15 April 2026

ASX Announcement

COBRE

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COMMENCEMENT OF 40,000m RESOURCE DRILLING CAMPAIGN

Sierra Atacama, Chile

Following the completion of an earn-in agreement into the Sierra Atacama Project in Northern Chile (see ASX Announcement 12 February 2026), Cobre Limited (**ASX:CBE** or the **Company**) is pleased to announcement the commencement of a major resource drilling programme in parallel to implementing a series of restructuring, upgrading and optimising processes to streamline the existing copper mining operation.

HIGHLIGHTS

Commencement of ~40,000m surface and underground drilling programme designed to:

- Convert the existing NI43-101 Resource to a JORC-compliant Resource & Reserve;
- Expand the resource between known deposits to investigate potential for a larger scale open-pit operation;
- Delineate areas for initial shallow starter pits which will be followed by a larger expansion project;
- Explore and delineate the high-grade mixed zone at the base of the oxide zone, which can provide a significant grade sweetener – the zone includes drill and channel assays that can exceed 10% total copper (CuT). Recent ore samples from the underground mine from this material demonstrate additional precious metal credits, such as the following samples:
  - Sample ***8106-1***: **52.92% CuT**, 148.0 g/t Ag & 0.68 g/t Au
  - Sample ***8106-2***: **51.81% CuT**, 155.8 g/t Ag & 0.57 g/t Au

Commenting on the drill programme, Chief Executive Officer Adam Wooldridge said:

" Cobre is advancing rapidly at Sierra Atacama, with a major 40,000m drilling programme about to commence. The programme is designed to deliver a JORC-compliant open pit resource that will build on the existing NI 43-101 resource base.

" Transitioning the operation from underground to open pit mining has the potential to significantly increase operational scale in a manner better suited to the geometry of the mineralised system. With mineralisation outcropping at surface and existing mining permits already in place, the development strategy contemplates a staged expansion, commencing with a series of starter pits and progressing toward a larger open pit operation that leverages existing infrastructure.

" A key focus of the drilling programme will be extending mineralisation between the currently mined deposits, where historical drilling has already confirmed the presence of additional mineralisation. In addition, delineating higher-grade mineralisation within the mixed zone has the potential to provide a meaningful grade enhancement to both the existing underground operation and any future open pit development."

Sierra Atacama can be a world class deposit

Sierra Atacama is located approximately 50 kilometres Northeast of Antofagasta in Chile's Atacama Desert, one of the world's most established copper mining regions. The project sits near major copper deposits including Marimaca and Mantos Blancos, and benefits from excellent access to ports, roads, power and an experienced local mining workforce. The property covers approximately 10 kilometres by 17 kilometres across 65 mining concessions, with largely unexplored additional exploration ground extending further south.

Commencement of ~40,000m surface and underground drilling programme

Cobre is commencing an extensive drilling campaign consisting of approximately 15,000 metres of reverse circulation ("RC") drilling and 25,000 metres of diamond core drilling, both from the surface and underground. In simple terms, RC drilling uses compressed air to bring rock chips rapidly to the surface for analysis, while diamond drilling cuts cylindrical rock cores that allow geologists to study the rock in fine detail. The new results will be combined with approximately 140 kilometres of historical drilling data and over 7,500 underground rock samples already collected from the mine.

Why This Drilling Matters — Four Key Objectives

1. **Converting the resource to Australian standards.** The project currently has a resource estimate of approximately 110 million tonnes of copper-bearing rock at an average grade of 0.67% total copper, prepared under Canadian reporting standards (NI 43-101). This is classified as a "foreign estimate" under Australian stock exchange rules. The drilling programme will collect the data needed to re-classify this resource under the JORC Code, which is the Australian standard required for ASX-listed companies. Until this conversion is complete, the Company cannot formally rely on the foreign estimate.

2. **Expanding the resource for a potential large open pit.** Copper at Sierra Atacama is found across several distinct zones. Drilling will test the poorly explored gaps between known deposits, with the aim of demonstrating that the copper-bearing rock is continuous enough to support a single, large open pit mine rather than multiple smaller operations. A larger open-pit would deliver significant economies of scale.

3. **Identifying areas for near-term starter pits.** In some areas, copper sits very close to the surface, meaning it can be extracted quickly and cheaply using small open pits. These "starter pits" could begin producing copper relatively soon, supplementing the existing underground mine while the larger open-pit development is planned and permitted.

4. **Exploring high-grade zones with precious metal credits.** At the boundary between the upper (oxide) and deeper (sulphide) mineralisation zones (subhorizontal layers), the mine has encountered exceptionally rich pockets of copper, with grades often exceeding 10% total copper — roughly fifteen times the average resource grade. Recent samples from this zone also contain meaningful amounts of silver (up to 155.8 g/t) and gold (up to 0.68 g/t), which would add value as by-product credits. Drilling will delineate this zone to understand its extent and economic significance.

The Strategic Shift — Underground to Open Pit

Sierra Atacama has historically been mined underground, which limits the tonnage that can be extracted on a daily basis. Because much of the oxide copper sits at or near the surface and extends across wide structural zones, the deposit is well suited to open pit mining — a method that allows far greater volumes to be extracted and processed at lower cost per tonne, allowing extraction of a greater amount of the overall mineralisation. The strategy is to begin with smaller starter pits for near-term production, while progressing engineering and approvals for a larger-scale open pit. Existing mining permits are already in place and requiring notification to the Department, rather than a complete re-application, significantly reducing permitting times and risk.

Existing Infrastructure and Parallel Work Programmes

Sierra Atacama is not a greenfield exploration project. It is an operating mine with extensive existing underground workings, a processing plant that extracts copper through leaching (a chemical dissolution process), and established road access. Alongside drilling, Cobre is undertaking parallel initiatives:

- a high-resolution drone magnetic survey to map underground structures;
- detailed geological mapping of mine tunnels to build a 3D-geological model;
- validation and re-testing of historical data to modern quality standards; and
- metallurgical test work to improve copper recovery rates from oxide material, with planning for processing of transitional material.

Broader Exploration Upside

The current mining area occupies only a small portion of the total property. The broader lease includes at least seven additional prospect areas with little modern exploration, despite evidence of historical mining and visible copper at surface. The property borders extend toward two major deposits (Marimaca and Mantos Blancos), one in development and the other a long term producer, with multiple other copper mines in the surrounding area. While not part of the current programme, these areas represent significant longer-term exploration upside.

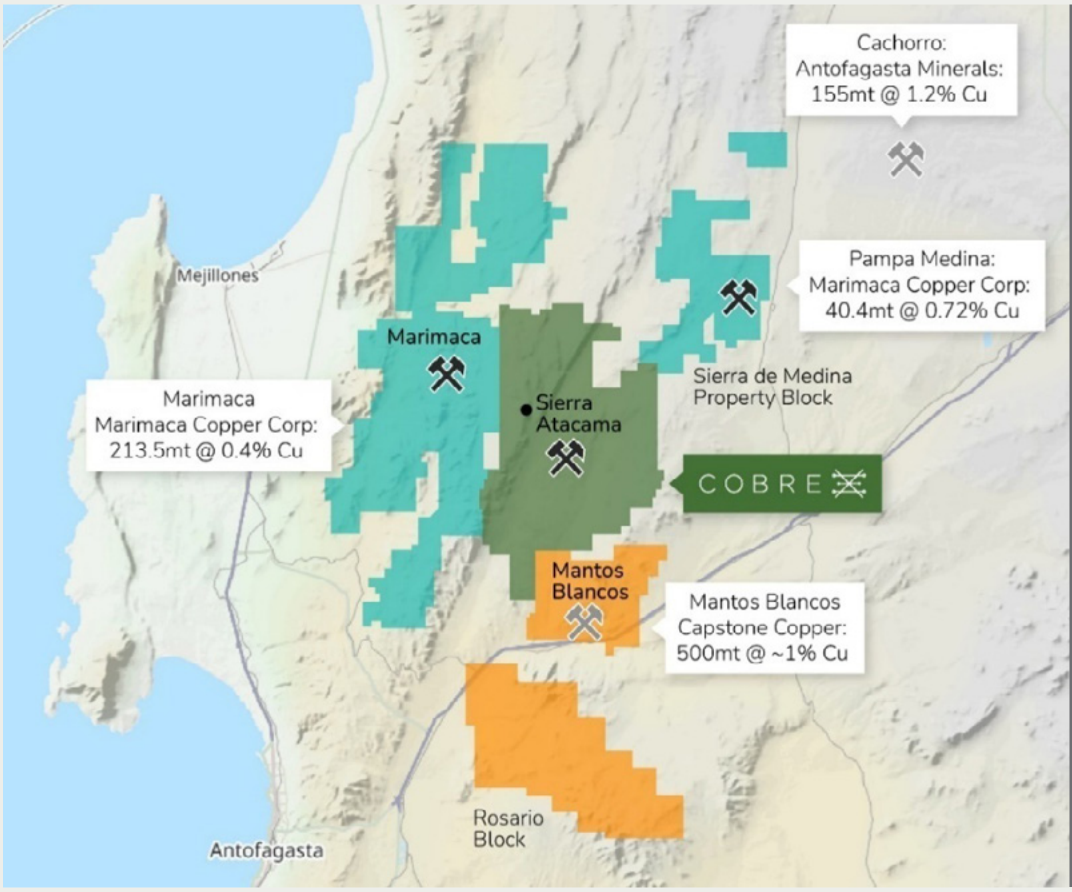


Figure 1. Location of the Sierra Atacama property relative to surrounding deposits. (deposit sizes quoted from company websites)

MAJOR DRILL PROGRAMME TO DEFINE RESOURCES AND UNLOCK VALUE IN UNDERLYING SULPHIDE MINERALISATION

Sierra Atacama, Chile

The Sierra Atacama project offers a massive opportunity for expansion by developing open pits on the shallow oxide mineralisation, allowing extraction of increased tonnage, with greater flexibility than in the current underground developments. The upcoming drill programme will be undertaken in order to convert the current 2025 NI 43-101 Mineral Resource to JORC compliance. In addition, the programme will test for lateral extensions between known copper mineralisation with a view to expanding the resource for a large open pit and developing a reserve for optimised open pit development.

Table 1 | Current NI43-101 Mineral Resource based on an open-pit mine design (see ASX Announcement 12 February 2026)

Classification	Tonnes (mt)	CuT (%)	CuS (%)
Measured	13.986	0.78	0.65
Indicated	44.097	0.67	0.56
Inferred	51.519	0.64	0.53
Measured + Indicated	**58.083**	**0.66**	**0.55**
Measured + Indicated + Inferred	**109.602**	**0.67**	**0.56**

The Mineral Resource Estimate for the Project was previously prepared in accordance with Canadian National Instrument 43-101. This estimate is considered a foreign estimate for the purposes of the ASX Listing Rules as it has not been prepared in accordance with the JORC Code (2012). A Competent Person has not undertaken sufficient work to classify the foreign estimate as a Mineral Resource under the JORC Code, and it is uncertain whether further evaluation will result in a JORC-compliant Mineral Resource. The Company is not relying on this foreign estimate for the purposes of this announcement.

The foreign estimates appear to have been conducted in a reasonable manner, but Cobre and the Competent Person have not independently validated the estimates and the presentation of this information for investors is not to be regarded as the company adopting or endorsing these estimates.

The current programme intends to validate the historical exploration data in order to convert the foreign estimates to estimates prepared in accordance with the JORC Code (2012), including information from the upcoming drilling program.

In accordance with ASX Listing Rule 5.12, Cobre provides additional information related to these foreign estimates in Appendix 1.

In addition to confirmation drilling of the existing NI43-101 Resource, the upcoming programme will test for addition resources between the Chabuca-Rebeca and Roxana trends, to confirm the tenor of mineralisation in this area, which is poorly explored compared to the mineralised trends. Building the resource in this area would support the option for a much larger open pit (see Figures 2 and 3).

