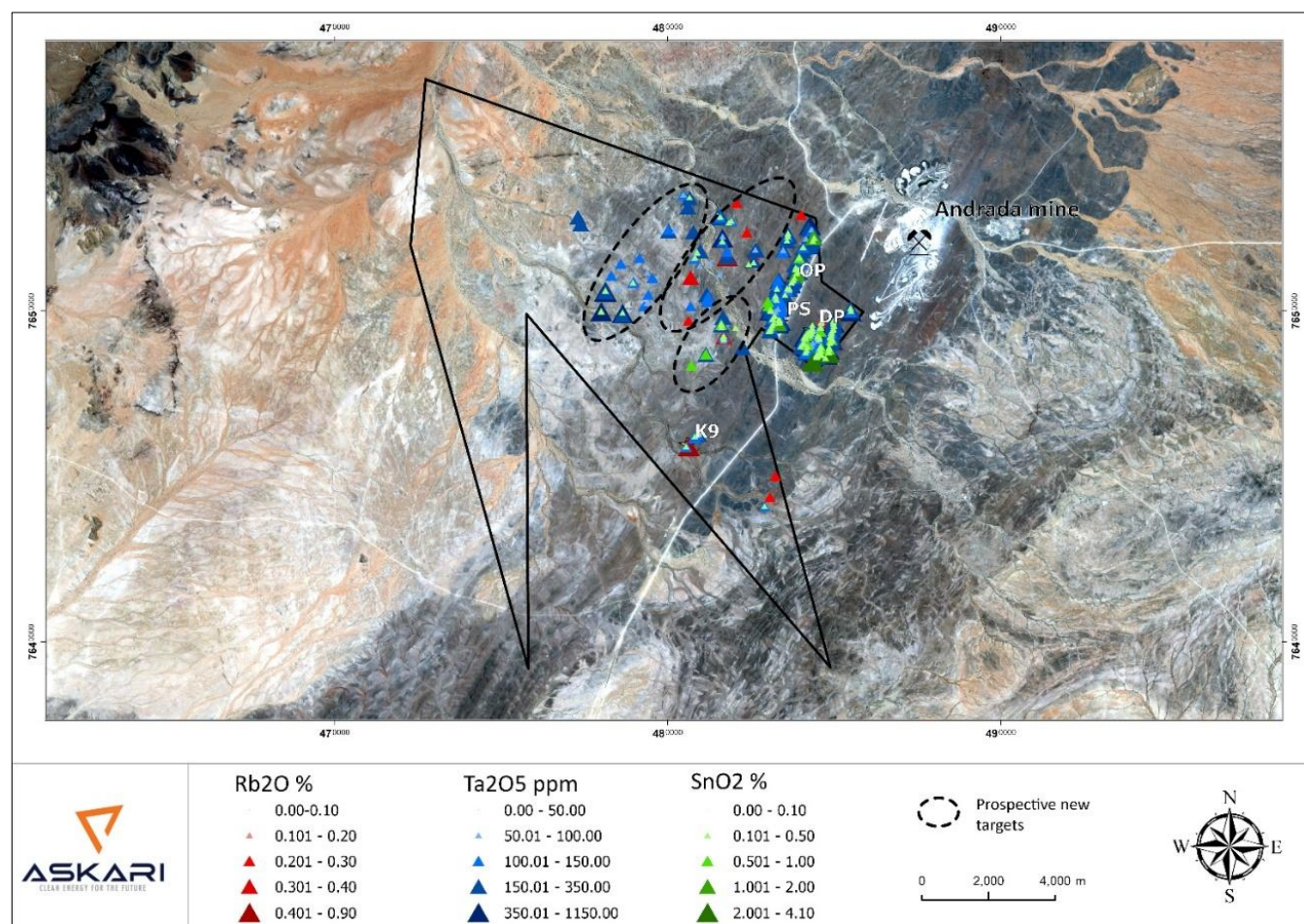


Figure 1: Map showing the interpreted corridor of interest on EPL 7345 along with pegmatite targets (DP, OP, PS and K9) trenched in the Phase 1 Trenching programme.

K9 Pegmatite Trenching

Trenching at the K9 Pegmatite Target was completed on a systematic grid designed to achieve approximately 40m spacing across most of the 950m strike length. The program was designed to test mineralisation both along strike and across the pegmatite, providing a strong foundation for geological interpretation and drill targeting.

A total of 38 trenches for 781.7m were completed at K9, generating 199 channel samples ranging from 0.3m to 1.9m in length for laboratory analysis. The program builds on earlier reconnaissance work, including mapping and surface sampling, and represents the first systematic test of the target.

Previous field work at the K9 Target returned high-grade surface values of up to **0.27% SnO₂**, **216ppm Ta₂O₅** and **0.49% Rb₂O**. These earlier results provided a strong indication of the target's polymetallic potential, which has now been materially strengthened by the Phase I trenching program.

The K9 trenching results have significantly improved geological understanding of the pegmatite system, defining its strike extent, width and polymetallic tenor with far greater confidence. The scale and continuity now outlined by trenching strongly supports planned follow-up drilling.

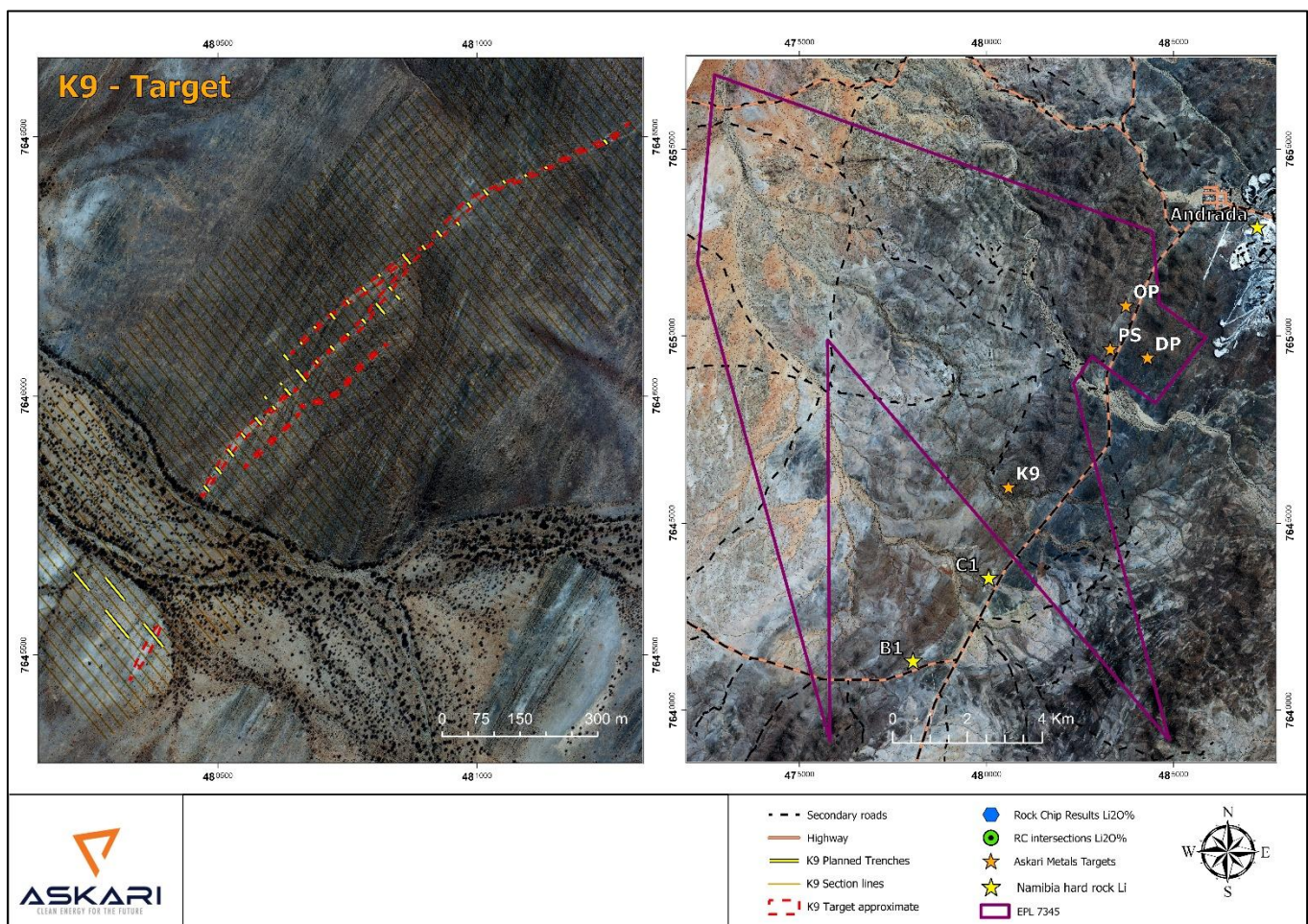


Figure 2: Map of the K9 pegmatite target including the location of the trench lines completed.

The image below demonstrates a surface outcrop of weathered spodumene mineralisation identified at the K9 Target.



Image 1: Pegmatite outcrop at the K9 Target exhibiting weathered spodumene mineralisation. Please note that visual estimates are not a proxy for laboratory results and assay information. No reliance should be placed on visual

The image below demonstrates the trenching and channel sampling methods used at the K9 Target are shown below.



Image 2: Example of the trenching completed at the K9 Target. Trenches are dug using a mechanised excavator to the point of refusal. The trenches are then cleaned manually and mapped by a geologist to document the exposed geology across the width of the pegmatite target and document the host lithology. Visual indicator marks are made across the pegmatite for channel sampling to be completed using a rock saw and hand chisel to remove the sample for bagging and sample preparation. Channel sampling is completed using a rock saw and hand chisel to remove the sample for bagging and sample preparation.



Multiple trenches intersected significant lithium, tin, tantalum, rubidium and caesium mineralisation across the K9 dyke system, which now extends for approximately 950m of strike. In several areas, the mineralisation tenor compares favourably with nearby known deposits, reinforcing K9's growing potential as a meaningful polymetallic target.

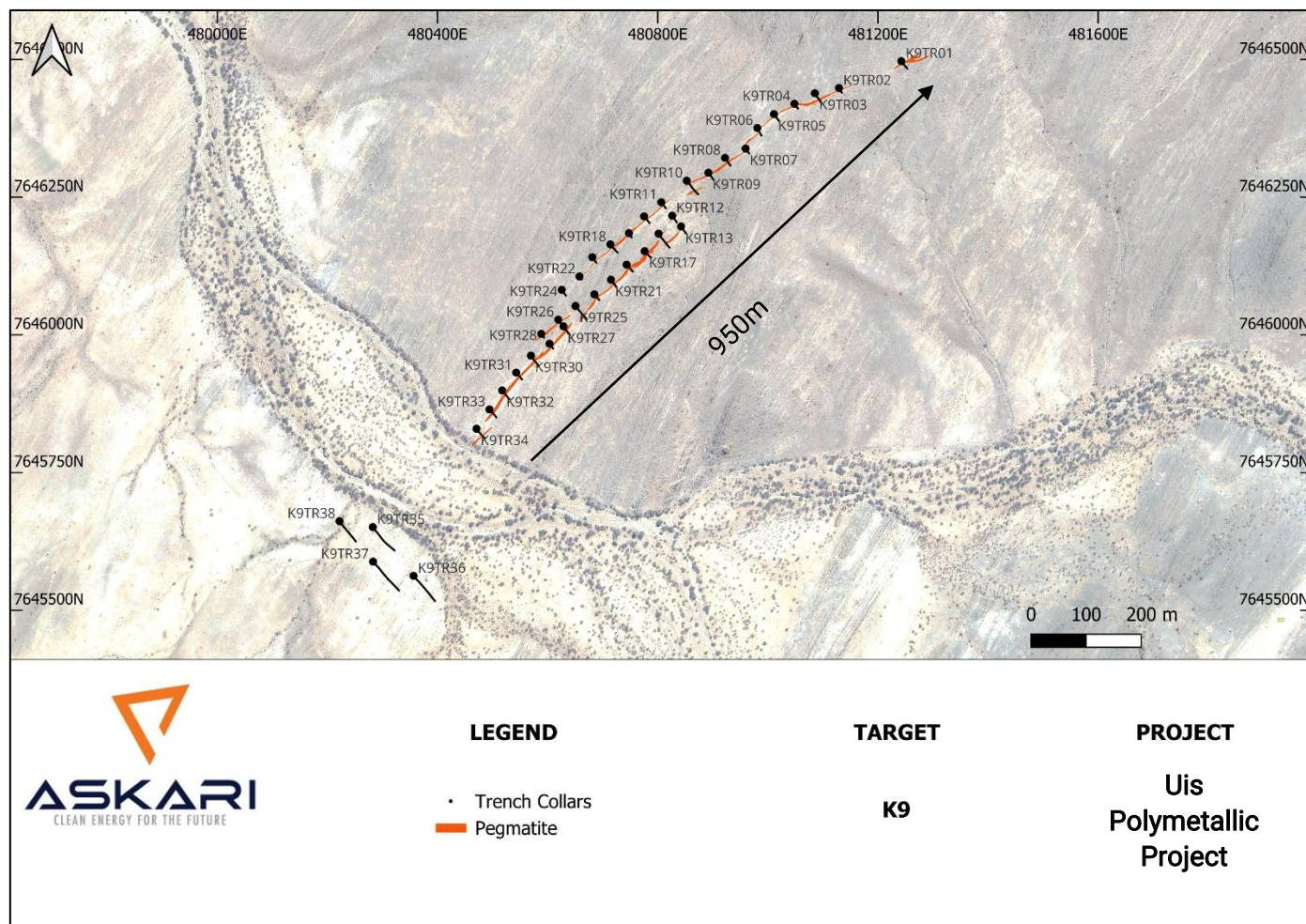


Figure 3: Map shows K9 trenches, pegmatites and their spatial nature of outcrop.

Discussion of Results

K9 trenching has confirmed broad polymetallic mineralisation across the pegmatite system, with encouraging tin, lithium, tantalum, rubidium and caesium results returned from multiple positions along strike. The consistency of mineralisation across the 950m target materially strengthens the Company's confidence in K9 as a high-priority drill target within the broader Uis Project.

Tin Results

Figure 4 highlights some of the strongest tin intercepts returned from K9, demonstrating multiple zones of continuous mineralisation along the 950m pegmatite trend.

These tin results increase confidence in the scale and continuity of mineralisation at K9 and support ongoing follow-up work, particularly given the target's position within the highly prospective B1/C1 corridor being explored at the neighbouring Uis Tin Mine.