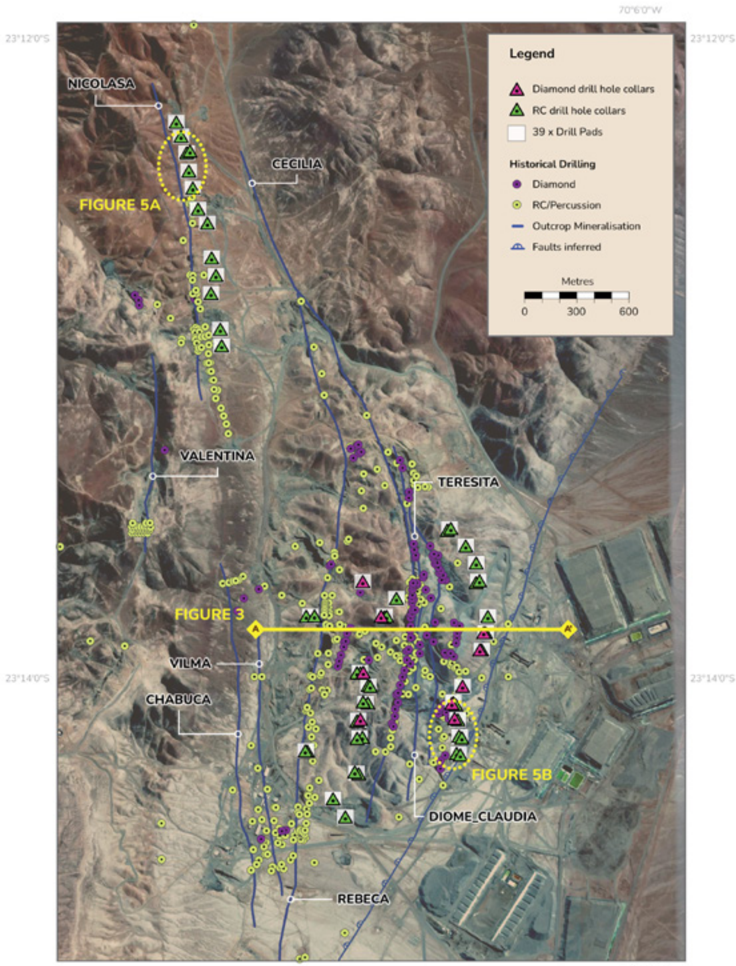
The diamond drill programme will also include a selection of deep diamond holes which, combined with underground drilling, will test vertical and lateral extensions of high-grade chalcocite mineralisation intersected in the deeper part of the Cecelia mine, which forms part of the mixed zone below the current oxide zone. Additional recent samples collected from this zone highlighted the additional potential for associated silver and gold credits. The precious metal credits would further upgrade the potential value of the sulphide ore below the mixed zone.

Examples of notable historical intersections from the deep portion of Cecelia are listed in Table 2 below and illustrated in Figure 4. Selected historical underground drill core photos are provided in Figure 5 to illustrate the style of mineralisation with accompanying assay information.

Table 2 | Notable chalcocite copper intersections from the Cecelia mine including surface and underground drilling as well as grade control composite samples. (see appendix for associated JORC tables).

Hole	From	To	CuT%	Length (m)	Type
ARC27_M5	0	2.5	18.3	2.5	UG DD
M-10	229	234	3.7	5	Surface DD
M13	0	2.113	15.1	2.113	UG DD
RP-01-01	32	36	6	4	UG DD
RP-09-01	198	202	7.5	4	Surface DD
SADDH-46	16	20	5.4	4	UG DD
SADDH-72	0	2	7.5	2	UG DD
SADDH-76	0	2	7.2	2	UG DD
SMRC-066	55	62	2.8	7	UG DD
SDD-13	446.5	448.85	2.8	2.35	Surface DD
M1090220	0	4.2	19.28	4.2	Channel composite
M1090259	0	4.2	15.49	4.2	Channel composite
M1090114	0	4.2	9.41	4.2	Channel composite
M1090125	0	4.2	9.41	4.2	Channel composite
M1090126	0	4.2	7.15	4.2	Channel composite
M1070218	0	4.2	6.48	4.2	Channel composite
M1090167	0	3.7	6.46	3.7	Channel composite
M109077	0	5.5	6.43	5.5	Channel composite
M1070144	0	4.2	6.28	4.2	Channel composite
M107079	0	1.3	5.92	1.3	Channel composite

In addition to potential for a large-scale open pit operation, there are areas where a significant portion of the mineralisation is accessible to rapid open pit extraction, particularly in sectors of the mine where there has been less historical extraction. Two examples of areas where starter pits could focus are illustrated in Figure 6. The upcoming drill programme will infill and delineate resources for these areas as a priority.



Planned RC and diamond holes on satellite imagery

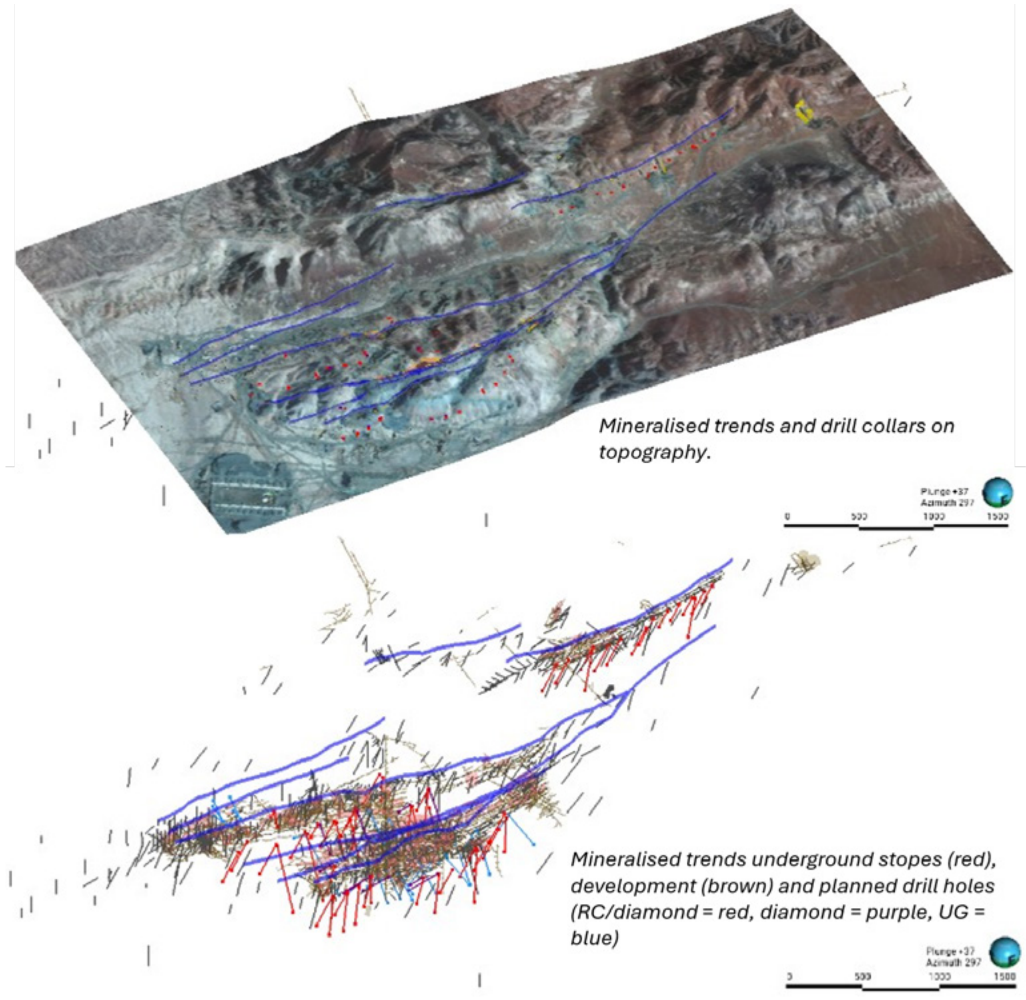


Figure 2 | Planned RC and diamond holes illustrated in plan and oblique 3D views with key mineralised trends highlighted for spatial context. Positions of follow-on figures highlighted.

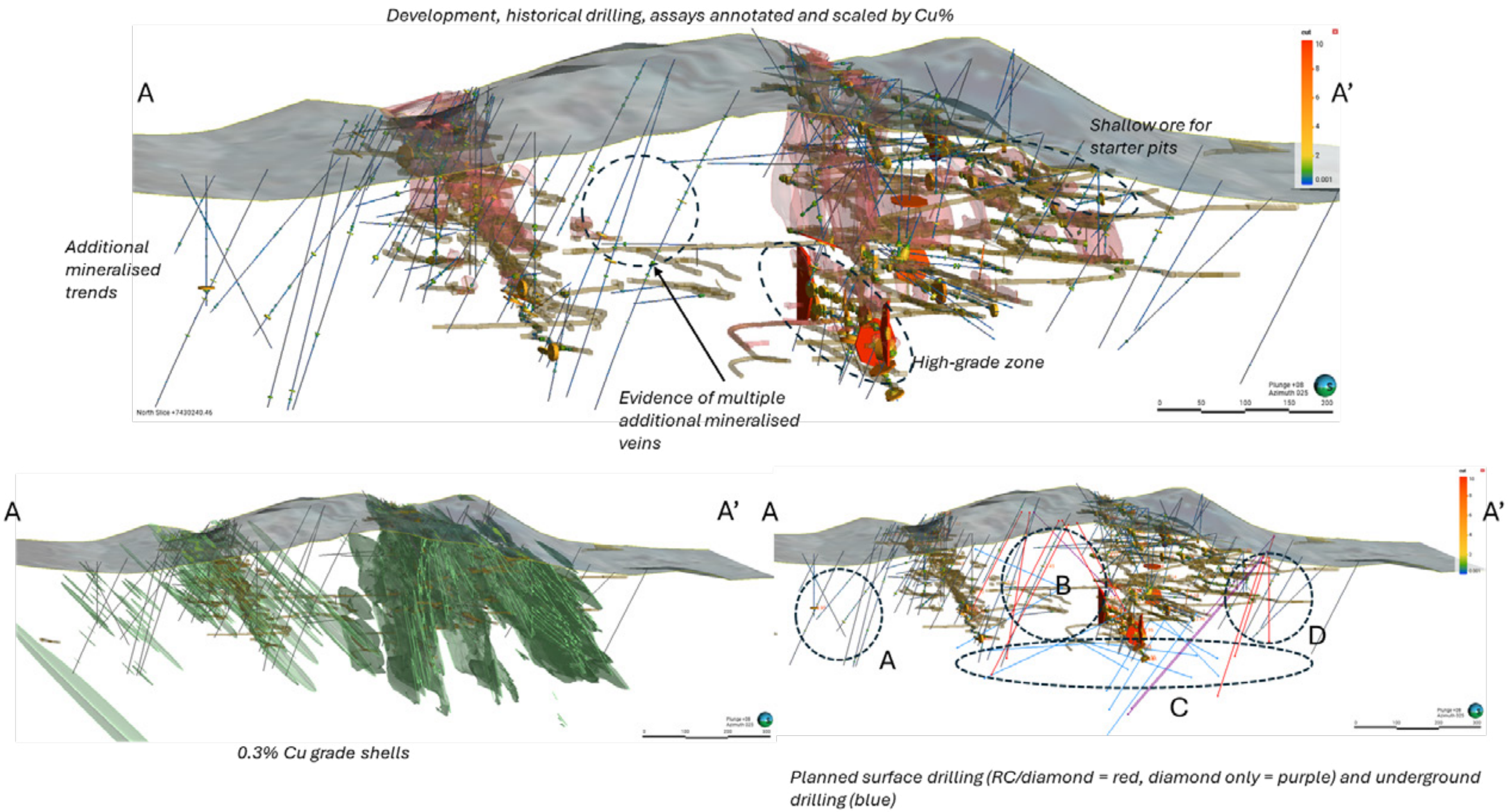


Figure 3 | 200m wide strip sections illustrating the existing underground mine working with key underexplored areas highlighted: **A**: prominent mineralised trend to the west of the primary mining operation; **B**: mineralisation between the main deposits which could allow for a much larger open-pit design; **C**: underexplored high-grade mixed zone which may offer a significant grade sweetener; **D**: shallow mineralisation ideal for an initial starter pit.

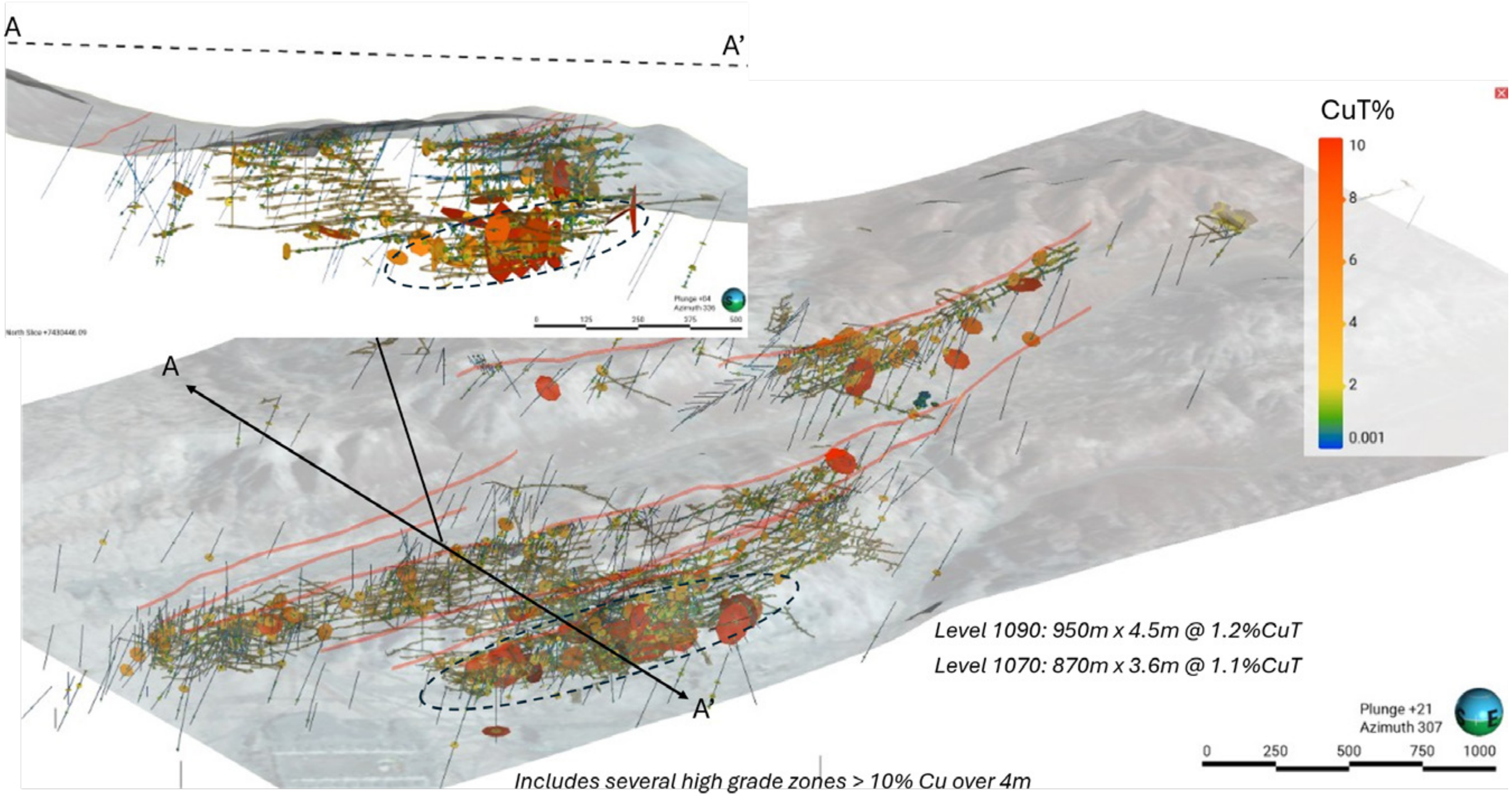


Figure 4 | 3D Oblique and section view of the high-grade zones (orange to red disks). In the Cecelia mine (Section A-A') these zones correspond with secondary chalcocite mineralisation at the base of the oxide zone. This zone is expected to continue at depth into the sulphide zone.

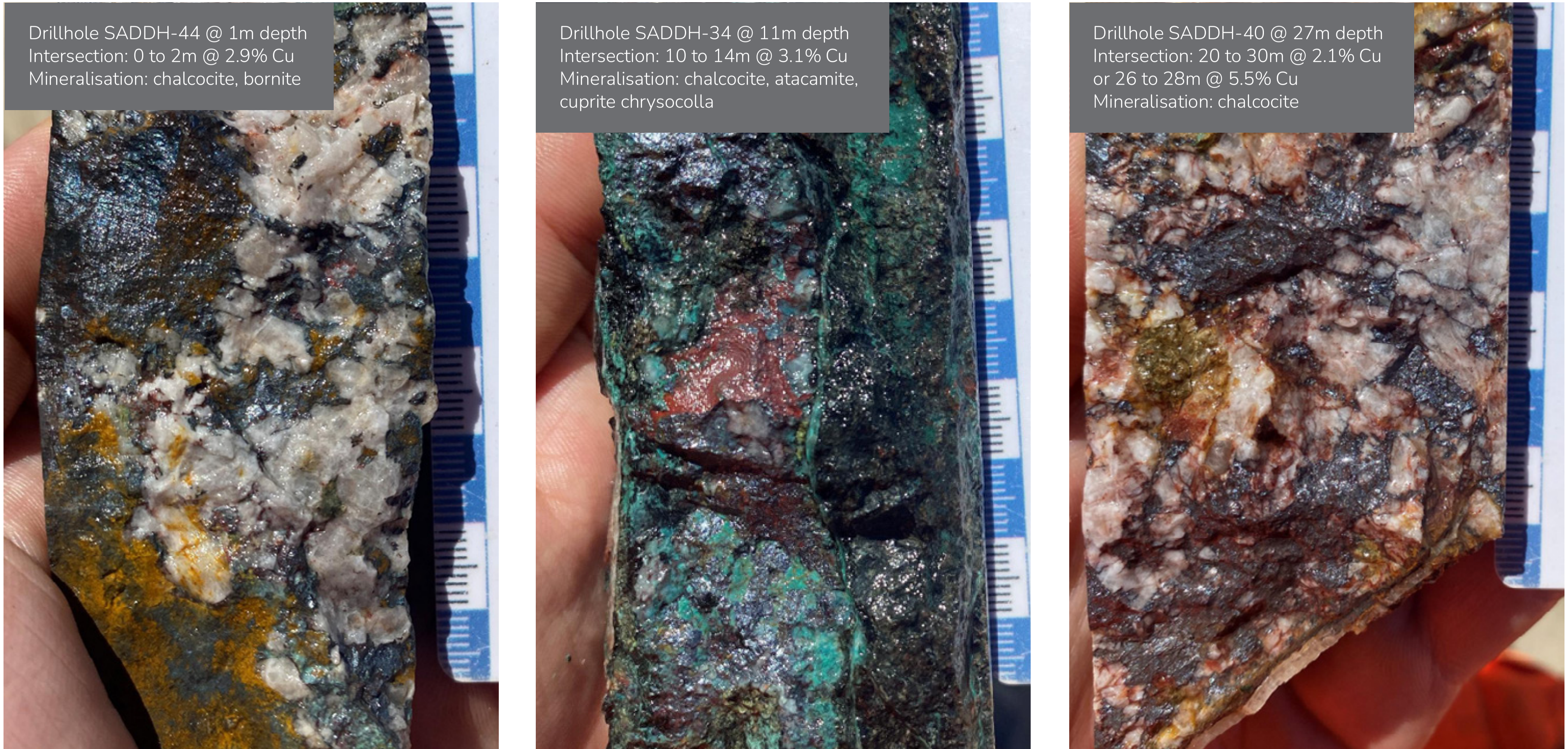


Figure 5 | Selected examples of historical drill intersections through the high-grade mixed-ore zone. Assay results are included for each intersection. Further details are provided in the associated JORC tables in the Appendix.

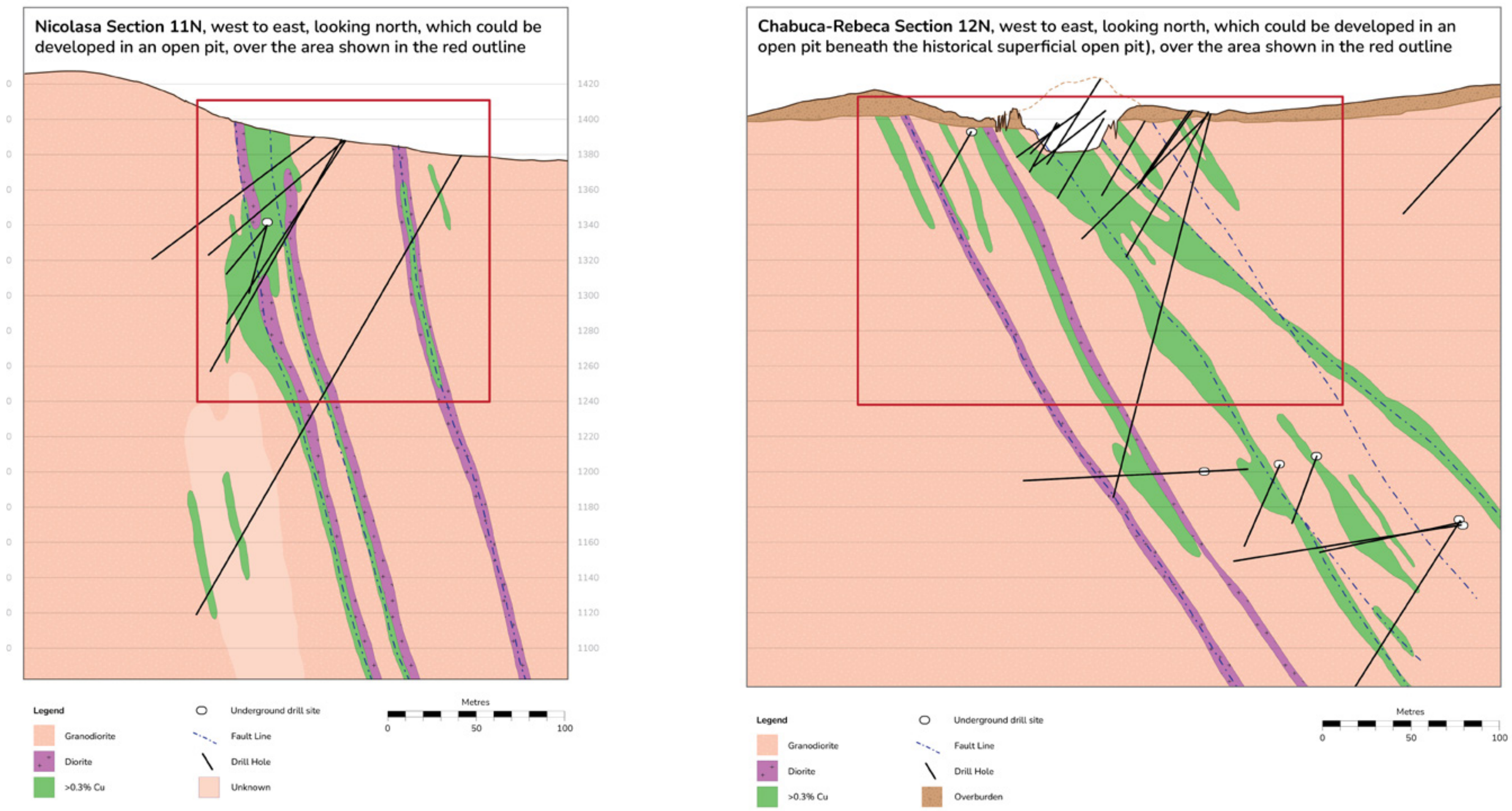


Figure 6 | Section views of shallow mineralisation modified after geological sections. Both areas represent obvious targets for initial open pit mining which would be used to supplement the underground mine until moving to a larger open pit operation. The upcoming drill programme will infill and delineate resources for these areas as a priority.

COMPLIMENTARY PROJECTS

Drone magnetic survey

To assist with mapping of mineralised structures and target drilling, an ultra-high resolution drone magnetic survey has been completed over the mining areas and is currently being processed and interpreted. Mineralisation is spatially associated with diorite intrusives, emplaced within the granodiorite Naguayan batholith that intrudes into andesite volcanics of the la Negra Formation. The batholith is host to copper mineralisation at Sierra Atacama, although the smaller diorite intrusives are noted to have a relationship with mineralisation. The objective is to map structures (areas of demagnetisation) and diorite intrusives (higher magnetic susceptibility), to assist interpretation of the structures controlling mineralisation, to aid drill targeting and resource development. Further magnetic surveys will be considered for the broader property area, once programs in the mine area are completed.

Structural and geological mapping to create a 3D geological model

There are extensive underground workings in the project area, including major drives which extend east-west across the trend of the mineralisation providing an opportunity for systematic detailed mapping of faults and mineralisation. The 3D geological model created from this work programme will provide valuable geotechnical information for resource models as well as a base model for targeting. Mapping and relogging of core has already been completed and modelling will commence shortly.