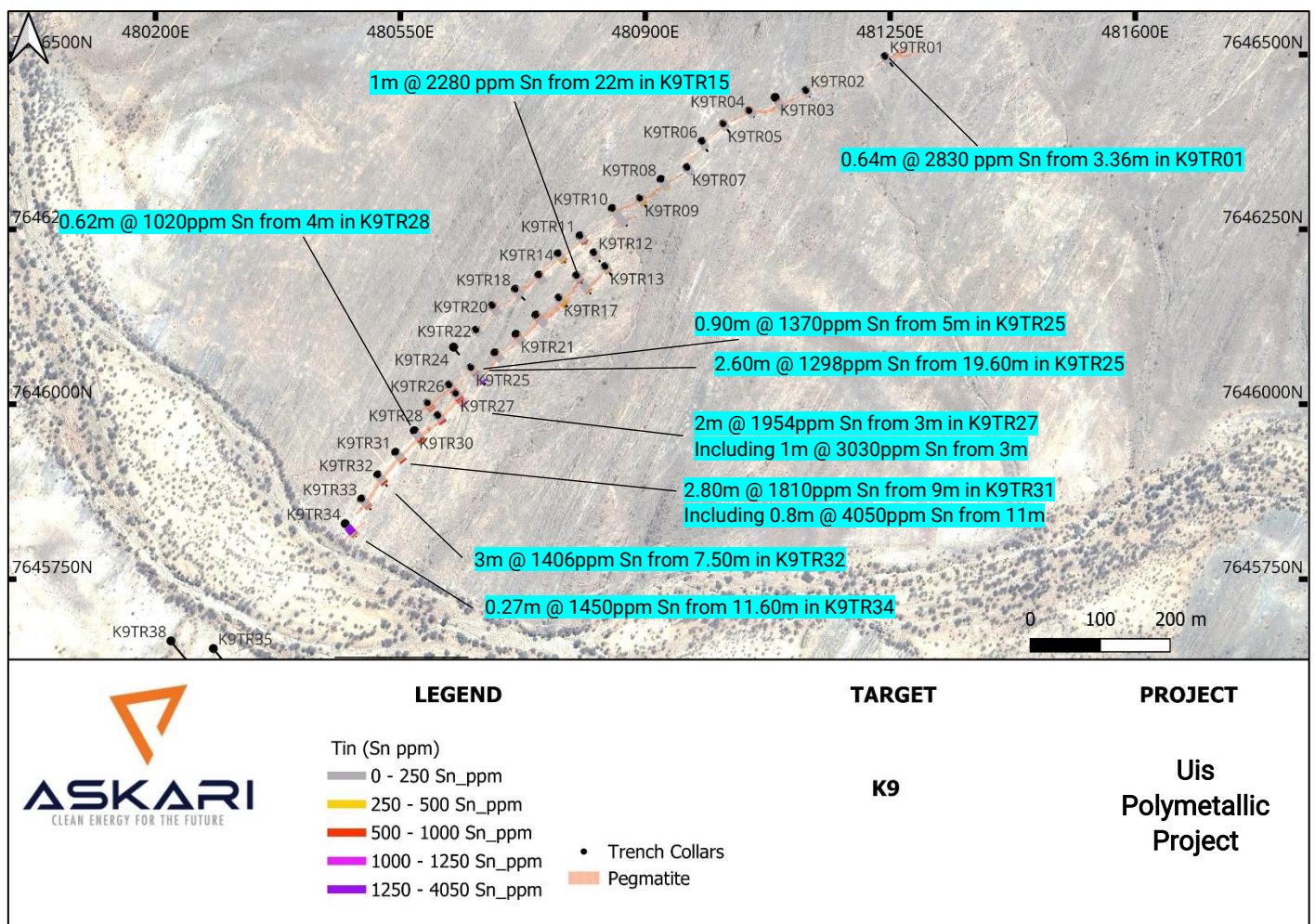


Figure 4: Tin (Sn) mineralisation intercepts from Phase1 K9 trenches with some highlights of high-grade tin exceeding 0.1% Sn.

Highlights of high-grade tin intercepts exceeding 0.1% Sn along much of the pegmatite strike length (Table 1) are indicative of K9's strong tin prospectivity and compare favourably with the nearby V1/V2 deposit at the Uis Tin Mine (Andrada Mining Ltd), which reports an average grade of 0.15% Sn.

A summary of the best tin intercepts is presented in **Table 1** below.

Table 1: A summary of the best Tin (Sn) intercepts from K9 pegmatite prepared using a cut-off grade of 0.05% Sn (500ppm Sn) based on historic cut-off grade for the adjacent Uis Tin Mine.

Trench ID	Best Tin (Sn_ppm) intercepts	Trench ID	Best Tin (Sn_ppm) intercepts
K9TR01	0.64m @ 2830 ppm Sn from 3.36m	K9TR20	1.05m @ 616ppm Sn from 8.25m
K9TR03	0.98m @ 680ppm Sn from 11.92m	K9TR23	2.40m @ 824ppm Sn from 6.10m
K9TR04	1.86m @ 571ppm Sn from 2.30m	K9TR25	0.30m @ 707ppm Sn from 4.20m
K9TR05	0.98m @ 680ppm Sn from 11.92m	K9TR25	0.90m @ 1370ppm Sn from 5m
K9TR09	1m @ 556ppm Sn from 3m	K9TR25	2.60m @ 1298ppm Sn from 19.60m
K9TR10	0.90m @ 595ppm Sn from 6.10m	K9TR26	2.32m @ 690ppm Sn from 3.40m
K9TR11	1.80m @ 778ppm Sn from 5.18m	K9TR27	2m @ 1954ppm Sn from 3m; including 1m @ 3030ppm Sn from 3m
K9TR13	0.84m @ 767ppm Sn from 3.30m	K9TR27	1.80m @ 694ppm Sn from 6m 1.98m @ 884ppm Sn from 11.9m; including 1.1m @ 1040 ppm Sn from 11.9m 0.58m @ 577ppm Sn from 14.32m
K9TR14	1.34m @ 890ppm Sn from 7m	K9TR28	1.06m @ 700ppm Sn from 1.54m
K9TR15	1.48m @ 533ppm Sn from 3.70m	K9TR28	0.62m @ 1020ppm Sn from 4m
K9TR15	1m @ 2280 ppm Sn from 22m	K9TR28	1.04m @ 766ppm Sn from 5.66m
K9TR16	2m @ 848 ppm Sn from 5.60m	K9TR29	3.70m @ 859ppm Sn from 3.90m
K9TR17	1m @ 592ppm Sn from 4.35m	K9TR30	3.90m @ 708ppm Sn from 8.90m
K9TR17	0.95m @ 530ppm Sn from 7.35m	K9TR30	0.70m @ 775ppm Sn from 16.00m
K9TR18	1.04m @ 565ppm Sn from 4.80m	K9TR31	2.80m @ 1810ppm Sn from 9m; including 0.8m @ 4050ppm Sn from 11m
K9TR19	2.40m @ 675ppm Sn from 7m	K9TR32	3m @ 1406ppm Sn from 7.50m
K9TR19	0.46m @ 529ppm Sn from 13.40m	K9TR33	1.15m @ 542ppm Sn from 7m 0.9m @ 1250ppm Sn from 10m
K9TR20	0.70m @ 657ppm Sn from 2.50m	K9TR34	0.27m @ 1450ppm Sn from 11.60m
K9TR21	1.1m @ 811ppm Sn from 7.5m 1.4m @ 816ppm Sn from 9.4m	K9TR34	1.44m @ 932ppm Sn from 14.56m

Lithium Results

Several trenches returned lithium assays in the 0.2% to 0.3% Li₂O range, reinforcing K9's lithium prospectivity and highlighting the potential for stronger grades at depth within fresher pegmatite.

The K9 pegmatites show surface evidence of spodumene weathering to albite and mica, suggesting near-surface lithium grades may be subdued by weathering and leaching. As a result, the Company



believes fresh-rock drilling has the potential to return stronger lithium mineralisation than is currently visible at surface, consistent with weathered pegmatite systems elsewhere in the Uis district.

These trench results strengthen confidence that follow-up drilling into fresh rock could deliver an uplift in lithium grades by testing below the weathered surface profile.

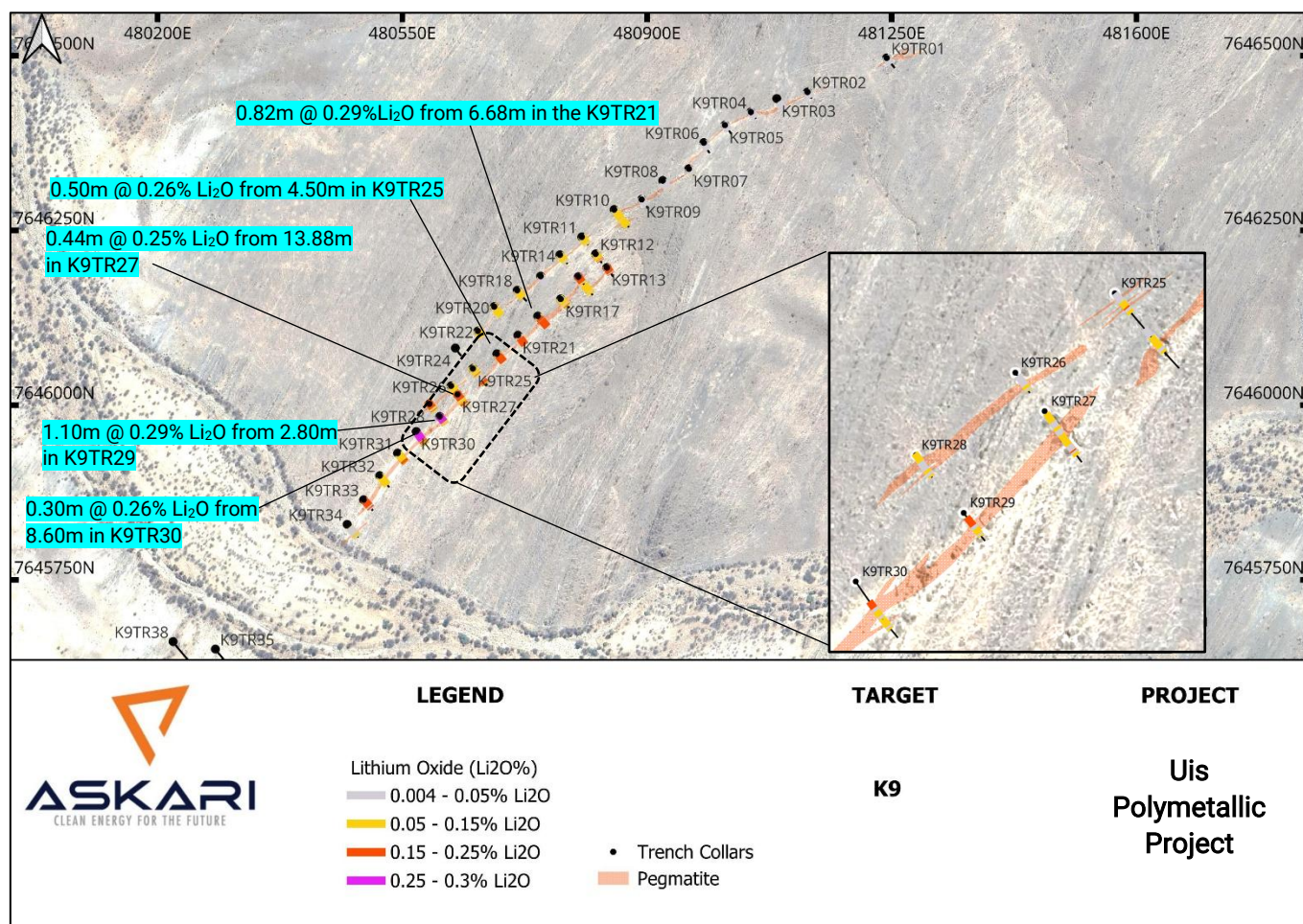


Figure 5: Lithium ($\text{Li}_2\text{O}\%$) results, with intercepts of 0.3% Li_2O labelled on the map.

A summary of intercepts using a 0.25% Li_2O are presented in the table below.

Table 2: Summary table of best Lithium oxide intercepts tabulated using a 0.25% Li_2O cut-off grade for spodumene pegmatites.

Trench ID	Best Lithium ($\text{Li}_2\text{O}\%$) intercepts	Trench ID	Best Lithium ($\text{Li}_2\text{O}\%$) intercepts
K9TR21	0.82m @ 0.29% Li_2O from 6.68m	K9TR29	1.10m @ 0.29% Li_2O from 2.80m
K9TR25	0.50m @ 0.26% Li_2O from 4.50m	K9TR30	0.30m @ 0.26% Li_2O from 8.60m
K9TR27	0.44m @ 0.25% Li_2O from 13.88m		

Tantalum Results

K9 trenching returned strong and broadly continuous tantalum mineralisation, with many intercepts exceeding 80ppm Ta along the full 950m strike length of the pegmatite. Peak results of up to 215ppm Ta highlight K9 as a compelling tantalum target within the broader polymetallic system.

These tantalum grades compare favourably with the neighbouring Uis Tin Mine, which reports average tantalum grades of 82ppm Ta and resource grades of 90ppm Ta (Measured), 86ppm Ta (Indicated) and 73ppm Ta (Inferred)*, highlighting the strength of the K9 results in a proven mineralised district.

Importantly, the higher-grade zones identified within EPL 7345 continue to reinforce the Uis Project's polymetallic opportunity across tin, tantalum, rubidium and lithium.