Data validation for resource estimation

As part of the resource estimation program historical assay data from the 140km of existing drilling and channel samples will be validated by a combination of:

- Re-assaying of original core samples and pulp samples, from historical drilling programs.
- Twinning of historical drill holes and comparison of new and historical assays.
- New drilling, to extend the resource along the trend of known mineralisation, bringing mineralisation into resources along the northern continuation of the Nicolasa trend.

The historical exploration did not utilize QA/QC standards that are consistent with current standards of control and reporting. For this reason, re-assaying and new sampling will be an important part of the resource definition program.

- Evaluation of all shallow mineralisation to establish where open pits will be developed. There are many potential sites for open pit development and a transition from underground to open pit mining.
- Resource Data validation. Re-assaying of historical drill samples and twinning of historical holes with diamond core, to assess historical site laboratory assays with certified independent laboratory standards.
- Drilling program design for resource estimation at multiple sites for potential open pit development.

Samples taken will be analysed in independent commercial laboratories, to compare with historical assay results as a check on the on-site laboratory, which were not subject to any consistent independent third party laboratory assaying.

Development of a mineralogical model

A mineralogical model will be developed to assist with mining and scheduling. Geological observations from logging will be used to build a mineralogical model for the mines, where the primary oxide copper minerals are Atacamite (~59.5% copper) and Chrysocolla (~36.2 % copper). Mine workings in a limited number of places have reached a depth at which chalcocite mineralisation has been reached. Chalcocite can be leached and planned changes to the leach process will enhance recovery from Chalcocite. The model will assist prioritising areas for mining and scheduling, as Atacamite has higher recoveries from leaching.

Metallurgical test work

Current optimised copper leach recoveries on chalcocite dominant ore are typically running in the 50 to 55% range. A series of vessel tests are ongoing to test the potential to re-leach this ore with a salt (chloride) solution. A series of bioleach and oxidant tests are also being undertaken. Initial results from this work are favourable.

BROADER LEASE AREAS

The project includes highly prospective exploration ground which extends from the limits of both the Marimaca and Mantos Blancos deposit properties on the western and southern property borders respectively. To date the property outside the mine area remains largely unexplored with systematic modern methods despite evidence of historical artisanal working and outcropping copper bearing vein systems. Exploration success in the broader property package could add significantly to the resource base of the project, to support higher throughput and longer mine life.

The mining occupies a small area in the north of the much larger property package. There are known mineralised prospects within the property, which have received much less exploration than the mine area. There are seven specific prospect areas adjacent to or further from the mining area. These include Agatha, Geisha, Bonita and la Vaca closest to the mine area and la Gorda, el Loco and Cerro Amarillo further from the mine.

The exploration licences that constitute the southern part of the property package to the southeast of the mining area do not have defined prospects but host significant gravel covered areas which could cover mineralisation.

Although no work is planned in these areas during the initial drilling, these other known prospects and the covered areas will be part of future exploration to define the full potential of the project.

PROJECT BACKGROUND

WORLD CLASS PROJECT LOCATION

The Sierra Atacama Copper Project is located in the II Region of northern Chile, approximately 50km to the northeast of the Antofagasta city, a major mining hub (see Figure 1), close to ports for exporting product and importing consumables.

The mining concessions of the Sierra Atacama Project cover an area approximately 10km in width by 17km in length, comprising a total of 65 mining concessions. The mining concessions occupy the northern part of the total property holdings. The southern part consists of exploration concessions, which extend as far south as the Mantos Blancos mine project area (see Figure 7).

FIRST CLASS REGIONAL LOCATION

The Project site and operational area are located east of the Coastal Range, at an average elevation of approximately 1,200 metres above sea level (masl). The project area is located within a tectonically complex zone, predominantly underlain by volcanic rocks of the La Negra Formation (of Jurassic age, 174–182 Ma) and intrusives belonging to the Naguayán Plutonic Complex (Jurassic, 169.6 Ma) to the west, and the Ercilla Batholith (Jurassic, 180–182 Ma) to the east.

These Jurassic geological units (Figure 7) are emplaced over and through older rock sequences present in the vicinity, including the Rencoret units (Upper Triassic to Sinemurian – lower early Jurassic) and the Sierra del Tigre Formation (Devonian).

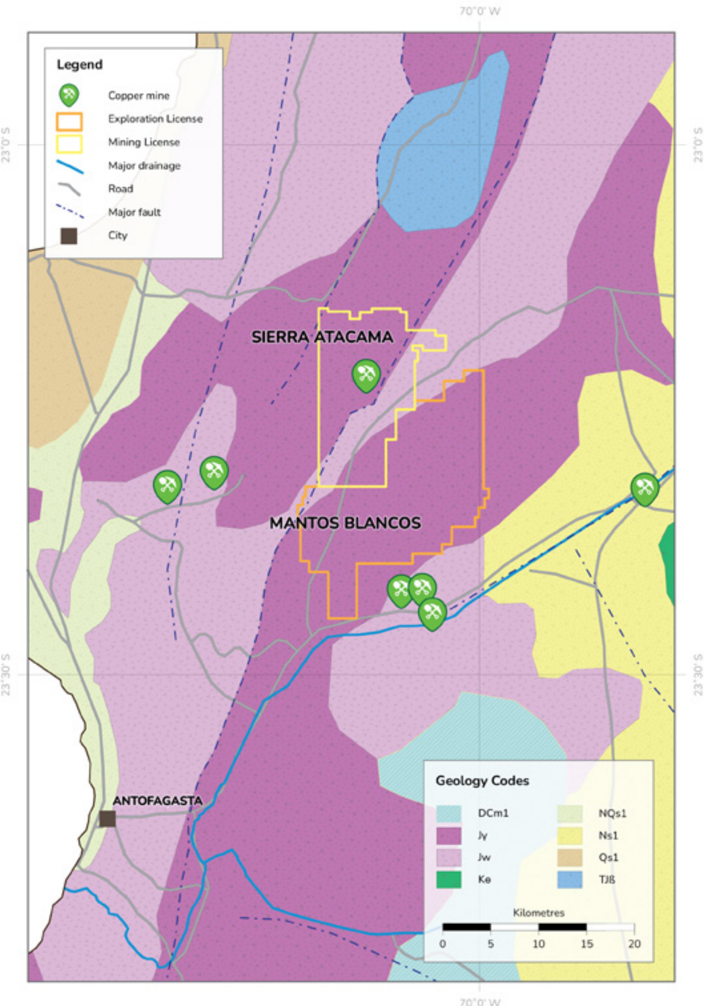


Figure 7 | Regional geological setting

MINERALISATION IS FAVOURABLE BUT REQUIRES FURTHER EXPLORATION

Sierra Atacama is an oxidized copper deposit that is structurally controlled. The dominant copper minerals are, by far, chrysocolla and atacamite. Thick bands of chalcocite have also been identified within larger accumulations of chrysocolla; in some cases, chalcocite rims are partially replaced by cuprite.

The main mineralized intervals appear to be associated with a reactivated fault zone characterized by poor geotechnical quality, withing rocks of high geotechnical quality.

Deeper sulphide mineralisation is known, but has not been part of the historical exploitation. The deeper sulphide mineralisation provides a source of future mineralisation which could be exploited, subject to mining studies. Geological mapping indicates a certain degree of mineralogical zoning within the mineralised structures:

- Specularite–chlorite–epidote assemblages occur at shallow levels (up to 300m below surface), and
- Magnetite–actinolite–epidote assemblages are observed at deeper levels, suggesting the presence of a calcic alteration assemblage.

PROJECT AREA GEOLOGY

The main geological feature hosting the Sierra Atacama Deposit is the Atacama Fault System, which locally trends N30°E with a dip of approximately 75°E. Sierra Atacama is interpreted as an extensional structural system, consistent with a Riedel-type shear model. Therefore, mineralization is not hosted in simple veins, but rather in structural corridors that act as conduits for mineralizing fluids.

The mine area can be divided into three distinct zones, each displaying marked geological differences that influence the distribution of copper mineralization. From east to west, these are the: Roxana, Chabuca-Rebeca and Nicolasa sectors (Figure 8).

Nicolasa

The Nicolasa Sector is located in the northwestern portion of the mining area, where vein-like structures are hosted within intrusive rocks of the Naguayán Batholith. The Nicolasa Fault-Vein (N–S trending/subvertical) represents a fracture system that formed open structural traps favourable for the emplacement of mineralized bodies. This structure extends over approximately 3,000 metres, of which only 1,500 metres in the southern portion have been historically exploited.

Chabuca-Rebeca

This fault-vein structure was extensively mined in the past and, as a result, is the area with the most comprehensive geological information, supported by a large number of drill holes and accessible open workings. All available data indicate that the fault-vein extends approximately 1,200 metres along a NNE strike direction, and is recognized vertically for at least 200 metres along its 70°E dipping plane.

Roxana

The Roxana Zone is hosted entirely within a volcanic environment of high permeability. As a result of tectonic activity in the area, the resulting structural corridors enabled the emplacement of large, north-south elongated mineralized bodies. These same corridors previously allowed the intrusion of tabular dioritic dykes, ranging from 20 to 100 metres in thickness.

Subsequent tectonic reactivation caused brecciation (cataclasite formation) in these dykes, creating favourable conditions for intense copper enrichment and associated hydrothermal alteration.

The most prominent structural zones in the Roxana sector are Cecilia (N–S oriented, subvertical mineralisation), Claudia-Diome, Teresita, and Chabuca.

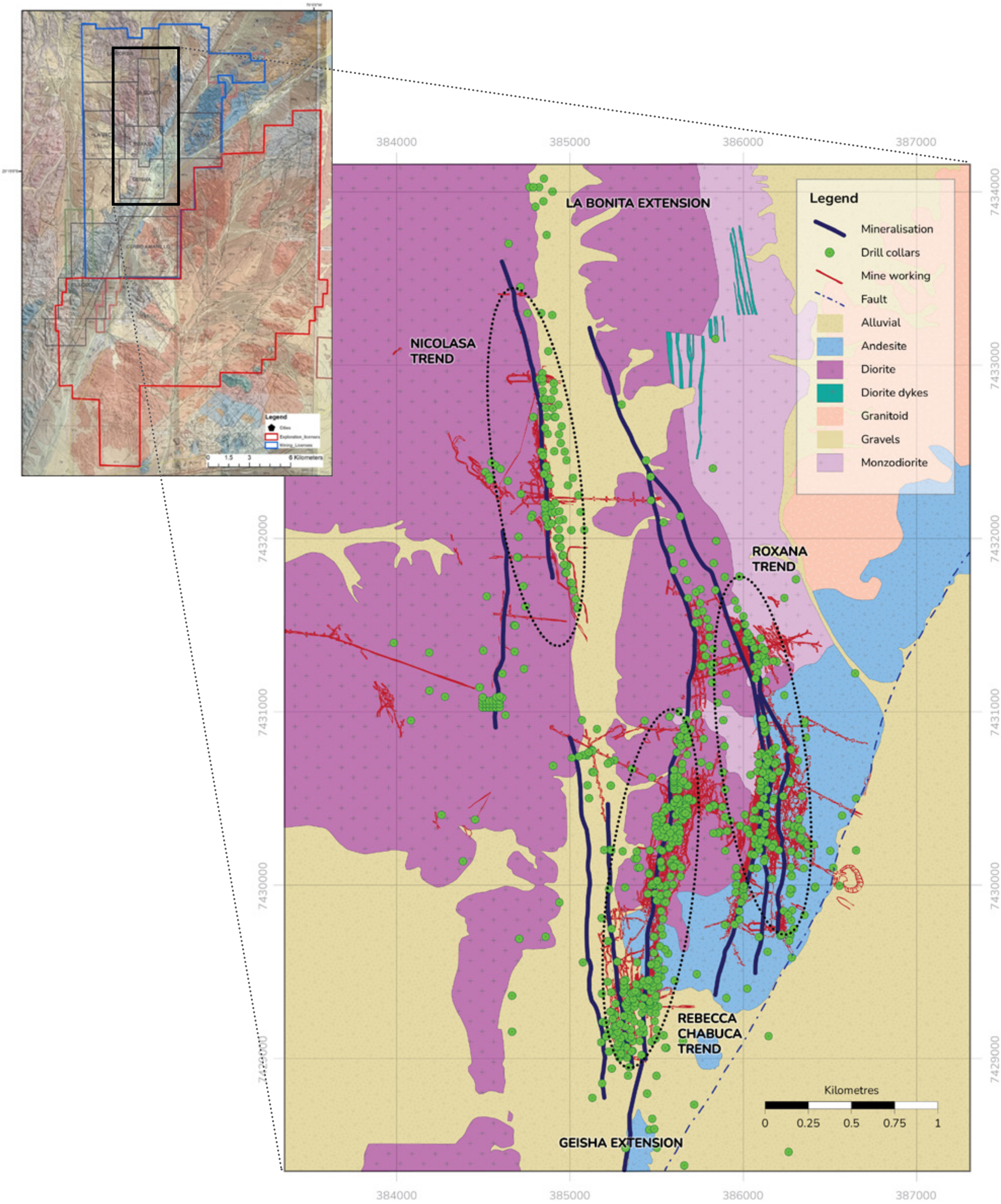


Figure 8 | Local geology with primary mineralised trends highlighted. Left side shows the overall mining properties in the north and exploration properties in the south, with detail of the mining area on the right side