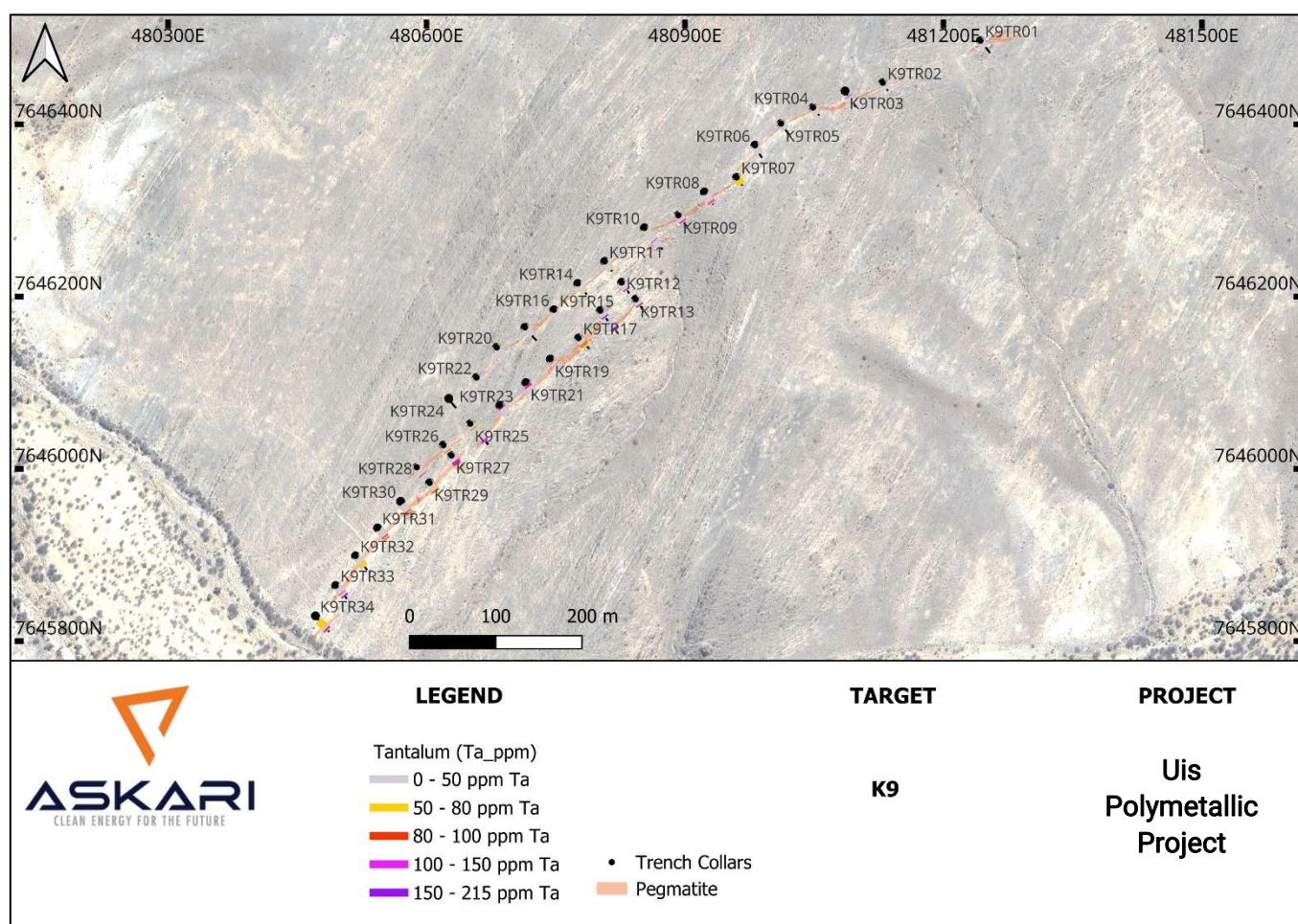


Figure 6: Tantalum (ppm Ta) results are the most consistent with at least an intercept of above 80ppm Ta in a significant number of trenches along the entire length of the pegmatite.

A summary of the best tantalum intercepts is presented in **Table 3** below.

Table 3: Summary of the best Tantalum (Ta) intercepts from K9 pegmatite prepared using a cut-off grade of 80ppm Ta, a value comparable to the V1/V2 deposit which has an average resource grade of 82ppm Ta.

Trench ID	Best Tantalum (Ta_ppm) intercepts	Trench ID	Best Tantalum (Ta_ppm) intercepts
K9TR03	0.98m @ 110ppm Ta from 11.92m	K9TR23	2.40m @ 121ppm Ta from 6.10m
K9TR04	1.86m @ 102ppm Ta from 2.30	K9TR23	0.30m @ 92ppm Ta from 8.80m
K9TR05	0.98m @ 119ppm Ta from 2.06m	K9TR25	0.65m @ 94ppm Ta from 1.70m
K9TR08	1.22m @ 94ppm Ta from 8.10m	K9TR25	2.60m @ 111ppm Ta from 19.60m
K9TR08	0.78m @ 117ppm Ta from 9.92m	K9TR26	0.60m @ 95ppm Ta from 3.40m
K9TR09	1.88m @ 146ppm Ta from 3m	K9TR27	4.80m @ 118ppm Ta from 3.0m
K9TR10	1.04 @ 115ppm Ta from 23.70m	K9TR27	1.10m @ 122ppm Ta from 11.90m
K9TR12	1.65m @ 113ppm Ta from 4.26m	K9TR28	1.04m @ 95ppm Ta from 5.66m
K9TR13	1.44m @ 124ppm Ta from 2.70m	K9TR29	1.60m @ 106ppm Ta from 6.00m
K9TR15	1.48m @ 188ppm Ta from 3.70m	K9TR30	1.10m @ 95ppm Ta from 8.90m
K9TR15	3.26m @ 131ppm Ta from 20.74m	K9TR30	0.80m @ 97ppm Ta from 12m
K9TR17	0.95m @ 95ppm Ta from 3.40m	K9TR30	0.70m @ 145ppm Ta from 16m
K9TR17	1m @ 98ppm Ta from 5.35m	K9TR31	1.50m @ 104ppm Ta from 7.50m
K9TR19	0.78m @ 119ppm Ta from 6.22m	K9TR31	0.80m @ 87ppm Ta from 11m
K9TR19	0.40m @ 97ppm Ta from 9m	K9TR33	0.85m @ 83ppm Ta from 6.15m
K9TR19	0.46m @ 142ppm Ta from 13.40	K9TR33	2m @ 131ppm Ta from 10m
K9TR21	3.30m @ 115ppm Ta from 7.50m	K9TR34	2.31m @ 114ppm Ta from 14.56m



Rubidium Results

Trenching at K9 has also defined broad zones of rubidium mineralisation, with many intervals averaging around 0.1% Rb_2O and peak results of up to 0.23% Rb_2O in individual intervals.

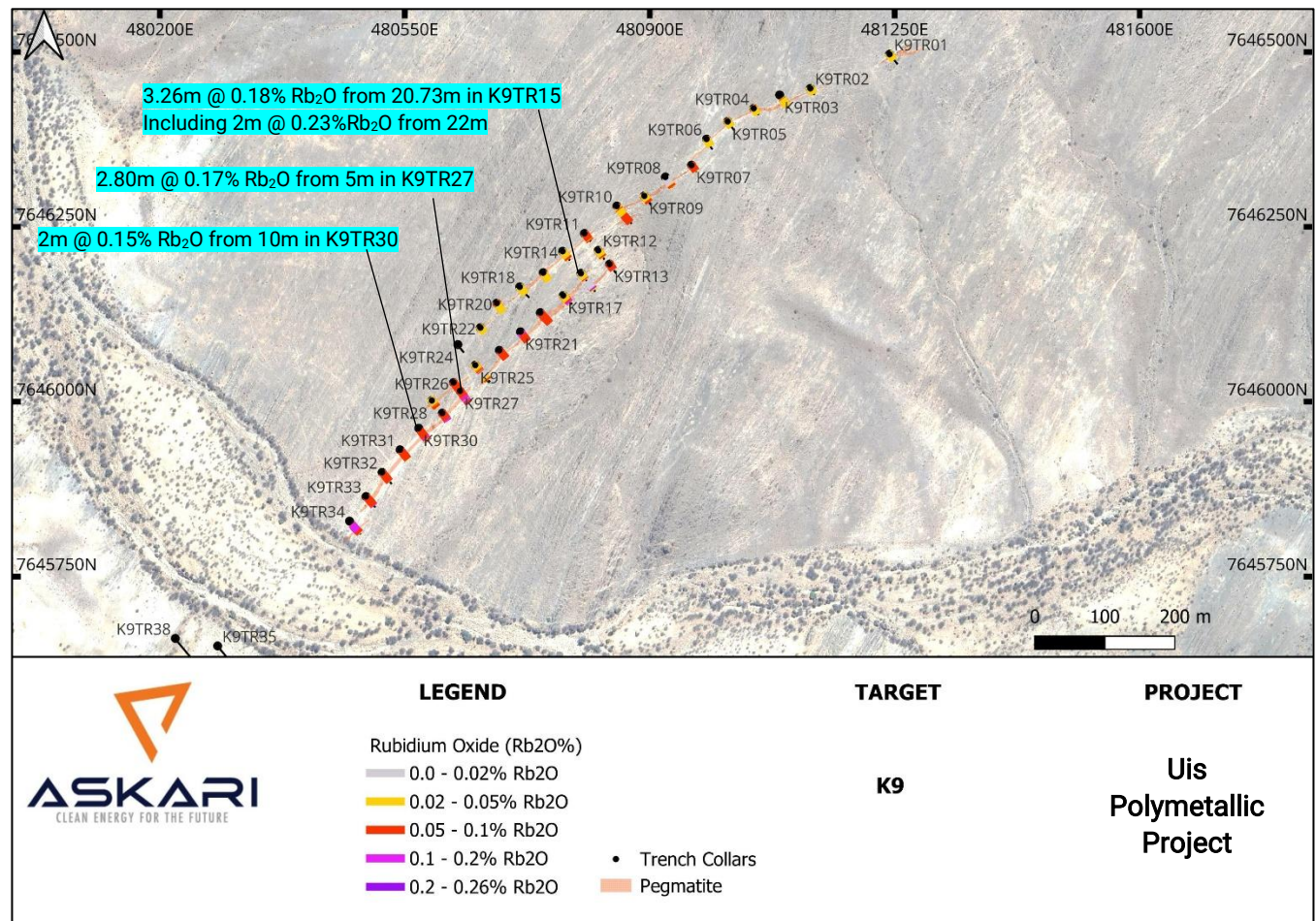


Figure 7: Rubidium Oxide ($\text{Rb}_2\text{O}\%$) results map, with intercepts that are above 0.15% Rb_2O labelled. Highlighted in the map are intercepts with assays comparable to Mt Edon Critical Mineral Project in Western Australia.

Rubidium values above 0.10% Rb_2O compare favourably with grades reported from the Mt Edon Critical Mineral Project in Western Australia, being developed by Everest Metals Corporation (ASX: EMC), which hosts an inferred resource of 3.6Mt grading 0.22% Rb_2O and 0.07% Li_2O at a 0.10% Rb_2O cut-off*.

Rubidium is widely used in biomedical research, electronics and defence applications. Rubidium is also among the key ingredients in pyrotechnics and specialty glass. According to the US Geological Survey, there was no published global production of Rubidium in 2024, though some was likely produced in China.

The US imports all its Rubidium, though its consumption is estimated at less than 2000 kilograms per year. However, Rubidium is listed as a critical mineral by the US, Japan and New Zealand.

* For further information, refer to: [MT EDON CRITICAL MINERAL PROJECT – Everest Metals Corporation](#)



A summary of the best rubidium intercepts is presented in **Table 4** below.

Table 4: A summary of the best Rubidium (Rb_2O) intercepts from K9 pegmatite prepared using a cut-off grade of 0.1% Rb_2O , a value comparable to Everest Metals' Mt Edon Critical Mineral Project in Western Australia.

Trench ID	Best Rubidium (Rb_2O %) intercepts	Trench ID	Best Rubidium (Rb_2O %) intercepts
K9TR13	0.84m @ 0.11% Rb_2O from 3.30m	K9TR25	0.50m @ 0.12% Rb_2O from 4.50m
K9TR14	1m @ 0.14% Rb_2O from 7m	K9TR27	1m @ 0.12% Rb_2O from 3m
K9TR15	0.80m @ 0.11% Rb_2O from 3.70m	K9TR27	2.80m @ 0.17% Rb_2O from 5m
K9TR15	3.26m @ 0.18% Rb_2O from 20.73m; including 2m @ 0.23% Rb_2O from 22m	K9TR27	0.90m @ 0.11% Rb_2O from 11m
K9TR17	2.95m @ 0.13% Rb_2O from 5.35m	K9TR27	0.44m @ 0.13% Rb_2O from 13.88m
K9TR19	1m @ 0.11% Rb_2O from 7m	K9TR29	2.60m @ 0.11% Rb_2O from 5m
K9TR21	4.12m @ 0.11% Rb_2O from 6.68m	K9TR30	2m @ 0.15% Rb_2O from 10m
K9TR23	0.30m @ 0.10% Rb_2O from 8.50m	K9TR30	0.70m @ 0.11% Rb_2O from 16m
K9TR33	1.10m @ 0.13% Rb_2O from 10.90m	K9TR34	0.27m @ 0.10% Rb_2O from 11.60m
		K9TR34	0.87m @ 0.11% Rb_2O from 16m

The chemical and physical properties of Rubidium are similar to Caesium (see results below) meaning that the two elements are often used together or interchangeably in many uses.

Caesium Results

K9 pegmatites carry encouraging concentrations of Caesium, a highly sought-after metal used in numerous applications such as drilling fluids, electronics and optics, catalyst, medical and industrial applications.

Encouraging Caesium mineralisation, with the best intercept grades ranging from over 100ppm Cs to 479ppm. Though these values are relatively low compared to most widely used cutoff grade of 1% Cs_2O , the Company is encouraged by the results, considering that surface weathering may have reduced the Caesium grade compared to fresh pegmatite material.

The Cape Cross-Uis pegmatites to which the K9 pegmatites belong tend to be weathered on or near surface, causing leaching of certain important Caesium-rich minerals such as pollucite, which lowers the surface concentration in pegmatites. It is, therefore, expected that Caesium values will increase in the fresh rock intersected during planned drilling to occur in H2 of 2026.

The polymetallic nature of these pegmatites adds value for the Company as each commodity (Li, Sn, Ta, Rb and Cs) has strong prospectivity potential on the Uis Project.

Caesium demand is expected to grow modestly, driven by advances in quantum computing, optical communications, perovskite solar cells, and the continued need for high-precision timing and reliable energy exploration tools.



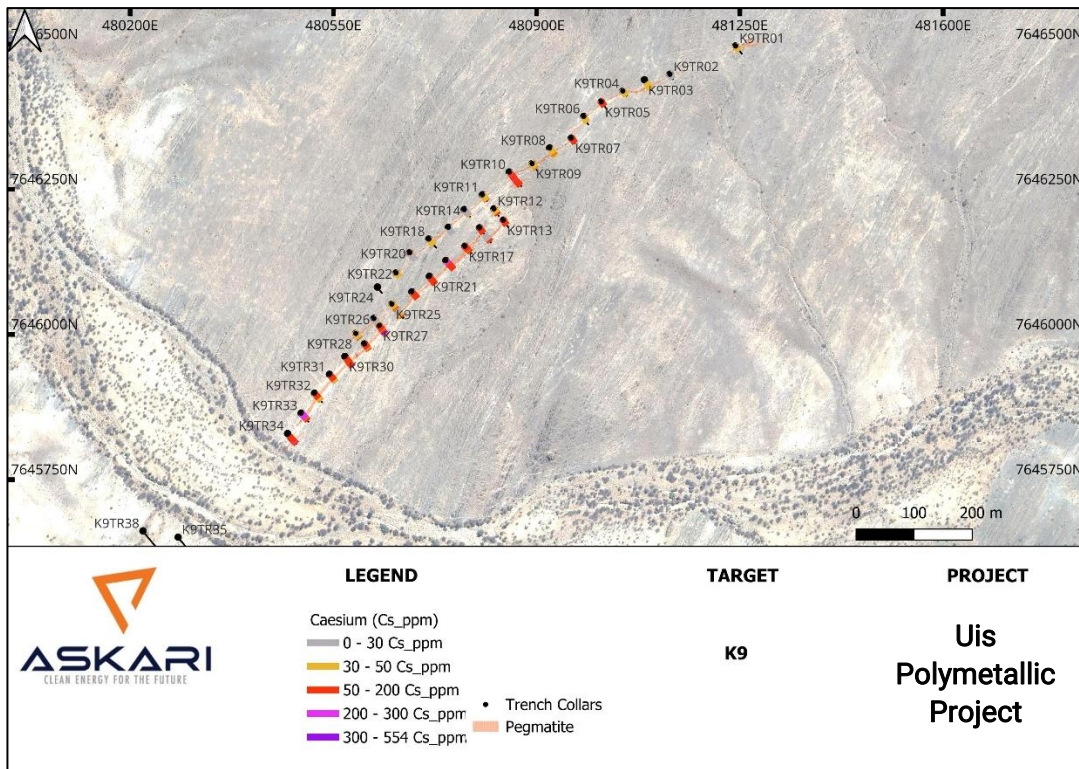


Figure 8: Caesium (ppm Cs) results shown across all trenches along the entire length of the pegmatite at the K9 Target.