CAUTIONARY STATEMENT ABOUT FORWARD-LOOKING STATEMENTS

This announcement contains certain "forward-looking statements" including statements regarding our intent, belief or current expectations with respect to Cobre's business and operations, market conditions, results of operations and financial condition, and risk management practices. The words "likely", "expect", "aim", "should", "could", "may", "anticipate", "predict", "believe", "plan", "forecast" and other similar expressions are intended to identify forward-looking statements. Indications of, and guidance on, future earnings, anticipated production, life of mine and financial position and performance are also forward-looking statements. These forward-looking statements involve known and unknown risks, uncertainties and other factors that may cause Cobre's actual results, performance and achievements or industry results to differ materially from any future results, performance or achievements, or industry results, expressed or implied by these forward-looking statements. Relevant factors may include (but are not limited to) changes in commodity prices, foreign exchange fluctuations and general economic conditions, increased costs and demand for production inputs, the speculative nature of exploration and project development, including the risks of obtaining necessary licences and permits and diminishing quantities or grades of reserves, political and social risks, changes to the regulatory framework within which Cobre operates or may in the future operate, environmental conditions including extreme weather conditions, recruitment and retention of personnel, industrial relations issues and litigation.

Forward-looking statements are based on Cobre's good faith assumptions as to the financial, market, regulatory and other relevant environments that will exist and affect Cobre's business and operations in the future. Cobre does not give any assurance that the assumptions will prove to be correct. There may be other factors that could cause actual results or events not to be as anticipated, and many events are beyond the reasonable control of Cobre. Readers are cautioned not to place undue reliance on forward-looking statements, particularly in the current economic climate with the significant volatility, uncertainty and disruption caused by the COVID-19 pandemic. Forward-looking statements in this document speak only at the date of issue. Except as required by applicable laws or regulations, Cobre does not undertake any obligation to publicly update or revise any of the forward-looking statements or to advise of any change in assumptions on which any such statement is based. Except for statutory liability which cannot be excluded, each of Cobre, its officers, employees and advisors expressly disclaim any responsibility for the accuracy or completeness of the material contained in these forward-looking statements and excludes all liability whatsoever (including in negligence) for any loss or damage which may be suffered by any person as a consequence of any information in forward- looking statements or any error or omission.

Competent Person Statement

The information in this announcement that relates to Exploration Results, Exploration Targets and Resources has been prepared by Mr Murray Brooker (AIG #3503; RPGEO # 10,086), of Hydrominex Geoscience Pty Limited. The information in the market announcement is an accurate representation of the available data and studies for the project referred to in the announcement.

Mr Brooker, who is an independent geological consultant to Cobre, is a Member of the Australian Institute of Geoscientists, (AIG), and has sufficient experience relevant to the style of mineralisation and type of deposit under consideration and to the activity he is undertaking to qualify as the "Competent Person" as defined in the 2012 Edition of the Australasian Code for Reporting Exploration Results, Mineral Resources and Ore Reserves. Mr Brooker consents to the inclusion in the announcement of the matters based on this information in the form and context in which it appears. The announcement is based on and fairly represents information and supporting documentation prepared by the competent person.

Mr Brooker has undertaken a site visit and inspected the existing operation, core yard and sample storage. Additional visits have been undertaken by Cobre CEO Mr Adam Wooldridge,who was assisted by mining engineers Luke Bryan (Novoco Consulting) and Ben Wilson (Unicorn Consulting) .

Mr Murray Brooker consents to the inclusion in the report of the matters based on his information in the form and context in which it appears.

APPENDIX 1
Additional Technical Information Relating to Foreign Estimate

ASX Listing Rule 5.12

The Project mineral resources are classified as a 'foreign estimate' as defined in Chapter 19 of the ASX Listing Rules. Additional information is detailed in the table below.

ASX Listing Rule	ASX Explanation/requirement	Commentary
5.12.1	The source and date of the historical estimates or foreign estimates.	■ The resources and reserve are from the NI 43-101 report with an effective date of 15th August, 2025, with the report titled "*NI 43-101 Technical Report Sierra Atacama Copper Project, Antofagasta, IInd Region, Chile.*" prepared by Geoinvest Limitada of Santiago, Chile, with primary author Mr Sergio Alvarado Casas, R.M.
5.12.2	Whether the historical estimates or foreign estimates use categories of mineralisation other than those defined in Appendix 5A (JORC Code) and if so, an explanation of the differences.	■ The owner of the Sierra Atacama project is not a company listed on a Canadian stock exchange. However, the NI 43-101 report format is widely used for the documentation of exploration and mining project data in the Americas. ■ While not a JORC-compliant resource the categories of mineralisation reported under the Canadian NI 43-101 standard are similar and comparable resource and reserve categories to the JORC (2012) categories.
5.12.3	The relevance and materiality of the historical estimates or foreign estimates to the entity.	■ Cobre and the CP consider these foreign estimates to be material for the company, as the project is an operating copper mine, with a long history of operations. The estimates provide a general quantification of the size of the project and the potential for larger scale open pit development, compared to historical underground and open pit operations.
5.12.4	The reliability of the historical estimates or foreign estimates, including by reference to any of the criteria in Table 1 of Appendix 5A (JORC Code) which are relevant to understanding the reliability of the historical estimates or foreign estimates.	■ The historical estimate appears to have been conducted with a reasonable technical basis by the authors (Geoinvest) in 2025. Some of the estimates were entirely based on modelling by Geoinvest. Some of the estimation is believed to have been based on models developed by the operator Sierra Atacama. ■ The available information meets most JORC Table 1 requirements, with the availability of collar and survey data, geological logs, assay data and consultants reports regarding data collection and estimation. ■ The QA/QC of analytical samples was not consistent with what would be considered current best practice, with historical assaying not accompanied by standards, field duplicates and blanks. This would be a focus of future planned work.

ASX Listing Rule	ASX Explanation/requirement	Commentary
5.12.4 **continued**	The reliability of the historical estimates or foreign estimates, including by reference to any of the criteria in Table 1 of Appendix 5A (JORC Code) which are relevant to understanding the reliability of the historical estimates or foreign estimates.	▪ Analyses are predominantly for total copper. The mining operation is in the oxidised to mixed portion of mineralisation, overlying a deeper sulphide zone. A general conversion factor has been used for the relationship between total copper and soluble copper, which can be extracted and processed in the SX-EW plant. ▪ Specific gravity data is not available from cores and the estimate has used an average value across all blocks (2.74 g/cc). ▪ The deposit is clearly described as structurally controlled and vein-style at a conceptual level, with mineralisation associated with fault zones and structural corridors rather than simple disseminated geometry. However, this geological interpretation is not fully carried through into the grade block model implementation. The estimation domains are primarily defined by grade shells, and the interpolation is performed using Ordinary Kriging within orthogonal, non-rotated block models. As a result, while the geology is described as vein-style, the resource model itself is not implemented as a truly structure- or vein-controlled model. in structurally controlled systems, one would normally expect clearer documentation of how structures influence domains, search orientations, or estimation strategy. ▪ The report does document an open pit optimisation step: Chapter 15.4 states that pit optimisation was carried out in Whittle for the Nicolasa and Chabuca–Rebeca/Roxana sectors, using the validated block models and the economic/geotechnical parametres in Table 15-2, with results reported at revenue factor 1.0 (Figures 15-4 and 15-5). However, the documentation reads as an optimised shell summary rather than a fully transparent mine design and method-selection trade-off, which limits how confidently a reader can rely on the open pit conclusion without seeing the underlying design/assumption set in more detail. A complete mine design will be undertaken as part of the next stage of work by Cobre.

5.12.5	To the extent known, a summary of the work programs on which the historical estimates or foreign estimates are based and a summary of the key assumptions, mining and processing parametres and methods used to prepare the historical estimates or foreign estimates.	▪ To the extent known to the Company, the historic reports indicate the following activities occurred on the properties, contributing to the estimation of the foreign resource. The project owner:
		  ▫ Carried out extensive drilling from surface, although a significant portion of this is reverse circulation drilling.
		  ▫ Carried out extensive underground channel sampling.
		  ▫ Carried out extensive surface trenching and sampling.
		  ▫ Has mined the deposit extensively in underground and open cut workings.

ASX Listing Rule	ASX Explanation/requirement	Commentary
5.12.5 **continued**	To the extent known, a summary of the work programs on which the historical estimates or foreign estimates are based and a summary of the key assumptions, mining and processing parametres and methods used to prepare the historical estimates or foreign estimates.	▪ The estimation is believed to be based on definition of a 0.4% Cu cut-off for copper that has been determined by the economic processing of material extracted from the mines, using actual mining costs. ▪ The resource estimate does discount past production from workings. ▪ The estimation was undertaken in Leapfrog software, using ordinary kriging. ▪ Mineralisation consists of mostly acid soluble oxide mineralisation, with metallurgical testwork indicating coper recoveries of 72% and an average CuS (soluble) to CuT (total) of 0.83. ▪ The Mineral reserve calculation utilises an open-pit mine plan considering metallurgical rates, geotechnical constraints and projected operating costs provided by the previous project owner.
5.12.6	Any more recent estimates or data relevant to the reported mineralisation available to the entity.	▪ At the date of this announcement the foreign estimates documented in the August 2025 NI 43-101 report have not been superseded by any later estimates. No more recent estimate has been provided to the company.

5.12.7	The evaluation and/or exploration work that needs to be completed to verify the historical estimates or foreign estimates as mineral resources or ore reserves in accordance with Appendix 5A (JORC Code).	▪ The company is currently undertaking an evaluation of the data available, with the aim of verifying the foreign estimate as Mineral Resources and to define the subsequent steps to improve the understanding regarding the definition of Mineral Reserves. Activities planned include the following:
		  ▪ Validation of the location of a portion of the historical drillholes with high precision GPS and downhole surveying equipment to check the dip and azimuth of holes.
		  ▪ Relogging of a portion of historical drillholes.
		  ▪ Reassaying a portion of the historical assays, including soluble and total copper and other potentially economic and deleterious elements (including for gold).
		  ▪ Use of standards, field duplicates and blanks as part of the re-assaying program.
		  ▪ It is likely that twin hole drilling of a portion of the original holes in the deposit will be required to verify the historical work and estimate in accordance with Appendix 5A (JORC Code).
		  ▪ The geological models will be evaluated with the validation information and modified as necessary.
		  ▪ At this stage Cobre would like to re-assess the potential open pit design in the current NI43-101 report against all existing underground mine working infrastructure and replace the simple reserve estimate with a thorough planned pit shell which accounts for geotechnical and practical design aspects etc. This will provide a more robust estimate.