Table 5: A summary of anomalous Caesium, (Cs_ppm) intercepts from K9 pegmatite prepared whilst fully aware of the globally accepted higher cut-off grade of 1% Cs₂O, and a sound understanding of the weathered nature of the surface geology of the K9 pegmatites.

Trench ID	Best Caesium (Cs ₂ O_ppm) intercepts	Trench ID	Best Caesium (Cs ₂ O_ppm) intercepts
K9TR07	1.30m @ 172ppm Cs ₂ O from 3m	K9TR25	0.50m @ 120ppm Cs ₂ O from 4.50m
K9TR07	0.60m @ 116ppm Cs ₂ O from 4.70m	K9TR27	2m @ 125ppm Cs ₂ O from 2m
K9TR08	0.60m @ 125ppm Cs ₂ O from 9.32m	K9TR27	1m @ 121ppm Cs ₂ O from 6m
K9TR10	0.8m @ 123ppm Cs ₂ O from 7.8m 1m @ 270ppm Cs ₂ O from 11m 1m @ 188ppm Cs ₂ O from 12.4m	K9TR27	1.4m @ 458ppm Cs ₂ O from 7.8m 0.9m @ 508ppm Cs ₂ O from 11m
K9TR10	3.3m @ 202ppm Cs ₂ O from 22.7m	K9TR27	0.44m @ 406ppm Cs ₂ O from 13.88m
K9TR12	0.68m @ 192ppm Cs ₂ O from 3.58m 1.1m @ 170ppm Cs ₂ O from 5.9m	K9TR27	1.10m @ 109ppm Cs ₂ O from 14.90m
K9TR13	0.64m @ 128ppm Cs ₂ O from 2m	K9TR28	1.04m @ 129ppm Cs ₂ O from 4.62m
K9TR15	0.80m @ 137ppm Cs ₂ O from 3.70m	K9TR29	1.10m @ 192ppm Cs ₂ O from 2.80m
K9TR15	1.02m @ 163ppm Cs ₂ O from 5.18m	K9TR29	0.40m @ 109 ppm Cs ₂ O from 7.60m
K9TR15	3m @ 180ppm Cs ₂ O from 22m	K9TR30	0.30m @ 134ppm Cs ₂ O from 8.60m
K9TR17	1m @ 101ppm Cs ₂ O from 6.35m	K9TR30	1.60m @ 223ppm Cs ₂ O from 15.70m
K9TR19	1.22m @ 103ppm Cs ₂ O from 5m	K9TR33	6.15m @ 216ppm Cs ₂ O from 5.35m
K9TR19	0.86m @ 235ppm Cs ₂ O from 9.54m 0.4m @ 215ppm Cs ₂ O from 13m	K9TR33	1.10m @ 111ppm Cs ₂ O from 10.90m
K9TR19	1.14m @ 174ppm Cs ₂ O from 13.86m	K9TR33	1.85m @ 137ppm Cs ₂ O from 8.15m
K9TR21	0.82m @ 170ppm Cs ₂ O from 6.68m	K9TR34	0.60m @ 168ppm Cs ₂ O from 11m
K9TR21	0.76m @ 194 ppm Cs ₂ O from 10.80m	K9TR34	1.13m @ 176ppm Cs ₂ O from 11.87m 0.56m @ 221ppm Cs ₂ O from 14m
K9TR23	0.30m @ 163ppm Cs ₂ O from 8.50m	K9TR34	2m @ 121ppm Cs ₂ O from 16m
K9TR23	0.50m @ 142ppm Cs ₂ O from 9.10m		



High Priority Prospective “Corridor of Interest”

The Company has defined a high-priority focus corridor of interest using the regional magnetic data along with chemical data (K/Rb ratios), and which was found to be approximately 15km long and approximately 5km wide, striking in a north east – south west direction (*refer to ASX announcement dated 21 September 2023*).

Additionally, the recently received data has allowed the Company to further identify zones prospective for Li-Sn-Ta mineralization, and areas prospective for Ta mineralization, as well as interpreted extensions of zones of mineralization warranting further exploration in upcoming programs.

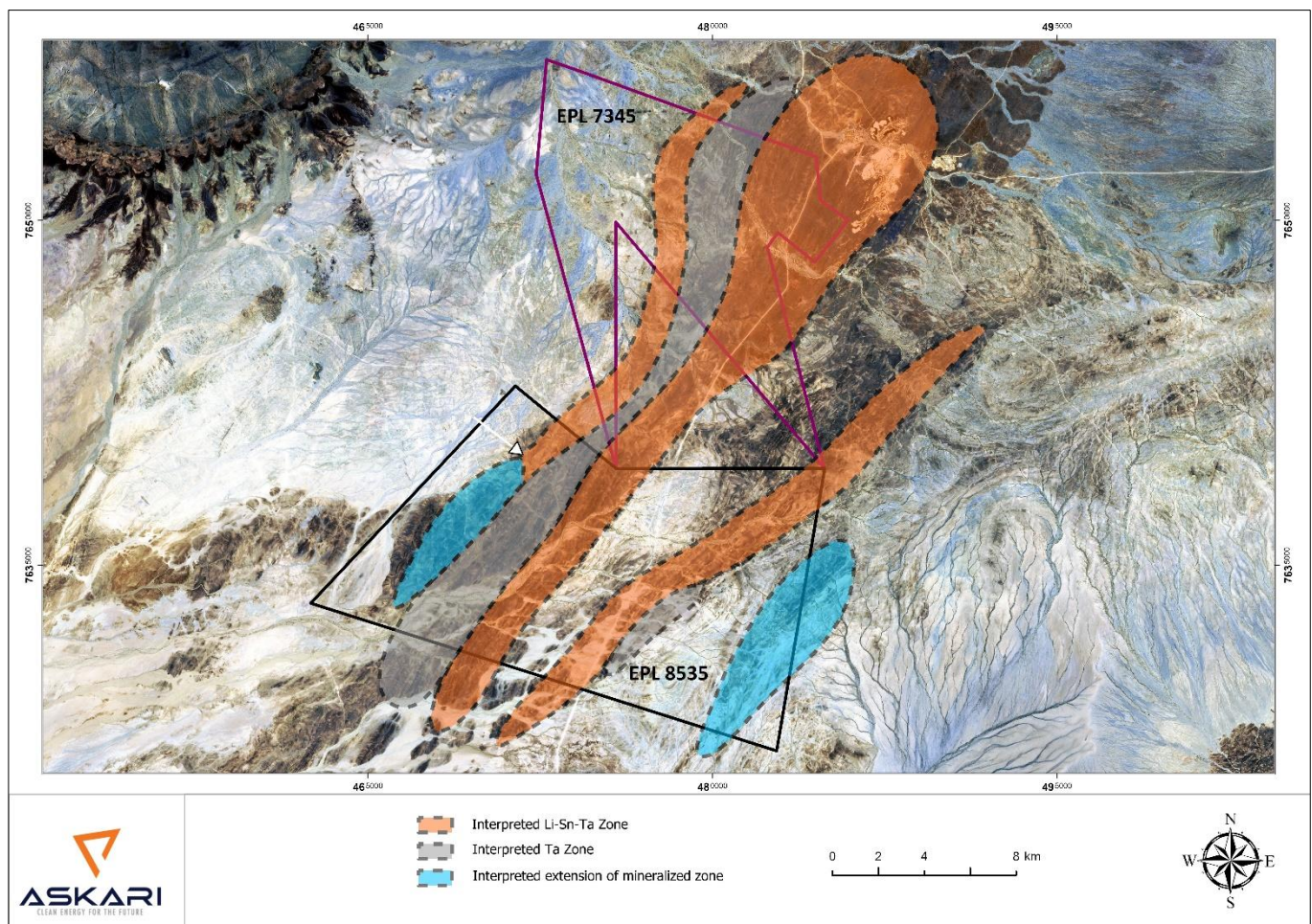


Figure 9: High priority prospective “corridor of interest” with re-defined Li-Sn-Ta prospective zones, Ta prospective zones and areas of potential mineralization extensions.

FUTURE WORK

The Company is planning a focused next phase of exploration aimed at advancing and expanding the known tin, tantalum and broader polymetallic mineralisation across EPL 7345. This work will consist of:

- Second phase infill soil geochemical sampling on EPL 7626
- First phase trenching program on EPL 7626
- First phase trenching program on EPL 8535
- Second phase trenching program on EPL 7345
- Detailed mapping and rock chip sampling of new targets on EPL 7345
- Pending successful results, mobilising an excavator to site for EPL 7345 Phase 2 trenching program
- RC drilling at the DP, OP, PS and K9 pegmatite targets

Figure 10 (below) outlines the tin and tantalum targets across EPL 7345, including extensions of the current OP, DP, PS and K9 targets previously identified by the Company. These areas will form the focus of upcoming follow-up exploration programs, aimed at delineating additional zones of high-grade tin and tantalum mineralisation. The planned low-cost fieldwork is designed to refine and prioritise high-confidence drill targets within EPL 7345, advancing the broader objective of testing and defining the polymetallic mineralisation associated with the Uis Project.

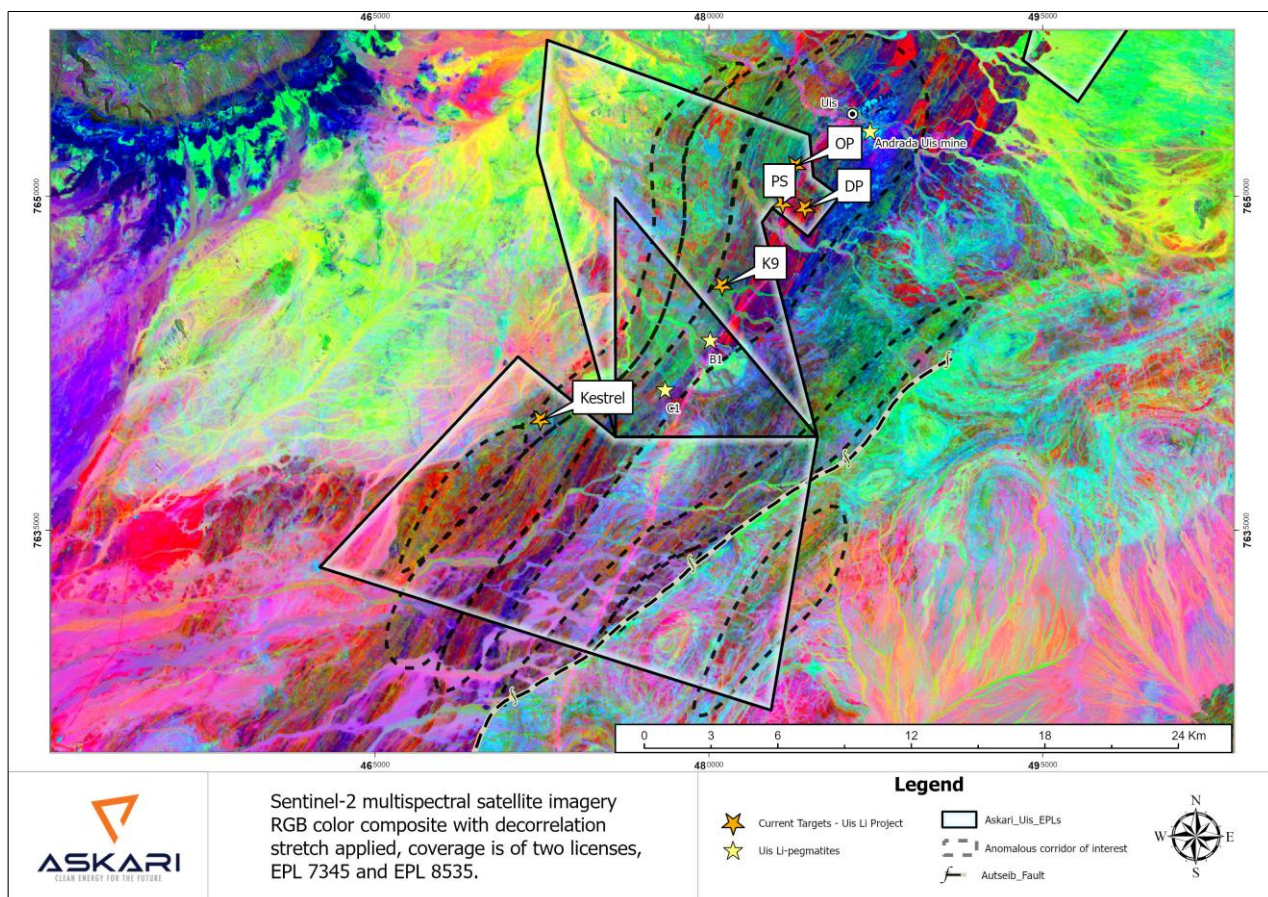


Figure 10: Hyperspectral imagery showing Askari Metals newly identified pegmatite targets on EPL 7345.

PLANNED RC DRILLING AT K9 PEGMATITE TARGET

RC drilling is now being advanced for the K9 pegmatite target, with **Figure 11** (below) showing the planned collar locations and drill traces designed to test the continuity, geometry and depth potential of the system.

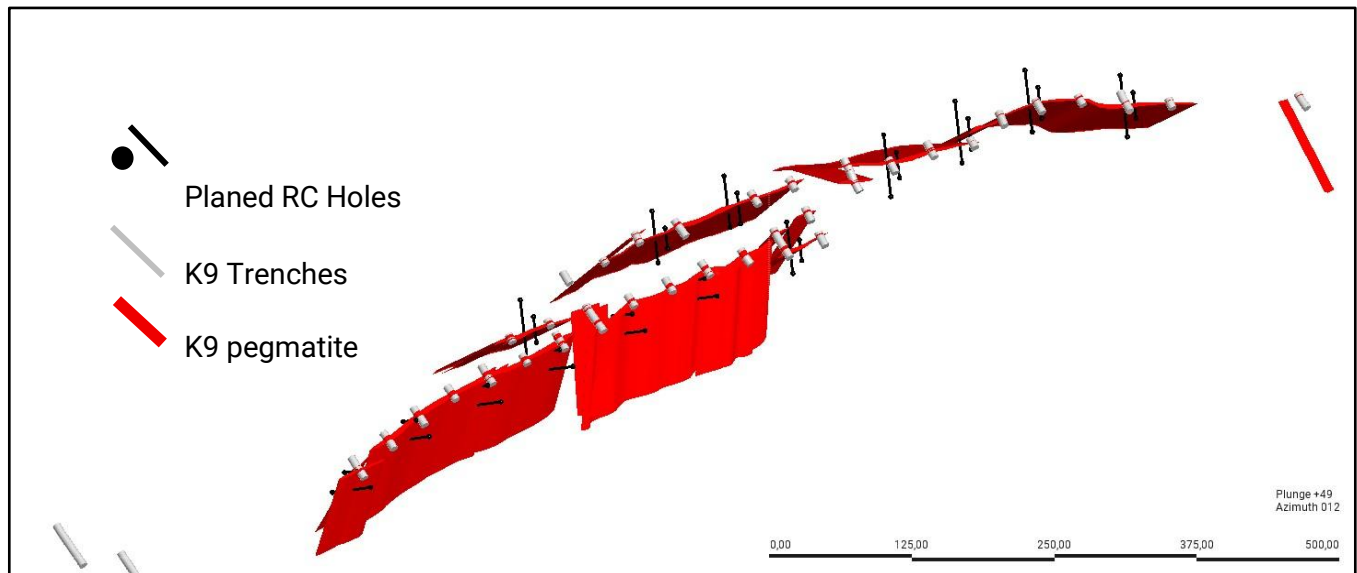


Figure 11: Modelled pegmatite wireframes using trench pegmatite intercepts and mapped structures for inclination.

K9 is interpreted as an inclined pegmatite body, dipping to the northwest on some sections and to the southeast on one section. Accordingly, the wireframes are based on down-dip projections of the apparent pegmatite widths observed in the trenches, providing a practical framework for planning the next phase of drilling.

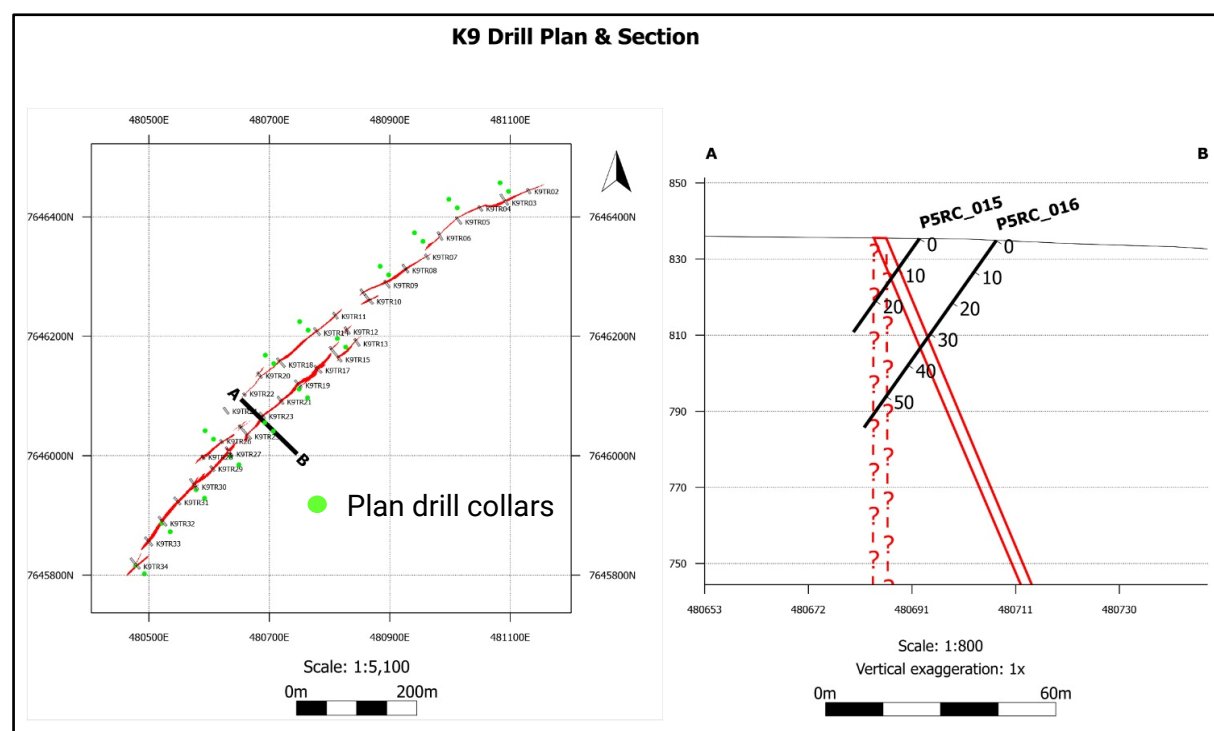


Figure 12: K9 Drill plan and Section View.

With a substantial 950m pegmatite system now defined at K9, strong polymetallic assay results in hand and multiple follow-up programs advancing across EPL 7345, Askari believes the Uis Project is building strong momentum as an emerging critical minerals opportunity. The Company looks forward to delivering continued newsflow as it advances toward planned RC drilling in H2 2026 and works to unlock the broader scale potential of the Uis Project.

Importantly, surface exposure likely represents only part of the K9 opportunity, with pegmatite thickness and strike potential capable of expanding or narrowing both along strike and at depth. Planned drilling is therefore designed to test the true subsurface scale, continuity and geometry of the system – a critical next step in unlocking K9's broader upside. This style of variability is consistent with pegmatites currently being mined and explored at the neighbouring Uis Tin Mine, further reinforcing the potential for K9 to evolve into a much larger mineralised system than surface mapping alone may suggest.

This announcement is authorized for release and distribution by the Board of Directors of Askari Metals Limited

- ENDS -

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ABOUT ASKARI METALS

Askari Metals is a focused African exploration company with a portfolio of highly prospective gold and critical minerals projects in Ethiopia and Namibia. The Company's flagship Nejo Project in Ethiopia is an advanced-stage brownfields gold and copper opportunity located on the Arabian-Nubian Shield, with a district-scale landholding of approximately 1,200km² surrounding the 1.7Moz Tulu Kapi Gold Mine and along strike from the 3.4Moz Kurmuk Mine.

In Namibia, Askari is advancing its 100%-owned Uis Project, a highly prospective polymetallic critical minerals project located within the Cape Cross–Uis Pegmatite Belt. The project sits close to Andrada Mining's operating Uis Tin Mine and is strategically positioned with access to the Walvis Bay Deepwater Port via sealed road infrastructure.

Askari continues to progress exploration across both core assets, with a focus on unlocking value through systematic drilling, target generation and resource growth opportunities.

For more information please visit: www.askarimetals.com



CAUTION REGARDING FORWARD-LOOKING INFORMATION

This document contains forward-looking statements concerning Askari Metals Limited. Forward-looking statements are not statements of historical fact and actual events and results may differ materially from those described in the forward-looking statements as a result of a variety of risks, uncertainties and other factors. Forward-looking statements are inherently subject to business, economic, competitive, political and social uncertainties and contingencies. Many factors could cause the Company's actual results to differ materially from those expressed or implied in any forward-looking information provided by the Company, or on behalf of, the Company. Such factors include, among other things, risks relating to additional funding requirements, metal prices, exploration, development and operating risks, competition, production risks, regulatory restrictions, including environmental regulation and liability and potential title disputes.

Forward looking statements in this document are based on the Company's beliefs, opinions and estimates of Askari Metals Limited as of the dates the forward-looking statements are made, and no obligation is assumed to update forward looking statements if these beliefs, opinions and estimates should change or to reflect other future developments.

CAUTIONARY STATEMENT

Visual estimates of mineral abundance should never be considered a proxy or substitute for laboratory analyses where concentrations or grades are the factor of principal economic interest. Visual estimates also potentially provide no information regarding impurities or deleterious physical properties relevant to valuations.

COMPETENT PERSONS STATEMENT

The information in this announcement that relates to Exploration Results concerning the K9 Trench Assay Results at the Uis Project in Namibia is based on and fairly represents information compiled by Mr Lachlan Reynolds, a Competent Person who is a member of both the Australian Institute of Mining and Metallurgy and the Australasian Institute of Geoscientists.

Mr. Reynolds is the principal of Sianora Pty Ltd and is employed as a technical consultant by Askari Metals Limited. Mr Reynolds has sufficient experience that is relevant to the style of mineralisation and types of deposits under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Mr. Reynolds consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

For further information and details on sources of previous exploration information completed by Askari Metals Limited and released to ASX in compliance with JORC (2012) guidelines, refer to ASX announcements as noted below covering the various dates and announcements.

The information in this announcement that relates to previous Exploration Results and potential for the Uis Project are based on information compiled by Clifford Fitzhenry, a Competent Person who is a Registered Professional Natural Scientist with the South African Council for Natural Scientific Professions (SACNASP) as well as a Member of the Geological Society of South Africa (GSSA) and a Member of the Society of Economic Geologists (SEG). Mr. Fitzhenry was previously a Technical Consultant for Askari Metals Limited, who has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves.

ASX COMPLIANCE STATEMENT AND RELIANCE ON PREVIOUS ASX ANNOUNCEMENTS

In preparing this announcement, the Company relied on the following ASX announcements:

15 April 2025	Extensive High-Grade Tin and Tantalum Mineralisation at Uis
28 April 2025	Supplementary Information to ASX Announcement dated 15.04.25
6 May 2025	Uis Project Delivers More High-Grade Tin and Tantalum
16 May 2025	Amendment and Supplementary Information to 6 May 2025
27 May 2025	Tin and Tantalum Exploration Program to Commence at Uis
18 June 2025	Askari Provides Operational and Activities Update

The Company confirms that it is not aware of any new information or data that materially affects those announcements previously made, or that would materially affect the Company from relying on those announcements for the purpose of this announcement.



Appendix 1 – JORC Code, 2012 Edition, Table 1 report

Section 1 Sampling Techniques and Data (Criteria in this section applies to all succeeding sections)

Criteria	JORC Code explanation	Commentary
Sampling techniques	- Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. - Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. - Aspects of the determination of mineralisation that are Material to the Public Report.	Trench Channel Sampling - Trenches at the K9 target were dug by a mechanical excavator to bucket refusal depth, approximately 0.3 to 0.5m deep. Fresh to weakly weathered pegmatite and host rock were exposed in the excavated trenches. - Trenches were oriented approximately perpendicular to known pegmatite exposures. - Trenches were marked in-situ, using a tape measure fixed at a defined origin point ("collar") to determine lengths along the trench from the collar. - A channel was cut into the exposed rock using a hand-held mechanical rock saw, which was used to cut two parallel lines in the centre of the trench floor, approximately 5-7cm apart and approximately 5-7cm deep. - Channel sample lengths were based on nominal 1m intervals, modified by geological controls and contacts as required. Sample intervals varied from a minimum of 0.3m to 1.9m. - Channel samples were collected systematically by chipping material from between the two rock saw cuts to a nominal 5-7cm depth. - Sample material was immediately transferred to transparent plastic bags and sealed. - Sample information was recorded at the time of sampling including, trench ID, sample ID, meter intervals, weight and lithology. - Field duplicates were sampled by cutting a second channel parallel and at equal length and depth to the original sample location, at the same position within the trench. - Standard operating procedures were adopted to ensure that the channel samples were systematically collected and recorded.
Drilling techniques	Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details.	Not applicable
Drill sample recovery	Method of recording and assessing core and chip sample recoveries and results assessed.	Trench Channel Sampling - Channel sample recovery was assessed visually based on the standardised width and depth of the channels. - Weights of the channel samples was recorded as the samples were collected to ensure consistency of sample recovery.



Criteria	JORC Code explanation	Commentary
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource Estimation, mining studies and metallurgical studies.	Trench Channel Sampling - Channel sample lithologies were geologically logged in the field. - The level of logging is not sufficient to support Mineral Resource Estimation, mining studies or metallurgical studies.
Sub-sampling techniques and sample preparation	For all sample types, the nature, quality and appropriateness of the sample preparation technique.	Trench Channel Sampling - Channel sample preparation was performed by Activation Laboratories Ltd (Actlabs) in Namibia. - The entire channel sample is crushed to a nominal -2 mm, then mechanically split to obtain a representative sample and then pulverized to at least 90% -75 microns (µm). - Actlab mills are mild steel and do not introduce Cr or Ni contamination. - A quartz flush is put through the pulveriser prior to each new batch of samples. A number of quartz flushes are also put through the pulveriser to ensure the bowl is clean prior to the next sample being processed. - Quality of crushing and pulverization is routinely checked as part of the laboratory quality assurance program. - An approximately 15g pulp sub-sample is taken from the large sample for shipping to the Actlabs Canada, where it was analysed. - Residual samples material is stored at Actlabs in Namibia.
Quality of assay data and laboratory tests	- The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. - Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	Trench Channel Sampling - Analytical sub-samples were submitted for assays to Activation Laboratories Ltd. (Actlabs) in Canada. - The samples were analysed for a multi-element suite using a Sodium Peroxide Fusion with ICP-MS and ICP-MS finish. This technique is considered to be appropriate for the sample types and to be a total assay. - ICP-MS finish - Fused samples are diluted and analyzed by Agilent 7900 ICP-MS. Calibration is performed using five synthetic calibration standards. A set of (10-20) fused certified reference material is run with every batch of samples for calibration and quality control. Fused duplicates are run every 10 samples. - ICP-OES finish - Samples are analyzed with a minimum of 10 certified reference materials for the required analytes, all prepared by sodium peroxide fusion. Every 10th sample is prepared and analyzed in duplicate; a blank is prepared every 30 samples and analyzed. Samples are analyzed using a Varian 735ES ICP and internal standards are used as part of the standard operating procedure.



Criteria	JORC Code explanation	Commentary
		- Actlabs randomly inserts analytical blanks, standards and duplicates into the client sample batches for laboratory QAQC performance monitoring. - The Company inserted standards and blanks samples to assess the accuracy and precision of the analytical results. - The Company also inserted duplicate samples to assess local geological variability in the mineralisation. - Assessment of the QAQC results showed a suitable level of accuracy and precision in the analytical results. 100% of results are within acceptable QAQC limits as stated by the standard deviation stipulated on the certificate for the reference material used.
Verification of sampling and assaying	- The verification of significant intersections by either independent or alternative company personnel. - Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. - Discuss any adjustment to assay data.	Trench Channel Sampling - Significant intersections identified by the Company personnel in Namibia were checked and verified by a consultant to the Company. No independent verification has been completed. - Documentation of primary data, data entry and verification was completed by Company personnel in Namibia. - Digital geological, survey and assay data is stored in a database managed and maintained by the Company. - Where appropriate, assay data has been converted to oxide equivalent values (see below).
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.	Trench Channel Sampling - Trenches collars were surveyed by Differential Global Positioning System (DGPS) to an accuracy of between 0.5 to 1.0m. - Trench lengths were surveyed by sub-division into meter-intervals systematically marked along the trench wall. - Down trench surveys were conducted using compass azimuth and slope variation, which was minimal. - All coordinates reported in this announcement are based on the WGS1984 datum, projection UTM Zone 33S.
Data spacing and distribution	- Data spacing for reporting of Exploration Results. - Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.	Trench Channel Sampling - Trenches are located on a nominal 40m spacing along the northeast-southwest oriented trend of the target pegmatite units. - Sample spacing is continuous along the floor of the trenches, with a nominal 1m sample length, modified as required.