ASX Listing Rule	ASX Explanation/requirement	Commentary
5.12.8	The proposed timing of any evaluation and/or exploration work that the entity intends to undertake and a comment on how the entity intends to fund that work.	■ Evaluation work will commence in 1Q26 and continue through 2026, to produce a JORC estimate for Mineral Resources and Mineral Reserves. ■ A new reserve calculation will be undertaken following completion of an updated JORC compliant Mineral Resource Estimate expected around Q4 2026. ■ The company will fund this initial validation and exploration work from existing funds. Additional funds will be raised as required, in compliance with listing rules, its Constitution, market conditions and appropriate shareholder approval in order to undertake additional drilling and geological evaluation.
5.12.9	A cautionary statement proximate to, and with equal prominence as, the reported historical estimates or foreign estimates stating that: the estimates are historical estimates or foreign estimates and are not reported in accordance with the JORC Code; a competent person has not done sufficient work to classify the historical estimates or foreign estimates as mineral resources or ore reserves in accordance with the JORC Code; and it is uncertain that following evaluation and/or further exploration work that the historical estimates or foreign estimates will be able to be reported as mineral resources or ore reserves in accordance with the JORC Code.	■ The company cautions that the NI 43-101 estimates are not reported in accordance with the JORC Code (2012). A competent person has not yet completed sufficient work to classify the NI 43-101 Estimates as JORC (2012) Code compliant Mineral Resources and Mineral Reserves. It is uncertain that following evaluation and or further exploration work that the NI 43-101 Estimates will be able to be reported as Mineral Resources or Mineral Reserves in accordance with the JORC Code. ■ No information has come to the attention of the Company that causes it to question the accuracy or reliability of the NI 43-101 Estimates, but the company has not independently validated these estimates and the models on which they are based and therefore the company and CP are not to be considered to be reporting, adopting or endorsing these estimates in the Ni 43-101 report.
5.12.10	A statement by a named competent person or persons that the information in the market announcement provided under rules 5.12.2 to 5.12.7 is an accurate representation of the available data and studies for the material mining project. The statement must include the information referred to in rule 5.22(b) and (c).	■ Mr Murray Brooker, Independent consultant to Cobre is the Competent Person for this announcement. ■ “The information in this announcement that relates to historical exploration reporting and foreign non-JORC resources has been prepared by Mr Murray Brooker . The information in the market announcement provided under rules 5.12.2 to 5.12.7 is an accurate representation of the available data and studies for the material mining project and the information referred to in rule 5.22(b) and (c).”

APPENDIX 2
JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	▪ Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. ▪ Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. ▪ Aspects of the determination of mineralisation that are Material to the Public Report. ▪ In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1m samples from which 3kg was pulverised to produce a 30g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	▪ Drilling consisted of a combination of Reverse Circulation (RC) and diamond drillholes. With a total of 1471 drillholes in the mine area of the project. 642 of the pre-2021 drillholes are stored in sheds on site. ▪ Much of the historical drilling was down the hole (believed to be open hole) hammer sampling (44.8%) of samples, with face sampling reverse circulation (31.1%); underground channel samples (16.7%) and diamond drilling (7%). ▪ Underground sampling consisted of chipped channels along the advancing faces of drives over variable sample lengths. ▪ Mineralised structures are interpreted to be generally steeply dipping and drillholes were designed to drill across the mineralised structures. ▪ Underground samples were taken along drive faces, generally at a high angle to the mineralisation, although this depends on the orientation of the different underground workings with respect to the mineralisation. ▪ The mineralisation is predominantly oxide mineralisation to the depth drilled, and a relatively high portion of this mineralisation is acid soluble (CuS), as distinguished from the total copper content (CuT). ▪ Drill core and RC drilling has been conducted in different drilling campaigns, with differences between campaigns. ▪ It is not clear how drill core was historically split for all of the holes, but observations of core trays and discussions with staff on site suggest they were predominantly split using a hydraulic pressure splitter. ▪ Assays were typically 2m assays, though thicknesses vary between approximately 1 and 3m long, depending on mineralisation and core recovery and sample type. ▪ Samples quoted in the text of the current announcement were selected from the current mining operation with a view to testing for potential associated precious metals.

Criteria	JORC Code explanation	Commentary
Drilling techniques	▪ Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	▪ Diamond drill holes are believed to have been predominantly HQ core diameter, with NQ diameter, depending on the hole depth and condition. ▪ It is believed triple tubes were not always used in the drilling, as core was generally highly competent. ▪ RC drilling was conducted. The date of the drilling relates to the type of bit that was used with the RC drilling. ▪ Approximately 76% of drilling intervals comes from reverse circulation (RC) and conventional air methods.
Drill sample recovery	▪ Method of recording and assessing core and chip sample recoveries and results assessed. ▪ Measures taken to maximise sample recovery and ensure representative nature of the samples. ▪ Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	▪ Drill cores were recovered to surface and placed in core boxes, stored in core racks and on pallets. Core trays were labelled with hole and depth intervals, allowing identification of holes and core intervals. ▪ Core recovery was noted and is generally high, due to the compact nature of the intrusive to volcanic host rock. Samples were sent for analysis to different laboratories over the history of the project. ▪ It is not clear whether there is a relationship between core recovery and copper grade. Sample bias could conceivably have happened, as oxide copper is present on fracture surfaces and could be broken into smaller pieces during sampling for analysis using a hydraulic splitter. This will be an area of additional evaluation for historical drill core.
Logging	▪ Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies. ▪ Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. ▪ The total length and percentage of the relevant intersections logged.	▪ Core and RC drill chips have been geologically logged for a description of the lithology and mineralisation. ▪ Underground rock chip samples were described for lithology and mineralisation. ▪ Descriptions are considered sufficient to support the resource estimate and mining studies. ▪ Logging is generally qualitative. ▪ The total length of drilling is recorded as 149,121 metres. ▪ Simple lithological logs of drill holes were prepared during the drilling process. This information was collated in excel spreadsheets and a database.

Criteria	JORC Code explanation	Commentary
Sub-sampling techniques and sample preparation	▪ If core, whether cut or sawn and whether quarter, half or all core taken. ▪ If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. ▪ For all sample types, the nature, quality and appropriateness of the sample preparation technique. ▪ Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. ▪ Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/ second-half sampling. ▪ Whether sample sizes are appropriate to the grain size of the material being sampled.	▪ Core was split for assay. Core was split using a core chisel for submission of one half of the core for the 2021 and later activities. 2m samples were collected for the samples from 2021 onward. For more historical samples the procedures are less clear but involved a hydraulic or pressure splitter. ▪ Details of the sample preparation are not certain, due to the historical nature of the activities for many drill holes. ▪ Drill hole orientations appear to have generally intersected mineralisation across the dip of the structure, although intersections do not represent true thicknesses of mineralisation. ▪ Historical quality control procedures were variable and prior to 2021 QA/QC procedures were not in place in drilling and sampling programs. ▪ For activities since 2021 a full range of QA/QC samples were collected, involving blanks, field duplicates, coarse reject duplicates, field and pulp duplicates and certified reference materials. ▪ Given that the descriptions of core recovery generally appear to be acceptable (high recovery) it is likely that sufficient sample was submitted for analysis to produce repeatable results. ▪ Sample sizes were considered appropriate for the mineralisation style.
Quality of assay data and laboratory tests	▪ The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. ▪ For geophysical tools, spectrometres, handheld XRF instruments, etc, the parametres used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. ▪ Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	▪ Samples were analysed for total copper, and in a lesser number of analyses of the same samples were analysed for soluble copper. The drillhole logs include total copper grades (CuT), a limited number of soluble copper grades (representing only 8.2% of the total assays), and lithological descriptions. Consequently most samples do not have soluble copper analyses. Similarly gold and silver were not widely analysed. The copper assays are total Cu analyses, except for the percentage with total and soluble analyses. ▪ Samples were sent to Activation Geological Services SpA (AGS), in Coquimbo, Chile, for analysis of samples from 2021 onwards. AGS holds ISO/IEC 17025 accreditation and participates in international proficiency testing programs (as of the date of samples analysis during 2021. These samples were dried, crushed, milled, pulverised and prepared with four acid digestion). ▪ Statistical evaluations applied included Absolute Mean Percentage Difference (AMPD) for precision and Mean Percentage Difference (MPD) for bias. Batches are rejected if more than one CRM fails (>3 standard deviations) or if duplicate errors exceeded 10% relative difference.

Criteria	JORC Code explanation	Commentary
Quality of assay data and laboratory tests **continued**	▪ The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. ▪ For geophysical tools, spectrometres, handheld XRF instruments, etc, the parametres used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. ▪ Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	▪ Previous sample campaigns were analysed in different laboratories. ▪ For drilling campaigns and trench sampling carried out in other sectors of the Sierra Atacama property, no formal QA/QC process was documented. These datasets lack certified control samples. ▪ Samples quoted in the current report were analysed by ICP:OES and Fire Assay for Au, Pt and Pd. Appropriate blanks and standards were included.
Verification of sampling and assaying	▪ The verification of significant intersections by either independent or alternative company personnel. ▪ The use of twinned holes. ▪ Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. ▪ Discuss any adjustment to assay data.	▪ Cobre personnel have undertaken validation of a portion of the available project data. ▪ More complete verification was carried out by consultants Geoinvest in 2025, included an evaluation of exploration data provided by owner CMSA, covering historical drilling, trenching, underground workings, and surface geological mapping. The information was cross-checked against original field records and geological logs to confirm accuracy and consistency. Geoinvest reported no discrepancies or inconsistencies that they stated could materially affect the interpretation of the mineralized zones or exploration potential. ▪ Only four diamond twinned holes are available for the project. These were undertaken by the company Hudbay during an evaluation of the project in 2012. The holes were not exactly parallel to the original holes, and showed some differences in copper content, which would be expected given the hole separation and the fracture hosted style of mineralisation. Additional twin holes are planned and re-evaluation of these four twinned holes (two of original diamond holes and two of RC holes)will be undertaken. ▪ Data entry procedures are believed to have varied over time.

Criteria	JORC Code explanation	Commentary
Location of data points	▪ Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. ▪ Specification of the grid system used. ▪ Quality and adequacy of topographic control.	▪ Drill collars are available in UTM coordinates. Elevations appear to have been determined by surveying holes. ▪ The location of drillholes and trenches was evaluated by Geoinvest in 2025. ▪ Surveys indicate that for at least the shallower holes downhole surveys are restricted to a single dip and azimuth value and not multiple down hole surveys. ▪ High-resolution surface topography was obtained through drone-based aerial surveys. ▪ Underground voids were presumably surveyed using laser scanning technology (LiDAR).
Data spacing and distribution	▪ Data spacing for reporting of Exploration Results. ▪ Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. ▪ Whether sample compositing has been applied.	▪ Drillholes have variable spacings and depth. ▪ The data spacing and distribution is considered sufficient to demonstrate geological and grade continuity, sufficiently to support resource estimation and the classification applied. ▪ RC samples were collected on a 2m basis for the most recent drilling program. ▪ It is uncertain whether compositing occurred in more historic programs.
Orientation of data in relation to geological structure	▪ Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. ▪ If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	▪ The orientation is generally considered to have been appropriate for the mineralisation, with drilling intended to drill at a high angle across the deposit orientation. ▪ Potential sampling bias will be evaluated in the 3D models in more detail when more detailed assessment of the project is undertaken.
Sample security	▪ The measures taken to ensure sample security.	▪ It is unknown the details of how samples were sent to the assay laboratories from the project.
Audits or reviews	▪ The results of any audits or reviews of sampling techniques and data.	▪ A review of the project data was undertaken by independent consultants Geoinvest in 2025. Geoinvest also undertook the most recent resource estimate.

APPENDIX 2
JORC Code, 2012 Edition – Table 1 continued

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	▪ Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. ▪ The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.	▪ The Sierra Atacama project consists of 65 mining concessions covering an area of ~15,000 ha ▪ The Sierra Atacama project also contains exploration concessions covering an area of ~25,000 ha ▪ The properties are 100% held by the current owner CMSA. ▪ There are no joint ventures or overriding royalties.
Exploration done by other parties	▪ Acknowledgment and appraisal of exploration by other parties.	▪ Exploration has been conducted on the mining concessions by the current and former owners, consisting of trenching, rock chip sampling and drilling.
Geology	▪ Deposit type, geological setting and style of mineralisation.	▪ The deposit shows a variable style, which has elements of manto and IOCG style mineralisation, which are common to the coastal belt area in northern Chile. Mineralisation consists of oxide copper minerals on fractures in the oxide zone with more than 200m of vertical extent, before reaching a zone with chalcocite transitional mineralisation. ▪ There could be a relationship to a deeper porphyry copper style deposit but at this stage this is only a concept and not supported by the available data. Porphyry style mineralisation is known from the Cerro Amarillo prospect south of the mining area.

Criteria	JORC Code explanation	Commentary
Drill hole Information	▪ A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: ▫ easting and northing of the drill hole collar ▫ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar ▫ dip and azimuth of the hole ▫ down hole length and interception depth ▫ hole length. ▪ If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	▪ There is extensive drilling in the project, with 1471 holes known to have been drilled. Coordinates are in UTM zone 19 south, PSAD 1956 Datum. ▪ Holes were surveyed downhole, although the equipment is unknown. Drillhole collar evaluations are recorded in the drillhole collar database. ▪ Drillhole dip and azimuth are variable, but generally towards 270 or 90 degrees. The deepest hole is more than 900m, although most holes are much shallower. ▪ A drill hole collar table is provided below. Coordinates are in UTM zone 19 south, PSAD 1956 Datum. Drill type is UG = underground, RC = reverse circulation (face sampling hammer), DD = diamond core. ▪ A table of significant intersections with a 2% total copper cut-off is provided after the drillhole table. Holes are listed in order of total Cu% x intersection width.

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
008-RC7-01	385334.2	7428899.9	1255.1	290	UG	68	270
008-RC7-02	385499.5	7428900.2	1243.7	228	UG	48	270
009-RC7-01	385340.8	7428949.9	1255.6	310	UG	60	270
010-RC7-01	385411.8	7429015.4	1253.9	330	UG	45	270
010-RC7-02	385413.8	7429015.5	1254.0	310	UG	65	270
011-RC7-01	385552.5	7429062.0	1246.1	400	UG	50	270
011-RC7-02	385554.4	7429062.0	1246.1	426	UG	75	270
011-RC7-03	385355.0	7429041.1	1258.7	306	UG	50	270
011-RC7-04	385222.5	7429038.6	1267.8	210	UG	50	270
012-RC7-01	385492.4	7429112.2	1251.2	360	UG	70	270
012-RC7-02	385404.1	7429099.9	1257.6	146	UG	60	270
013-RC7-01	385498.4	7429162.3	1251.2	290	UG	55	270
013-RC7-02	385427.7	7429148.9	1256.8	138	UG	55	270
014-RC7-01	385488.3	7429212.4	1252.2	310	UG	55	270
014-RC7-02	385205.6	7429202.3	1273.3	180	UG	50	270
014-RC7-03	385408.7	7429199.9	1258.2	316	UG	50	270
015-RC7-01	385495.2	7429262.3	1253.0	280	UG	55	270
016-RC7-01	385508.4	7429300.1	1253.4	260	UG	55	270
017-RC7-01	385493.0	7429345.4	1255.7	290	UG	45	270

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
032-RC7-01	385391.4	7430101.2	1318.8	294	UG	70	270
032-RC7-02	385400.3	7430101.5	1318.8	246	UG	50	270
033-RC7-01	385372.6	7430150.3	1320.7	234	UG	46	270
033-RC7-02	385384.0	7430151.3	1320.1	296	UG	75	270
034-RC7-01	385384.5	7430194.4	1318.0	298	UG	74	270
065-RC7-01	385890.9	7431776.5	1369.5	162	UG	45	250
067-RC7-01	385828.0	7431856.5	1358.6	222	UG	65	255
071-RC7-01	385079.8	7432047.7	1369.1	320	UG	65	270
071-RC7-02	385005.1	7432046.5	1376.0	228	UG	45	270
073-RC7-01	385060.0	7432150.2	1368.6	336	UG	60	270
075-RC7-01	385048.1	7432250.0	1368.6	386	UG	59	270
077-RC7-01	385015.2	7432350.1	1369.9	348	UG	55	270
079-RC7-01	384977.3	7432450.0	1371.2	344	UG	56	270
080-RC7-01	384968.4	7432499.9	1371.8	250	UG	45	270
081-RC7-01	384942.7	7432549.9	1373.9	250	UG	45	270
081-RC7-02	384944.2	7432550.0	1373.5	380	UG	62	270
082-RC7-01	384871.1	7432604.7	1379.3	130	UG	45	270
082-RC7-02	384935.8	7432599.4	1373.8	280	UG	45	270
083-RC7-01	384948.5	7432647.2	1371.7	280	UG	45	270
083-RC7-02	384949.5	7432647.2	1371.6	420	UG	57	270
083-RC7-03	384854.6	7432638.9	1384.0	202	UG	45	270
084-RC7-01	384865.2	7432699.8	1384.1	100	UG	45	270
084-RC7-02	384906.6	7432700.0	1377.1	250	UG	45	270
084-RC7-03	384914.5	7432699.8	1376.4	230	UG	64	270
085-RC7-01	384859.0	7432749.9	1383.5	100	UG	45	270
085-RC7-02	384897.7	7432749.9	1377.1	192	UG	60	270
086-RC7-01	384858.4	7432800.1	1385.3	162	UG	45	270
086-RC7-02	384889.6	7432800.1	1382.5	310	UG	64	270
087-RC7-01	384902.7	7432850.0	1379.2	250	UG	55	270
087-RC7-02	384903.8	7432850.0	1379.1	380	UG	70	270
099-RC7-01	384711.9	7433449.9	1411.9	150	UG	50	270
104-RC7-01	384644.5	7433699.8	1433.3	180	UG	60	270
105-RC7-01	384863.1	7433749.9	1405.8	250	UG	63	270
110-RC7-01	384898.6	7433999.5	1411.8	234	UG	50	270
116-RC7-01	384943.1	7434309.8	1392.4	250	UG	50	270
125-RC7-01	384937.4	7434770.0	1368.5	180	UG	57	270
A-005	385675.0	7430499.9	1343.6	49.5	UG	55	270
A-007	385600.4	7430475.0	1337.4	31.5	UG	60	270
A-008	385625.3	7430474.3	1337.8	49.5	UG	60	270
A-009	385649.9	7430475.1	1338.5	49.5	UG	60	270
A-010	385674.6	7430474.1	1341.0	49.5	UG	55	270

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
A-011	385599.5	7430450.1	1334.8	21	UG	45	270
A-011A	385600.0	7430451.0	1335.0	12	UG	90	360
A-011B	385600.0	7430452.5	1335.0	7.5	UG	45	0
A-012	385626.6	7430450.0	1338.4	30	UG	50	270
A-013	385650.4	7430449.9	1340.5	45	UG	60	270
A-014	385672.9	7430450.0	1342.2	45	UG	75	270
A-016	385624.3	7430425.0	1344.2	30	UG	50	270
A-017	385649.4	7430425.0	1345.4	45	UG	60	270
A-018	385674.7	7430425.2	1346.9	45	UG	75	270
A-019	385650.0	7430399.9	1349.9	45	UG	55	270
A-020	385674.9	7430400.2	1351.9	49.5	UG	85	270
A-021	385650.9	7430375.2	1351.3	45	UG	55	270
A-021A	385650.1	7430375.2	1351.3	10.5	UG	55	270
A-023	385621.5	7430349.8	1351.7	39	UG	70	270
A-025	385628.7	7430326.3	1356.1	49.5	UG	70	270
A-027	385524.9	7430301.0	1317.8	19.5	UG	85	270
A-028	385550.4	7430299.9	1334.4	40.5	UG	75	270
A-029	385575.4	7430299.9	1341.1	39	UG	75	270
A-030	385600.1	7430300.0	1348.6	30	UG	75	270
A-031	385631.7	7430295.7	1359.5	60	UG	75	270
A-032A	385512.6	7430277.5	1321.3	34.5	UG	85	270
A-033	385549.6	7430275.1	1336.4	69	UG	75	270
A-034	385573.4	7430274.8	1340.6	69	UG	75	270
A-036	385624.6	7430276.7	1358.7	60	UG	75	270
A-043	385624.7	7430251.4	1360.1	67.5	UG	60	270
A-083	385550.7	7430450.1	1331.5	34.5	UG	60	270
A-084	385575.1	7430449.8	1332.4	39	UG	60	270
A-087	385544.0	7430424.1	1329.9	34.5	UG	60	270
A-088	385494.2	7430395.3	1324.9	34.5	UG	60	270
A-089	385523.7	7430400.8	1328.4	34.5	UG	60	270
A-091	385500.7	7430375.2	1325.0	34.5	UG	60	270
A-092	385529.8	7430375.3	1330.8	34.5	UG	60	270
A-093	385494.9	7430350.1	1325.2	34.5	UG	60	270
A-094	385518.7	7430350.5	1328.6	37.5	UG	60	270
A-095	385491.8	7430325.4	1324.4	34.5	UG	60	270
A-096	385525.0	7430320.9	1324.1	81	UG	60	270
A-097	385539.2	7430318.9	1317.6	39	UG	60	270
A-098	385574.7	7430325.4	1341.3	54	UG	60	270
A-099	385599.3	7430325.0	1349.1	55.5	UG	60	270
A-100	385500.4	7430300.0	1323.7	60	UG	60	270
AL-01-01	384449.9	7430376.1	1448.8	150	RC	61	247

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
AL-02-01	384256.7	7430403.5	1449.7	200	RC	67	241
AL-03-01	384079.1	7430947.7	1442.4	200	RC	59	250
C-00	386000.8	7429980.9	1340.3	133.5	UG	48	87
C-01	385958.0	7430000.1	1341.2	106.5	UG	48	88
C-01A	385956.2	7430000.1	1341.0	120	UG	62	276
C-01B	385919.7	7429957.9	1331.1	120	UG	55	235
C-02	385957.4	7430049.9	1349.3	140	UG	55	83
C-02A	385966.7	7430049.8	1349.4	127.5	UG	73	88
C-03	385956.8	7430097.9	1361.9	142	UG	53	89
C-04	386119.8	7430150.1	1353.9	97.5	UG	24	265
C-04A	386121.9	7430152.9	1354.1	121	UG	90	360
C-05	386094.3	7430199.8	1357.8	102	UG	42	264
C-06	386121.3	7430250.2	1352.7	110.5	UG	36	266
C-07	386121.1	7430250.3	1353.1	90	UG	5	270
C-07A	386123.8	7430250.4	1352.1	150	UG	90	360
C-08	386117.7	7430300.4	1349.5	106.5	UG	0	266
C-09	386119.7	7430300.6	1348.3	123	UG	39	270
C-10	386122.6	7430349.8	1347.6	88.5	UG	37	268
C-10A	386124.1	7430350.0	1347.3	148.5	UG	90	360
C-11	386132.0	7430400.0	1351.2	111	UG	0	272
C-12	386133.4	7430400.1	1350.0	99	UG	34	268
C-13	386121.2	7430449.8	1356.2	72	UG	3	269
C-13A	386123.8	7430450.2	1354.7	85.5	UG	38	264
C-14	386125.3	7430450.2	1354.4	103.5	UG	90	360
C-15	386117.1	7430499.9	1371.1	96	UG	21	270
C-16	386173.8	7430500.3	1348.5	129	UG	28	271
C-16A	386174.6	7430501.3	1348.8	129	UG	17	5
C-17	386122.9	7430550.0	1381.0	70.5	UG	54	270
C-18	386134.1	7430549.9	1379.7	91.5	UG	70	270
C-19	386138.0	7430599.8	1379.5	81	UG	50	270
C-19A	386165.5	7430615.7	1383.0	103.5	UG	49	54
C-1B	385956.2	7429957.9	1331.1	120	UG	55	235
C-20	386142.4	7430649.8	1381.0	82.5	UG	50	270
C-21	386158.2	7430700.7	1383.3	81	UG	50	270
C01-08	386129.0	7430670.0	1214.0	35.5	RC	21	270
C02-08	386129.0	7430670.0	1214.0	45	RC	44	270
C03-08	386138.0	7430694.0	1214.0	55	RC	16	315
C04-08	386138.0	7430694.0	1214.0	60	RC	32	315
C05-08	386103.0	7430761.0	1216.0	31	RC	56	90
C06-08	386103.0	7430761.0	1216.0	40	RC	77	90
C07-08	386115.0	7430604.0	1215.0	67.5	RC	19	250