Criteria	JORC Code explanation	Commentary
	Whether sample compositing has been applied.	- Data spacing and distribution is not sufficient to establish the degree of geological and grade continuity appropriate for a Mineral Resource estimate. - Sample compositing has not been applied.
Orientation of data in relation to geological structure	Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.	Trench Channel Sampling - Trenches and channel samples were designed to minimise sample bias. - Trenches are oriented approximately perpendicular to the northeast-southwest oriented trend of the target pegmatite units. - The sampled pegmatite units have a variable dip, with an approximate average dip of -45 degrees toward the northwest. - Sample intervals are reported based on their position along the trenches and have not been adjusted to account for the true width of the pegmatite units.
Sample security	The measures taken to ensure sample security.	Trench Channel Sampling - All samples were collected and in the custody of Company employees/consultants during channel sampling. - All samples were bagged into clear 200-micron thick nylon/plastic bags and closed with cable ties. - Samples were transported to Actlabs in Windhoek by Company personnel for sample preparation and were shipped by Actlabs to Canada for assay. - The appropriate manifest of sample numbers and a sample submission form containing laboratory instructions were submitted to the laboratory. Any discrepancies between sample submissions and samples received were routinely followed up and accounted for.
Audits or reviews	The results of any audits or reviews of sampling techniques and data.	Trench Channel Sampling No external audits have been conducted on the trench channel sampling data, except for software-based data validation (using Micromine).



Section 2 Reporting of Exploration Results (Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	- Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. - The security of the tenure held at the time of reporting along with any known impediments to obtaining a license to operate in the area.	- The Uis Lithium-Tantalum-Tin Project (Uis Project) comprises 3 Exclusive Prospecting Licences (EPL) covering an area of approximately 380km² within the Erongo Region of west-central Namibia. - EPL 7345 and EPL 7626 is held 100% by the Company whilst EPL 8535 is held 80% by the Company. - The results reported in this announcement relate to EPL7345. The licence was granted for 3 years on 15 March 2021. The licence renewal is currently being processed by the Ministry of Industries, Mines and Energy. The Company is in compliance with the EPL conditions and expects the licence to be renewed in due course. - The tenure is considered secure and there are no known impediments to obtaining further licences to operate in the area. - The Uis Project is located less than 5km from the township of Uis and less than 2.5km from the operating Uis Tin-Tantalum-Lithium Mine, owned and operated by Andrada Mining plc (LSE. ATM). - Swakopmund, the capital city of the Erongo Region and Namibia's fourth largest settlement is located approximately 165km south of the Uis Project, while the Namibian capital city of Windhoek is located approximately 270km southeast of the Uis Project.
Exploration done by other parties	Acknowledgment and appraisal of exploration by other parties.	- Tin and tantalum prospecting and exploration has been undertaken by other parties in the region, and a number of mineral deposits and occurrences are documented. - Limited exploration for lithium has been completed in this region. No drilling for lithium has been previously reported, apart from the reconnaissance drilling conducted by the Company during the first tenure period of the licence.
Geology	Deposit type, geological setting and style of mineralisation.	- The rocks of the Erongo Region, and specifically the Dâures Constituency, are represented by rocks of the Khomas Subgroup, a division of the Swakop Group of the Damara Sequence, which have been intruded by numerous zones and unzoned mineralised pegmatites rich in cassiterite, lepidolite, petalite, amblygonite, spodumene, tantalite, columbite, beryl, gem tourmaline, and rare to sparse sulphides, wolframite, scheelite, pollucite or rare earth metals. - The Uis and Nainais-Kohero swarm of pegmatites represents the fillings of en-echelon tension gashes that formed as a result of shearing of a regional nature, which evolved slowly over considerable geological time. These pegmatites are pervasively altered or extensively albitised, with only relics of the original potassium feldspars left after their widespread replacement by albite. They are remarkably similar in composition, except for the varying intensity of pneumatolytic effects, and the introduction or concentration of trace elements during the final stages of crystallisation has resulted in complex pegmatite mineralogies. These pegmatites are found within schistose and quartzose rocks of the Khomas Subgroup, a division of the Swakop Group, which have been subjected to intense tectonic deformation and regional metamorphism. - Detailed geological mapping within the Uis area suggests that the Uis swarm of pegmatites consists of over 100 individual pegmatite bodies. Shearing opened spaces within the Khomas Subgroup country rocks, spaces in which pegmatite or quartz veins were subsequently intruded. Within the Nainais pegmatites, high tin values are found in



Criteria	JORC Code explanation	Commentary
		smaller altered mica-rich pegmatites near the pegmatite edges. The pegmatite mineralisation composition changes in the distance from the granitic contacts with a mineral crystallisation sequence having been mapped, which indicates garnet and schorl occurring closest to the granitic contacts, the cassiterite and lithium-tourmaline occurring further away therefrom, and the tantalite being associated with lithium-tourmaline and quartz blows. The Uis Project boasts more than 80 mapped pegmatites across the project area, with many of the pegmatites having been mined historically for tin and semi-precious stones.
Drill hole Information	A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:	Trench Channel Sampling See Appendix 2 for a tabulation of Trench location details.
Data aggregation methods	- In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. - Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.	- No Mineral Resource has been estimated for the project at this stage. The results presented are based on the previously undisclosed Exploration Results. - No maximum or minimum grade truncations have been applied to the assay data. - Intervals are based on weighted average grades using the cut-off grades detailed below: - Tin (Sn): Intervals with continuous samples each grading $\geq 500\text{ppm}$ Sn were averaged to calculate significant intersections. Higher grade internal zones $\geq 1000\text{ppm}$ Sn were averaged and used as best intercept highlights in summary tables map labels. - Lithium (Li_2O): Intervals with continuous samples each grading $\geq 0.25\%$ Li_2O were averaged to calculate significant intersections. Higher grade internal zones $\geq 0.25\%$ Li_2O were averaged and used as best intercept highlights in summary tables and $\geq 0.35\%$ Li_2O on map labels. - Tantalum (Ta): Intervals with continuous samples each grading $\geq 80\text{ ppm}$ Ta were averaged and used as best intercept highlights in summary tables. - Rubidium (Rb_2O): Intervals with continuous samples each grading $\geq 0.1\%$ Rb_2O Rb were averaged and used as best intercept highlights in summary tables and $\geq 0.15\%$ Rb_2O Rb on map labels. - Caesium (Cs_2O): Intervals with continuous samples each grading $\geq 100\text{ ppm}$ Cs_2O were averaged and used as best intercept highlights in summary tables.



Criteria	JORC Code explanation	Commentary																		
		- Conversion of elemental assay data to oxide values is based on standard element-to-stoichiometric oxide conversion factors (see table below). Factors are taken from the James Cook University Advanced Analytical Centre (refer to https://www.jcu.edu.au/advanced-analytical-centre/resources/element-to-stoichiometric-oxide-conversion-factors). <table border="1"> <thead> <tr> <th>Element</th><th>Oxide Form</th><th>Conversion Factor</th></tr> </thead> <tbody> <tr> <td>Li</td><td>Li₂O</td><td>2.153</td></tr> <tr> <td>Rb</td><td>Rb₂O</td><td>1.0925</td></tr> <tr> <td>Ta</td><td>Ta₂O₅</td><td>1.2211</td></tr> <tr> <td>Sn</td><td>SnO₂</td><td>1.2696</td></tr> <tr> <td>Cs</td><td>Cs₂O</td><td>1.0602</td></tr> </tbody> </table> - Conversion of original element grades or their respective oxide values in parts per million (ppm) to percentage (%) values has been completed where appropriate by dividing ppm grade by 10,000.	Element	Oxide Form	Conversion Factor	Li	Li ₂ O	2.153	Rb	Rb ₂ O	1.0925	Ta	Ta ₂ O ₅	1.2211	Sn	SnO ₂	1.2696	Cs	Cs ₂ O	1.0602
Element	Oxide Form	Conversion Factor																		
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Sn	SnO ₂	1.2696																		
Cs	Cs ₂ O	1.0602																		
Relationship between mineralisation widths and intercept lengths	- These relationships are particularly important in the reporting of Exploration Results. - If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.	Trench Channel Sampling - The trend of the pegmatites hosting mineralisation is generally in a northeast-southwest direction. - The dip of the pegmatites varies, from near vertical to shallow towards the northwest, with an average dip of approximately -60 degrees to the northwest. - Trenching and channel sampling was completed approximately perpendicular to the strike and parallel to the dip of the mineralised pegmatites. - The true width of the mineralisation is not yet constrained by drilling.																		
Diagrams	Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported. These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	Appropriate diagrams and tabulated results are included in the body of the announcement.																		
Balanced reporting	Where comprehensive reporting of all Exploration Results is not practicable, representative	Trench Channel Sampling All trench channel sample results from the K9 target have been reported in this announcement, see Appendix 3.																		



Criteria	JORC Code explanation	Commentary
	reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of results.	
Other substantive exploration data	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Trench Channel Sampling Assessment of other substantive exploration data is not yet complete however considered immaterial at this stage.
Further work	The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).	- Planned exploration of the mineralised pegmatites at the Uis Project is intended to test for lateral and depth extensions of the known mineralised zones and completion of resource evaluation drilling if appropriate. - Further RC percussion drilling of key mineralised pegmatites. - Project wide soil geochemical sample programmes across the “Corridor of Interest” with an aim to delineate further anomalous areas (targeting buried / blind pegmatites). - Detailed mapping and rock chip sampling of new targets on EPL 7345. - Phase 2 trenching program. - Further RC drilling.



Appendix 2 – Table of trench location details pertaining to this announcement

Trench_ID	X_actual	Y_actual	Z_actual	Azi_T_start	EOT_m	Survey_method	Surveyed_by	Coordindate_reference_system
K9TR01	481242.84	7646496.97	853.55	144.00	17.00	DGPS	HS_Surv	WGS84_UTM33S
K9TR02	481129.58	7646448.16	855.65	152.00	9.90	DGPS	HS_Surv	WGS84_UTM33S
K9TR03	481085.69	7646438.7	858.39	155.00	21.50	DGPS	HS_Surv	WGS84_UTM33S
K9TR04	481048.57	7646419.49	859.87	149.00	10.60	DGPS	HS_Surv	WGS84_UTM33S
K9TR05	481011.45	7646400.78	860.64	145.00	14.80	DGPS	HS_Surv	WGS84_UTM33S
K9TR06	480981.21	7646375.67	860.61	153.00	15.80	DGPS	HS_Surv	WGS84_UTM33S
K9TR07	480959.88	7646338.29	859.09	139.00	10.60	DGPS	HS_Surv	WGS84_UTM33S
K9TR08	480922.5	7646321.36	857.57	140.00	16.90	DGPS	HS_Surv	WGS84_UTM33S
K9TR09	480892.33	7646294.38	853.36	145.00	14.80	DGPS	HS_Surv	WGS84_UTM33S
K9TR10	480852.96	7646279.82	853.99	148.00	33.00	DGPS	HS_Surv	WGS84_UTM33S
K9TR11	480806.78	7646240.72	853.42	126.00	13.30	DGPS	HS_Surv	WGS84_UTM33S
K9TR12	480826.52	7646216.39	849.47	146.00	14.60	DGPS	HS_Surv	WGS84_UTM33S
K9TR13	480842.69	7646196.83	845.09	146.00	14.80	DGPS	HS_Surv	WGS84_UTM33S
K9TR14	480775.51	7646215.17	852	139.00	15.60	DGPS	HS_Surv	WGS84_UTM33S
K9TR15	480801.76	7646183.73	848.44	144.00	32.00	DGPS	HS_Surv	WGS84_UTM33S
K9TR16	480747.90	7646184.61	847.19	140.30	9.07	DGPS	HS_Surv	WGS84_UTM33S
K9TR17	480776.5	7646151.93	846.32	140.00	16.60	DGPS	HS_Surv	WGS84_UTM33S
K9TR18	480714.32	7646164.33	845.59	144.00	19.50	DGPS	HS_Surv	WGS84_UTM33S
K9TR19	480743.77	7646127.43	844.2	140.00	16.60	DGPS	HS_Surv	WGS84_UTM33S
K9TR20	480681.51	7646140.98	841.65	144.00	12.40	DGPS	HS_Surv	WGS84_UTM33S
K9TR21	480715.34	7646100.1	840.79	148.00	15.70	DGPS	HS_Surv	WGS84_UTM33S
K9TR22	480658.06	7646106.06	837.08	140.00	6.50	DGPS	HS_Surv	WGS84_UTM33S
K9TR23	480685.2	7646073.52	836.65	140.00	13.60	DGPS	HS_Surv	WGS84_UTM33S
K9TR24	480625.87	7646081.72	833.03	145.00	13.00	DGPS	HS_Surv	WGS84_UTM33S
K9TR25	480650.86	7646052.4	832.3	144.00	30.70	DGPS	HS_Surv	WGS84_UTM33S
K9TR26	480619.70	7646027.52	828.31	137.00	7.60	DGPS	HS_Surv	WGS84_UTM33S
K9TR27	480628.97	7646015.48	828.05	144.00	19.50	DGPS	HS_Surv	WGS84_UTM33S
K9TR28	480588.68	7646001.83	824.25	141.00	8.50	DGPS	HS_Surv	WGS84_UTM33S
K9TR29	480603.67	7645983.76	824.15	145.00	10.80	DGPS	HS_Surv	WGS84_UTM33S
K9TR30	480569.98	7645962.22	820.29	146.00	21.70	DGPS	HS_Surv	WGS84_UTM33S
K9TR31	480543.26	7645931.34	816.60	135.00	16.00	DGPS	HS_Surv	WGS84_UTM33S
K9TR32	480517.66	7645899.01	813.67	144.00	20.10	DGPS	HS_Surv	WGS84_UTM33S
K9TR33	480494.64	7645864.52	810.74	146.00	19.00	DGPS	HS_Surv	WGS84_UTM33S
K9TR34	480471.11	7645829.40	807.32	144.00	23.40	DGPS	HS_Surv	WGS84_UTM33S
K9TR35	480282.63	7645650.86	805.53	146.00	58.00	DGPS	HS_Surv	WGS84_UTM33S
K9TR36	480356.69	7645562.31	806.8	143.00	60.00	DGPS	HS_Surv	WGS84_UTM33S
K9TR37	480283.25	7645588.16	806.81	141.00	70.30	DGPS	HS_Surv	WGS84_UTM33S
K9TR38	480222.13	7645661.57	805.41	147.00	47.00	DGPS	HS_Surv	WGS84_UTM33S



Appendix 3 – Table of assay results pertaining to this announcement

Trench_ID	Sample_ID	From_m	To_m	Width_m	Weight_Kg	Cs_ppm	Li_ppm	Rb_ppm	Sn_ppm	Ta_ppm	Li2O_%	SnO2_%	Ta2O5_ppm	Rb2O_%	Cs2O_ppm
K9TR34	Q5702	11.00	11.60	1.16	3	158	550	500	136	7	0.12	0.02	8.55	0.05	167.51
K9TR34	Q5703	11.60	11.87	0.64	4	66.2	129	926	1450	76.4	0.03	0.18	93.29	0.10	70.19
K9TR34	Q5704	11.87	13.00	1.00	9	166	482	532	72.8	3.5	0.10	0.01	4.27	0.06	175.99
K9TR34	Q5705	14.00	14.56	0.86	5	208	370	546	66.9	6.6	0.08	0.01	8.06	0.06	220.52
K9TR34	Q5706	14.56	16.00	0.44	10	64.5	57	727	932	126	0.01	0.12	153.86	0.08	68.38
K9TR34	Q5707	16.00	16.87	0.70	7	98.4	156	945	487	93.5	0.03	0.06	114.17	0.10	104.32
K9TR34	Q5708	16.87	18.00	0.92	6	126	311	225	53.1	14.6	0.07	0.01	17.83	0.02	133.59
K9TR33	Q5709	5.35	6.15	0.98	7	204	817	627	108	13.4	0.18	0.01	16.36	0.07	216.28
K9TR33	Q5710	6.15	7.00	1.10	9	77.5	134	874	470	82.7	0.03	0.06	100.98	0.10	82.17
K9TR33	Q5711	7.00	8.15	0.70	11	49.9	176	757	542	42.6	0.04	0.07	52.02	0.08	52.90
K9TR33	Q5712	10.00	10.90	0.60	17	58.1	133	743	1250	106	0.03	0.16	129.44	0.08	61.60
K9TR33	Q5713	10.90	12.00	0.70	10	105	125	1190	416	152	0.03	0.05	185.61	0.13	111.32
K9TR33	Q5714	8.15	10.00	1.16	14	129	1010	856	150	7.3	0.22	0.02	8.91	0.09	136.77
K9TR32	Q5715	5.00	5.80	0.84	7	58.3	563	555	84.9	8.7	0.12	0.01	10.62	0.06	61.81
K9TR32	Q5716	5.80	7.50	1.06	15	33.7	338	660	496	52.5	0.07	0.06	64.11	0.07	35.73
K9TR32	Q5717	7.50	9.00	0.98	14	35.5	493	655	1940	73.7	0.11	0.25	90.00	0.07	37.64
K9TR32	Q5718	9.00	10.50	0.96	20	45.7	276	780	873	69.9	0.06	0.11	85.35	0.09	48.45
K9TR32	Q5719	10.50	11.10	0.90	9	86.4	301	740	357	44	0.06	0.05	53.73	0.08	91.60
K9TR32	Q5721	11.10	12.00	0.96	11	46.2	310	171	39.3	9.7	0.07	0.00	11.84	0.02	48.98
K9TR31	Q5722	7.00	7.50	1.04	5	55.2	672	506	88.5	8.2	0.14	0.01	10.01	0.06	58.52
K9TR31	Q5723	7.50	9.00	1.30	15	44	801	656	458	104	0.17	0.06	126.99	0.07	46.65
K9TR31	Q5724	9.00	10.00	0.40	11	31.9	778	627	860	59.4	0.17	0.11	72.53	0.07	33.82
K9TR31	Q5725	10.00	11.00	0.60	9	28.1	769	491	968	70.3	0.17	0.12	85.84	0.05	29.79
K9TR31	Q5726	11.00	11.80	0.60	8	32.6	271	542	4050	86.8	0.06	0.51	105.99	0.06	34.56
K9TR31	Q5727	11.80	12.40	1.10	5	20.5	743	297	129	5.7	0.16	0.02	6.96	0.03	21.73
K9TR30	Q5728	8.60	8.90	0.90	2	126	1190	481	73.9	15.5	0.26	0.01	18.93	0.05	133.59
K9TR30	Q5729	8.90	10.00	0.32	9	55.9	329	688	765	94.5	0.07	0.10	115.39	0.08	59.27
K9TR30	Q5730	10.00	11.00	0.60	10	85.1	874	1350	944	70.8	0.19	0.12	86.45	0.15	90.22
K9TR30	Q5731	11.00	12.00	0.78	10	71.7	894	1110	509	48.1	0.19	0.06	58.73	0.12	76.02
K9TR30	Q5732	12.00	12.80	0.50	7	64.8	357	853	582	97.2	0.08	0.07	118.69	0.09	68.70
K9TR30	Q5733	12.80	13.30	0.90	4	86.7	956	607	87	33	0.21	0.01	40.30	0.07	91.92
K9TR30	Q5734	15.70	16.00	1.10	3	189	548	400	132	10.3	0.12	0.02	12.58	0.04	200.38



Trench_ID	Sample_ID	From_m	To_m	Width_m	Weight_Kg	Cs_ppm	Li_ppm	Rb_ppm	Sn_ppm	Ta_ppm	Li2O_%	SnO2_%	Ta2O5_ppm	Rb2O_%	Cs2O_ppm
K9TR30	Q5735	16.00	16.70	0.90	8	170	330	981	775	145	0.07	0.10	177.06	0.11	180.23
K9TR30	Q5736	16.70	17.30	1.00	6	269	849	667	149	20.5	0.18	0.02	25.03	0.07	285.19
K9TR28	Q5737	0.60	1.54	0.88	6	35	806	375	39.2	3.1	0.17	0.00	3.79	0.04	37.11
K9TR28	Q5738	1.54	2.60	1.12	7	35.4	306	599	700	43.7	0.07	0.09	53.36	0.07	37.53
K9TR28	Q5739	2.60	3.00	1.00	3	24.3	356	384	409	38.8	0.08	0.05	47.38	0.04	25.76
K9TR28	Q5741	3.00	4.00	0.90	5	22.7	205	511	443	35.6	0.04	0.06	43.47	0.06	24.07
K9TR28	Q5742	4.00	4.62	0.80	5	29.2	191	518	1020	39.8	0.04	0.13	48.60	0.06	30.96
K9TR28	Q5743	4.62	5.66	0.90	6	122	826	640	188	6.5	0.18	0.02	7.94	0.07	129.34
K9TR28	Q5744	5.66	6.70	1.00	10	44.9	282	723	766	95	0.06	0.10	116.00	0.08	47.60
K9TR28	Q5745	6.70	7.30	0.40	3	37.4	675	450	82.4	11.1	0.15	0.01	13.55	0.05	39.65
K9TR29	Q5746	2.80	3.90	1.00	11	181	1370	914	212	14.1	0.29	0.03	17.22	0.10	191.90
K9TR29	Q5747	3.90	5.00	1.00	14	37.2	421	891	505	59.7	0.09	0.06	72.90	0.10	39.44
K9TR29	Q5748	5.00	6.00	1.04	14	30.8	594	970	842	76	0.13	0.11	92.80	0.11	32.65
K9TR29	Q5749	6.00	7.00	1.26	14	59.5	620	1050	1230	93.5	0.13	0.16	114.17	0.11	63.08
K9TR29	Q5750	7.00	7.60	1.00	8	76	210	932	916	126	0.05	0.12	153.86	0.10	80.58
K9TR29	Q5751	7.60	8.00	1.00	4	103	700	636	94.8	43	0.15	0.01	52.51	0.07	109.20
K9TR26	Q5752	2.35	3.40	0.80	6	29.2	357	490	80.8	10.2	0.08	0.01	12.46	0.05	30.96
K9TR26	Q5753	3.40	4.00	0.92	5	24.2	329	492	640	94.6	0.07	0.08	115.52	0.05	25.66
K9TR26	Q5754	4.00	5.00	0.48	6	39.2	879	772	644	63.2	0.19	0.08	77.17	0.08	41.56
K9TR26	Q5755	5.00	5.72	0.68	7	39.2	395	546	794	38.9	0.09	0.10	47.50	0.06	41.56
K9TR26	Q5756	5.72	6.00	0.74	2	37.7	705	601	127	19.8	0.15	0.02	24.18	0.07	39.97
K9TR27	Q5757	2.00	3.00	0.90	8	99.1	981	612	160	7.3	0.21	0.02	8.91	0.07	105.07
K9TR27	Q5758	3.00	4.00	1.10	10	136	203	1130	3030	185	0.04	0.38	225.90	0.12	144.19
K9TR27	Q5759	4.00	5.00	0.64	8	47.8	253	849	877	98.7	0.05	0.11	120.52	0.09	50.68
K9TR27	Q5761	5.00	6.00	0.60	8	84.1	534	1770	291	102	0.11	0.04	124.55	0.19	89.16
K9TR27	Q5762	6.00	7.00	0.84	8	114	422	1640	570	82.2	0.09	0.07	100.37	0.18	120.86
K9TR27	Q5763	7.00	7.80	0.86	9	91.1	255	1110	850	123	0.05	0.11	150.20	0.12	96.58
K9TR27	Q5764	7.80	8.30	0.98	5	373	806	711	142	19.1	0.17	0.02	23.32	0.08	395.45
K9TR27	Q5765	8.30	9.20	0.62	6	465	561	398	54	2.7	0.12	0.01	3.30	0.04	492.99
K9TR27	Q5766	11.00	11.90	1.00	7	479	1070	981	122	5.2	0.23	0.02	6.35	0.11	507.84
K9TR27	Q5767	11.90	13.00	1.00	9	42.9	226	606	1040	122	0.05	0.13	148.97	0.07	45.48
K9TR27	Q5768	13.00	13.88	0.34	7	76.4	427	695	690	58.5	0.09	0.09	71.43	0.08	81.00
K9TR27	Q5769	13.88	14.32	0.66	6	383	1180	1210	244	25.9	0.25	0.03	31.63	0.13	406.06
K9TR27	Q5770	14.32	14.90	0.70	4	37.1	162	606	577	75.4	0.03	0.07	92.07	0.07	39.33
K9TR27	Q5771	14.90	16.00	0.80	8	103	546	547	136	22.8	0.12	0.02	27.84	0.06	109.20
K9TR25	Q5772	1.20	1.70	0.68	4	33.3	396	349	61.3	8.4	0.09	0.01	10.26	0.04	35.30



Trench_ID	Sample_ID	From_m	To_m	Width_m	Weight_Kg	Cs_ppm	Li_ppm	Rb_ppm	Sn_ppm	Ta_ppm	Li2O_%	SnO2_%	Ta2O5_ppm	Rb2O_%	Cs2O_ppm
K9TR25	Q5773	1.70	2.35	1.02	5	47.8	155	644	460	93.6	0.03	0.06	114.29	0.07	50.68
K9TR25	Q5774	2.35	3.00	1.10	5	46.7	485	456	33.5	3.2	0.10	0.00	3.91	0.05	49.51
K9TR25	Q5775	3.00	4.20	1.26	7	59.9	663	529	92.1	4.7	0.14	0.01	5.74	0.06	63.51
K9TR25	Q5776	4.20	4.50	1.00	3	48.1	749	650	707	50.9	0.16	0.09	62.15	0.07	51.00
K9TR25	Q5777	4.50	5.00	1.00	4	113	1200	1090	378	34	0.26	0.05	41.52	0.12	119.80
K9TR25	Q5778	5.00	5.90	1.00	5	44.5	329	452	1370	53.7	0.07	0.17	65.57	0.05	47.18
K9TR25	Q5779	5.90	7.00	1.08	8	54.7	644	600	135	8.5	0.14	0.02	10.38	0.07	57.99
K9TR25	Q5781	15.60	16.46	1.00	2	0.7	22	3.8	4.6	1	0.00	0.00	1.22	0.00	0.74
K9TR25	Q5782	19.00	19.60	1.00	3	33.7	848	333	73	11.9	0.18	0.01	14.53	0.04	35.73
K9TR25	Q5783	19.60	21.00	1.00	7	43	956	791	1280	102	0.21	0.16	124.55	0.09	45.59
K9TR25	Q5784	21.00	22.20	1.00	5	54.3	392	841	1320	121	0.08	0.17	147.75	0.09	57.57
K9TR25	Q5785	22.20	23.00	0.95	2	56.6	974	451	99.9	10.5	0.21	0.01	12.82	0.05	60.01
K9TR23	Q5786	5.00	6.10	1.00	8	54.7	849	677	167	16.9	0.18	0.02	20.64	0.07	57.99
K9TR23	Q5787	6.10	7.00	1.00	15	56.8	304	838	943	109	0.07	0.12	133.10	0.09	60.22
K9TR23	Q5788	7.00	8.00	1.00	10	41.5	283	687	765	125	0.06	0.10	152.64	0.08	44.00
K9TR23	Q5789	8.00	8.50	0.95	4	62.2	251	865	729	133	0.05	0.09	162.41	0.09	65.94
K9TR23	Q5790	8.50	8.80	1.00	3	154	964	923	234	16.7	0.21	0.03	20.39	0.10	163.27
K9TR23	Q5791	8.80	9.10	1.02	2	59.2	372	586	362	92.2	0.08	0.05	112.59	0.06	62.76
K9TR23	Q5792	9.10	9.60	1.04	3	134	953	565	149	9	0.21	0.02	10.99	0.06	142.07
K9TR22	Q5793	2.00	2.80	1.16	6	33.8	307	263	47.3	2.5	0.07	0.01	3.05	0.03	35.83
K9TR22	Q5794	2.80	3.65	1.00	5	51.7	76	531	346	41.7	0.02	0.04	50.92	0.06	54.81
K9TR22	Q5795	3.65	4.20	1.22	5	33.7	261	330	79.4	8.6	0.06	0.01	10.50	0.04	35.73
K9TR20	Q5796	2.00	2.50	0.78	2	48.5	439	402	123	3.2	0.09	0.02	3.91	0.04	51.42
K9TR20	Q5797	2.50	3.20	1.00	4	23.4	90	564	657	62	0.02	0.08	75.71	0.06	24.81
K9TR20	Q5798	3.20	4.00	1.00	4	71.3	308	552	242	17.7	0.07	0.03	21.61	0.06	75.59
K9TR20	Q5799	7.20	8.25	0.40	5	30.8	223	341	90.6	4.1	0.05	0.01	5.01	0.04	32.65
K9TR20	Q5801	8.25	9.30	0.86	6	27.1	48	478	616	48.9	0.01	0.08	59.71	0.05	28.73
K9TR20	Q5802	9.30	10.40	0.40	5	25.8	263	226	36.6	2.1	0.06	0.00	2.56	0.02	27.35
K9TR21	Q5803	6.68	7.50	0.46	6	160	1340	1090	153	4.4	0.29	0.02	5.37	0.12	169.63
K9TR21	Q5804	7.50	8.60	1.14	12	80.6	283	1130	811	132	0.06	0.10	161.19	0.12	85.45
K9TR21	Q5805	8.60	9.40	0.50	13	55.9	417	967	460	86.2	0.09	0.06	105.26	0.11	59.27
K9TR21	Q5806	9.40	10.80	0.70	17	72.9	188	988	816	117	0.04	0.10	142.87	0.11	77.29
K9TR21	Q5807	10.80	11.56	0.80	7	183	948	602	92.6	4.9	0.20	0.01	5.98	0.07	194.02
K9TR18	Q5808	3.78	4.80	1.05	5	87.7	430	420	39.3	3.1	0.09	0.00	3.79	0.05	92.98
K9TR18	Q5809	4.80	5.84	1.05	6	25.5	111	394	565	27.3	0.02	0.07	33.34	0.04	27.04
K9TR18	Q5810	5.84	7.00	1.10	10	20.1	81	326	493	38.4	0.02	0.06	46.89	0.04	21.31



Trench_ID	Sample_ID	From_m	To_m	Width_m	Weight_Kg	Cs_ppm	Li_ppm	Rb_ppm	Sn_ppm	Ta_ppm	Li2O_%	SnO2_%	Ta2O5_ppm	Rb2O_%	Cs2O_ppm
K9TR18	Q5811	7.00	8.00	0.82	7	33.6	373	446	89.7	12.1	0.08	0.01	14.78	0.05	35.62
K9TR19	Q5812	5.00	6.22	1.10	7	97.1	698	483	45	7	0.15	0.01	8.55	0.05	102.95
K9TR19	Q5813	6.22	7.00	0.80	5	71	231	628	479	119	0.05	0.06	145.31	0.07	75.27
K9TR19	Q5814	7.00	8.00	1.40	5	58.2	215	962	561	67	0.05	0.07	81.81	0.11	61.70
K9TR19	Q5815	8.00	9.00	0.76	7	48.5	250	911	784	71.9	0.05	0.10	87.80	0.10	51.42
K9TR19	Q5816	9.00	9.40	0.80	4	51.1	393	810	687	96.7	0.08	0.09	118.08	0.09	54.18
K9TR19	Q5817	9.54	10.40	0.85	4	222	1000	821	87.7	8.4	0.22	0.01	10.26	0.09	235.36
K9TR19	Q5818	13.00	13.40	0.55	3	203	1130	588	110	10.8	0.24	0.01	13.19	0.06	215.22
K9TR19	Q5819	13.40	13.86	1.10	4	74.1	157	600	529	142	0.03	0.07	173.40	0.07	78.56
K9TR19	Q5821	13.86	15.00	0.90	6	164	793	504	169	20.4	0.17	0.02	24.91	0.06	173.87
K9TR15	Q5822	3.00	3.70	1.00	5	90.9	698	378	70.2	7.2	0.15	0.01	8.79	0.04	96.37
K9TR15	Q5823	3.70	4.50	0.50	6	129	305	972	527	215	0.07	0.07	262.54	0.11	136.77
K9TR15	Q5824	4.50	5.18	0.30	7	84.2	138	816	539	156	0.03	0.07	190.49	0.09	89.27
K9TR15	Q5825	5.18	6.20	0.30	6	154	682	348	19.2	2.2	0.15	0.00	2.69	0.04	163.27
K9TR15	Q5826	19.64	20.74	0.50	5	27.3	336	119	26.1	6.7	0.07	0.00	8.18	0.01	28.94
K9TR15	Q5827	20.74	22.00	0.50	11	92.1	102	963	328	163	0.02	0.04	199.04	0.11	97.64
K9TR15	Q5828	22.00	23.00	0.65	8	147	506	1850	2280	127	0.11	0.29	155.08	0.20	155.85
K9TR15	Q5829	23.00	24.00	0.65	8	198	346	2380	410	95.3	0.07	0.05	116.37	0.26	209.92
K9TR15	Q5830	24.00	25.00	1.20	6	165	540	417	60.3	10.1	0.12	0.01	12.33	0.05	174.93
K9TR17	Q5831	2.40	3.40	0.30	5	81.3	598	335	28.4	3.2	0.13	0.00	3.91	0.04	86.19
K9TR17	Q5832	3.40	4.35	0.50	5	74.1	193	797	335	95.1	0.04	0.04	116.13	0.09	78.56
K9TR17	Q5833	4.35	5.35	0.90	4	47.4	210	645	592	65.7	0.05	0.08	80.23	0.07	50.25
K9TR17	Q5834	5.35	6.35	1.10	6	77.1	357	1230	485	98.4	0.08	0.06	120.16	0.13	81.74
K9TR17	Q5835	6.35	7.35	0.86	7	95.6	829	1290	413	79.1	0.18	0.05	96.59	0.14	101.36
K9TR17	Q5836	7.35	8.30	0.60	5	56.2	310	1020	530	79.1	0.07	0.07	96.59	0.11	59.58
K9TR17	Q5837	8.30	9.30	1.40	5	39.3	553	276	40.7	5	0.12	0.01	6.11	0.03	41.67
K9TR14	Q5838	4.40	5.38	1.20	9	21.8	386	371	54.5	35.7	0.08	0.01	43.59	0.04	23.11
K9TR14	Q5839	5.38	6.00	0.80	8	26.5	83	666	414	48.9	0.02	0.05	59.71	0.07	28.10
K9TR14	Q5841	6.00	7.00	1.05	11	27.3	102	632	411	47.2	0.02	0.05	57.64	0.07	28.94
K9TR14	Q5842	7.00	8.00	0.60	10	50.9	107	1290	957	63.6	0.02	0.12	77.66	0.14	53.96
K9TR14	Q5843	8.00	8.34	1.00	3	37	80	789	692	52.4	0.02	0.09	63.99	0.09	39.23
K9TR14	Q5844	8.34	9.00	0.72	7	42.3	375	371	36.1	1.6	0.08	0.00	1.95	0.04	44.85
K9TR16	Q5845	4.52	5.60	0.28	9	30.5	344	538	302	39.2	0.07	0.04	47.87	0.06	32.34
K9TR16	Q5846	5.60	6.60	1.00	13	20.9	139	458	506	28.1	0.03	0.06	34.31	0.05	22.16
K9TR16	Q5847	6.60	7.60	1.00	12	26.5	85	601	1190	49.8	0.02	0.15	60.81	0.07	28.10
K9TR16	Q5848	7.60	8.60	1.00	10	25	142	307	140	18.5	0.03	0.02	22.59	0.03	26.51



Trench_ID	Sample_ID	From_m	To_m	Width_m	Weight_Kg	Cs_ppm	Li_ppm	Rb_ppm	Sn_ppm	Ta_ppm	Li2O_%	SnO2_%	Ta2O5_ppm	Rb2O_%	Cs2O_ppm
K9TR13	Q5849	2.00	2.64	1.00	7	121	714	495	73.1	4.1	0.15	0.01	5.01	0.05	128.28
K9TR13	Q5850	2.70	3.30	1.00	8	60.8	98	747	283	81.7	0.02	0.04	99.76	0.08	64.46
K9TR13	Q5851	3.30	4.14	0.80	6	91	101	981	767	155	0.02	0.10	189.27	0.11	96.48
K9TR13	Q5852	4.14	5.00	0.50	11	81.1	723	399	118	6.9	0.16	0.01	8.43	0.04	85.98
K9TR11	Q5853	4.18	5.18	0.90	6	35.8	456	462	50	4	0.10	0.01	4.88	0.05	37.96
K9TR11	Q5854	5.18	6.18	0.90	7	18	88	446	780	35.4	0.02	0.10	43.23	0.05	19.08
K9TR11	Q5855	6.18	6.98	1.10	5	35.9	103	685	776	73.1	0.02	0.10	89.26	0.07	38.06
K9TR11	Q5856	6.98	7.90	0.88	5	50.2	448	516	92.1	3.2	0.10	0.01	3.91	0.06	53.22
K9TR12	Q5857	3.10	3.58	0.44	2	42.3	252	273	95.7	5.9	0.05	0.01	7.20	0.03	44.85
K9TR12	Q5858	3.58	4.26	0.58	4	181	752	599	97.6	7	0.16	0.01	8.55	0.07	191.90
K9TR12	Q5859	4.26	5.00	1.10	5	55.3	60	697	145	96	0.01	0.02	117.23	0.08	58.63
K9TR12	Q5861	5.00	5.90	0.94	7	86.5	187	884	349	127	0.04	0.04	155.08	0.10	91.71
K9TR12	Q5862	5.90	7.00	1.06	8	160	872	402	18.1	5.7	0.19	0.00	6.96	0.04	169.63
K9TR09	Q5863	1.00	2.10	0.40	8	39.8	167	358	37.2	2.5	0.04	0.00	3.05	0.04	42.20
K9TR09	Q5864	2.10	3.00	1.00	9	31.6	51	801	410	74.3	0.01	0.05	90.73	0.09	33.50
K9TR09	Q5865	3.00	4.00	0.62	12	36.5	76	662	556	146	0.02	0.07	178.28	0.07	38.70
K9TR09	Q5866	4.00	4.88	1.04	10	56.2	55	650	446	146	0.01	0.06	178.28	0.07	59.58
K9TR09	Q5867	4.88	6.00	1.04	11	34	129	466	14.9	3.6	0.03	0.00	4.40	0.05	36.05
K9TR08	Q5868	6.30	6.90	0.60	3	30.4	92	134	42.6	2.1	0.02	0.01	2.56	0.01	32.23
K9TR08	Q5869	7.00	8.10	1.10	4	68.3	227	414	59.9	15	0.05	0.01	18.32	0.05	72.41
K9TR08	Q5870	8.10	9.00	1.10	4	25	43	379	163	92.1	0.01	0.02	112.46	0.04	26.51
K9TR08	Q5871	9.00	9.32	1.00	2	32.4	72	457	142	101	0.02	0.02	123.33	0.05	34.35
K9TR08	Q5872	9.32	9.92	1.00	3	118	346	664	154	65	0.07	0.02	79.37	0.07	125.10
K9TR08	Q5873	9.92	10.70	0.60	6	45.1	72	542	358	117	0.02	0.05	142.87	0.06	47.82
K9TR08	Q5874	10.80	11.30	0.40	3	40.2	58	615	333	61.9	0.01	0.04	75.59	0.07	42.62
K9TR08	Q5875	11.30	12.20	0.30	4	46.3	172	293	39.7	5.5	0.04	0.01	6.72	0.03	49.09
K9TR07	Q5876	3.00	4.30	1.10	7	162	378	467	72.5	5.4	0.08	0.01	6.59	0.05	171.75
K9TR07	Q5877	4.30	4.70	1.00	4	92.9	132	900	151	77.6	0.03	0.02	94.76	0.10	98.49
K9TR07	Q5878	4.70	5.30	1.00	5	109	401	438	69.8	4.7	0.09	0.01	5.74	0.05	115.56
K9TR06	Q5879	3.50	4.40	0.80	12	40.8	153	348	69.4	10.5	0.03	0.01	12.82	0.04	43.26
K9TR06	Q5881	4.40	5.36	0.50	13	57.7	67	775	291	74.7	0.01	0.04	91.22	0.08	61.17
K9TR06	Q5882	5.36	6.40	0.30	12	37.6	135	358	67.8	9.5	0.03	0.01	11.60	0.04	39.86
K9TR05	Q5883	1.00	2.06	0.70	8	53.4	197	360	46	6.3	0.04	0.01	7.69	0.04	56.61
K9TR05	Q5884	2.06	3.04	0.60	10	49.1	59	852	567	119	0.01	0.07	145.31	0.09	52.06
K9TR05	Q5885	3.04	4.00	0.50	6	65.8	194	329	30.8	9.8	0.04	0.00	11.97	0.04	69.76
K9TR04	Q5886	1.00	1.70	1.50	6	13	102	165	4.3	1.3	0.02	0.00	1.59	0.02	13.78



Trench_ID	Sample_ID	From_m	To_m	Width_m	Weight_Kg	Cs_ppm	Li_ppm	Rb_ppm	Sn_ppm	Ta_ppm	Li2O_%	SnO2_%	Ta2O5_ppm	Rb2O_%	Cs2O_ppm
K9TR04	Q5887	1.70	2.30	1.00	6	25.1	167	236	16.6	2.6	0.04	0.00	3.17	0.03	26.61
K9TR04	Q5888	2.30	3.00	1.00	5	32.4	25	659	595	110	0.01	0.08	134.32	0.07	34.35
K9TR04	Q5889	3.00	4.16	0.80	10	25.9	28	561	556	97.5	0.01	0.07	119.06	0.06	27.46
K9TR04	Q5890	4.16	5.00	0.60	5	39.9	152	447	112	28.1	0.03	0.01	34.31	0.05	42.30
K9TR03	Q5891	11.00	11.92	0.80	5	38.9	95	328	42.4	11.6	0.02	0.01	14.16	0.04	41.24
K9TR03	Q5892	11.92	12.90	1.70	9	38.7	25	795	680	110	0.01	0.09	134.32	0.09	41.03
K9TR03	Q5893	12.90	14.00	1.50	6	34.1	130	296	26	6.5	0.03	0.00	7.94	0.03	36.15
K9TR02	Q5894	2.00	2.86	1.50	4	16.5	52	219	43.1	5.3	0.01	0.01	6.47	0.02	17.49
K9TR02	Q5895	2.86	3.30	0.60	4	17.8	65	306	109	41.1	0.01	0.01	50.19	0.03	18.87
K9TR02	Q5896	3.30	4.00	0.90	3	20.2	81	378	38.8	8.3	0.02	0.00	10.14	0.04	21.42
K9TR01	Q5908	2.20	3.36	0.80	6	48.5	142	225	24.5	1.5	0.03	0.00	1.83	0.02	51.42
K9TR01	Q5909	3.36	4.00	0.85	7	24.4	17	252	2830	55.7	0.00	0.36	68.02	0.03	25.87
K9TR01	Q5910	4.00	5.00	1.15	9	45.5	163	317	242	9	0.04	0.03	10.99	0.03	48.24
K9TR10	Q5897	5.10	6.10	0.90	9	49.9	447	356	43.2	7.8	0.10	0.01	9.52	0.04	52.90
K9TR10	Q5898	6.10	7.00	1.10	6	34.6	60	748	595	71	0.01	0.08	86.70	0.08	36.68
K9TR10	Q5899	7.00	7.80	1.85	6	46	130	727	351	47.1	0.03	0.04	57.51	0.08	48.77
K9TR10	Q5901	7.80	8.70	0.60	11	116	515	449	38.5	3.7	0.11	0.00	4.52	0.05	122.98
K9TR10	Q5902	11.00	12.00	0.27	8	255	619	688	34.8	2.3	0.13	0.00	2.81	0.08	270.35
K9TR10	Q5903	12.00	12.40	1.13	8	71.3	188	516	405	71.7	0.04	0.05	87.55	0.06	75.59
K9TR10	Q5904	12.40	13.40	0.56	8	177	557	434	72.4	9.3	0.12	0.01	11.36	0.05	187.66
K9TR10	Q5905	22.70	23.70	1.44	7	276	692	807	101	8.1	0.15	0.01	9.89	0.09	292.62
K9TR10	Q5906	23.70	24.74	0.87	7	102	161	623	180	115	0.03	0.02	140.43	0.07	108.14
K9TR10	Q5907	24.74	26.00	1.13	5	195	593	504	80.4	2.6	0.13	0.01	3.17	0.06	206.74