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
C08-08	386115.0	7430604.0	1215.0	43	RC	40	270
CH01-08	385349.6	7429116.0	1101.9	38.5	RC	60	270
CH02-08	385180.0	7429808.0	1201.0	40	RC	0	270
CH03-08	385220.0	7429677.0	1168.0	40	RC	63	270
CHP-24-09	385307.9	7429375.0	1102.9	35.5	RC	2	94
CHP-25-09	385353.1	7429240.1	1101.9	31	RC	73	83
CHP-26-09	385399.9	7429150.1	1107.3	35.5	RC	66	282
CHP-28-09	385418.9	7429175.0	1110.0	56.5	RC	33	264
CHP-29-09	385420.6	7429174.8	1110.9	56.5	RC	88	332
CHP-32-09	385313.7	7429452.7	1100.7	25	RC	88	231
CHP-33-09	385317.2	7429452.8	1102.3	22	RC	5	96
CHP-35-09	385341.1	7429275.0	1101.9	31	RC	70	268
CHP-36-09	385328.5	7429250.4	1133.4	40	RC	90	0
CHS-1	385338.6	7429105.9	1150.0	35	RC	0	276
CHS-2	385299.0	7429112.5	1150.0	18	RC	0	270
DCH093-001	385219.5	7430701.1	1329.6	290	DD	66	272
DCH093-002	385231.5	7429268.5	1274.8	80	DD	76	272
DCH093-003	385852.5	7430297.5	1362.5	380	DD	69	261
DCH093-004	384682.6	7431496.9	1471.3	286	DD	55	273
DIDTH-02	386251.0	7430873.0	1145.0	35	UG	30	90
DIDTH-03	386236.0	7430873.0	1145.0	40	UG	90	0
DIDTH-04	386224.0	7430843.0	1145.0	30	UG	90	0
DIDTH-05	386244.0	7430843.0	1145.0	30	UG	90	0
DIDTH-06	386268.0	7430843.0	1145.0	30.6	UG	90	0
DTH-EXP-01	384871.8	7432066.0	1403.3	29.5	RC	90	0
DTH-EXP-02	384865.8	7432100.7	1400.8	23.5	RC	90	0
DTH-EXP-03	384857.4	7432141.9	1394.5	20.5	RC	90	0
DTH-EXP-04	384859.7	7432165.4	1390.1	13.5	RC	90	0
DTH-EXP-05	384857.1	7432199.6	1389.4	16	RC	90	0
DTH-EXP-06	384855.4	7432182.7	1389.4	17	RC	90	0
DTH-EXP-07	384874.9	7432084.8	1402.0	20.5	RC	90	0
DTH-EXP-08	384861.7	7432113.4	1399.9	31	RC	90	0
DTH-EXP-09	384863.0	7432153.4	1391.7	14.5	RC	90	0
DTH-EXP-10	384853.0	7432174.2	1389.8	26.5	RC	90	0
DTH-EXP-11	384869.9	7432191.2	1389.3	14.5	RC	90	0
DTH-EXP-12	385494.1	7429448.5	1120.1	34	RC	0	93
DTH-EXP-13	385508.5	7429475.0	1120.8	60	RC	0	86
DTH-EXP-14	385498.6	7429414.0	1120.9	30	RC	0	91
DTH-EXP-15	385975.8	7429850.0	1164.0	60	RC	61	260
DTH-EXP-16	385997.0	7429953.9	1152.3	68.5	RC	58	263
DTH-EXP-17	386049.0	7430176.5	1159.9	45	RC	54	265

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
DTH-EXP-18	385947.9	7429771.5	1170.7	70	RC	55	237
DTH-EXP-19	386001.6	7429995.4	1153.7	55	RC	59	274
DTH-EXP-20	386069.1	7430236.8	1161.4	55.5	RC	56	267
DTH-EXP-21	386081.2	7430653.5	1148.9	70	RC	49	95
DTH-EXP-22	386086.5	7430749.2	1148.0	61	RC	53	86
DTH-EXP-23	386096.0	7430543.9	1152.5	59.5	RC	60	266
DTH-EXP-24	386114.8	7430607.0	1150.7	61.5	RC	60	270
DTH-EXP-25	386087.1	7430697.7	1148.3	62.5	RC	63	97
DTH-EXP-26	385987.0	7429897.6	1157.8	65.5	RC	69	261
DTH-EXP-27	385998.8	7429976.4	1152.5	61	RC	60	275
DTH-EXP-28	385978.3	7429799.1	1171.5	70	RC	38	258
DTH-EXP-29	386087.0	7430374.3	1158.9	61	RC	64	257
DTH-EXP-30	386096.8	7430458.6	1155.7	85	RC	65	253
DTH-EXP-33	385612.8	7430497.8	1344.0	45	RC	36	283
DTH-EXP-34	385627.5	7430495.6	1344.0	52	RC	37	282
DTH-EXP-38	385360.9	7429099.3	1103.6	70	RC	0	270
DTH-EXP-39	385351.4	7429127.4	1104.0	61	RC	0	271
DTH-EXP-40	386325.1	7430264.7	1181.0	46	RC	37	52
DTH-EXP-41	386321.7	7430379.6	1178.8	45	RC	59	262
DTH-EXP-42	386141.9	7430616.9	1258.6	60	RC	36	83
DTH-EXP-43	386145.9	7430699.8	1257.9	65	RC	29	104
DTH-EXP-44	386148.5	7430647.0	1258.9	61	RC	31	98
DTH-EXP-45	386145.2	7430727.7	1258.8	65	RC	38	104
DTH-EXP-46	386143.7	7430757.8	1258.6	61	RC	35	107
DTH-I-1-09	385010.7	7430733.1	1290.4	50.5	RC	20	257
DTH-I-2-09	385048.1	7430741.9	1290.0	50.5	RC	58	257
DTH-I-3-09	385074.6	7430747.8	1289.7	67.5	RC	58	257
DTH-I-4-09	385101.0	7430754.0	1290.1	67	RC	58	257
DTH-I-5-10	385089.7	7430751.4	1290.1	67	RC	85	257
DTH-I-6-10	385096.5	7430749.0	1289.9	67	RC	55	205
DTH-L01-10	385423.7	7429293.1	1210.6	67	RC	8	219
DTH-L02-10	385442.4	7429319.4	1211.1	49	RC	10	324
DTH-L03-10	385458.5	7429330.3	1211.0	50	RC	9	52
DTHAL-01-01	384450.2	7430376.1	1448.8	150	RC	61	247
DTHLL-01	385199.1	7427998.4	1240.6	121.5	RC	90	360
DTHLL-02	385550.1	7427900.0	1212.9	81	RC	90	360
DTHLL-03	384924.6	7427299.6	1244.2	120	RC	90	360
DTHLL-04	385398.8	7428230.4	1232.2	120	RC	90	360
DTHLL-05	385657.6	7428380.8	1217.9	76	RC	90	360
DTHLL-06	385715.2	7428729.7	1232.0	37	RC	90	360
DTHLL-07	385457.1	7428587.2	1239.4	121.5	RC	90	360

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
DTHLL-08	385486.6	7428590.7	1231.3	120	RC	60	270
DTHLL-09	385318.8	7428482.5	1248.3	120	RC	90	360
DTHLL-10	384979.8	7428337.9	1266.9	63	RC	90	360
DTHLL-11	385189.7	7427610.7	1222.7	67.5	RC	90	360
DTHLL-12	385201.2	7426601.6	1201.9	73.5	RC	90	360
DTHMG-00-02	385183.2	7429373.7	1281.7	152	RC	90	360
DTHMG-02-01	385188.5	7429209.5	1276.7	200	RC	90	360
DTHMG-02-02	385072.1	7429553.0	1297.8	150	RC	84	324
DTHMG-02-03	385385.4	7429553.7	1271.9	150	RC	87	300
DTHTS-02-01	384664.3	7429359.9	1330.5	158	RC	62	264
DTHTS-03-01	384664.4	7429154.2	1326.2	200	RC	76	281
ERM-1	385126.8	7430777.1	1343.5	160	RC	40	298
ERM-1A	385127.7	7430776.8	1343.4	179.5	RC	40	298
ERM-2	385255.8	7430720.1	1325.6	192	RC	40	298
ERM-3	385355.7	7430668.8	1325.1	181	RC	40	298
ERM-4	385470.8	7430620.5	1331.0	181	RC	40	298
F01A-08	386192.2	7431289.0	1298.4	20	RC	0	0
F02A-08	386123.0	7431310.0	1298.6	20	RC	0	0
F03A-08	386108.7	7431325.5	1298.7	20.5	RC	0	0
F07-08	386016.0	7431421.9	1400.1	31.5	RC	73	235
F08-08	386023.2	7431414.8	1401.7	40	RC	70	235
F09-08	386131.6	7431282.0	1403.4	41.5	RC	62	235
F10-08	386131.6	7431282.0	1403.4	59.5	RC	81	235
F11-08	386113.5	7431305.2	1410.2	46.5	RC	68	235
F12-08	386114.0	7431305.6	1410.4	69	RC	81	235
F13-08	386109.1	7431327.3	1412.0	43.5	RC	61	235
F14-08	386109.5	7431327.7	1412.0	68.5	RC	74	235
F15-08	386106.0	7431369.9	1415.5	70	RC	45	233
F16-08	386124.3	7431352.8	1411.6	77.5	RC	45	233
G1-A	385612.4	7430120.2	1178.0	59.5	RC	0	250
G1-B	385581.6	7430126.3	1177.3	25	RC	45	258
G1-C	385581.6	7430126.3	1177.3	31	RC	70	258
G340-1-10	386329.7	7430275.5	1209.2	50.5	RC	7	180
G340-3-10	386404.7	7430233.1	1205.9	70	RC	42	269
G340-4-10	386403.0	7430233.1	1206.5	70	RC	7	271
G340-5-10	386369.5	7430228.9	1181.4	22	RC	39	237
G340-6-10	386370.8	7430229.8	1181.2	40	RC	82	220
G340-7-10	386353.5	7430250.2	1180.9	25	RC	52	235
G340-8-10	386355.9	7430251.8	1180.6	40	RC	90	218
G340-9-10	386371.8	7430181.6	1189.3	59.5	RC	5	94
HS-1	385450.0	7429450.0	1170.0	121	RC	40	120

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
HS-2	385276.0	7429088.0	1170.0	63	UG	45	120
HS-3	385276.5	7429185.5	1170.0	70.5	UG	0	90
HS-4	385303.0	7429063.5	1170.0	126	UG	0	90
HS-5	385282.0	7429088.0	1170.0	129	UG	0	270
HS-A	385323.0	7429411.0	1178.0	60	UG	0	270
HS-B	385357.0	7429375.0	1179.0	39	UG	0	270
HS-C	385361.0	7429345.0	1179.0	51	UG	0	259
JP-1	385497.5	7430005.0	1251.0	80	RC	12	258
JP-2	385500.5	7430023.5	1250.0	102	RC	45	296
JP-3	385500.5	7430023.5	1251.0	80	RC	12	296
JP-4	385522.0	7430204.0	1251.0	73	RC	12	299
JP-5	385557.0	7430335.0	1250.0	102	RC	55	272
JP-6	385557.0	7430335.0	1251.0	80	RC	12	272
JP-7	385259.0	7429185.0	1170.0	123	RC	0	270
JP-8	385259.0	7429250.0	1171.0	111	RC	0	270
L01-08	385335.0	7429329.8	1266.0	85.5	RC	52	259
L02-08	385321.6	7429311.1	1266.5	82.5	RC	61	263
L03-08	385354.0	7429309.9	1264.1	89.5	RC	62	262
L04-08	385344.0	7429290.0	1264.2	80.5	RC	52	267
L05-09	385459.8	7429299.9	1256.6	68.5	RC	90	0
L06-09	385460.0	7429325.0	1257.4	64	RC	90	0
L07-09	385484.7	7429324.6	1255.9	77.5	RC	90	0
L08-09	385484.9	7429300.2	1254.9	80.5	RC	90	0
L09-09	385485.1	7429275.0	1254.2	80.5	RC	90	0
L10-09	385460.2	7429275.0	1256.0	80.5	RC	90	0
L11-09	385433.1	7429287.6	1258.0	80.5	RC	90	0
L12-09	385472.9	7429262.2	1254.9	34	RC	90	0
L13-09	385465.5	7429263.3	1255.5	80.5	RC	90	0
L14-09	385475.0	7429313.0	1175.0	55.5	RC	-10	103
L15-09	385475.0	7429313.0	1175.0	50.5	RC	44	103
L16-09	385473.0	7429314.0	1175.0	50.5	RC	77	103
L17-09	385470.0	7429316.0	1175.0	40	RC	62	285
M-01	386275.2	7429794.8	1233.1	136	RC	65	282
M-02	386216.7	7429711.2	1220.1	100	RC	65	272
M-03	386347.4	7430095.1	1246.7	205	RC	57	273
M-04	386166.4	7430699.9	1384.0	136	RC	60	278
M-05	386130.7	7430900.8	1403.8	80	RC	70	272
M-06	386123.9	7430335.5	1346.6	150	RC	60	275
M-07	386132.2	7430402.4	1351.3	156	RC	60	274
M-08	386251.5	7429898.7	1247.1	120	RC	65	273
M-09	386281.6	7429972.5	1252.6	90	RC	60	277

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
M-10	386275.5	7429793.7	1223.2	274	RC	90	36
M-11	386220.2	7429711.7	1220.0	130	RC	70	272
M-12	386170.0	7430701.2	1384.0	236	RC	90	360
M-14	385961.1	7431486.2	1389.1	70	RC	60	240
M-15	386070.4	7431189.8	1390.6	90	RC	60	247
M-16	386650.0	7430200.0	1201.2	250	RC	60	270
M-17	386650.0	7430500.0	1231.3	260	RC	65	270
M-18	386570.0	7430400.0	1229.9	260	RC	60	270
N-01	384911.4	7432204.5	1382.5	89.5	RC	50	270
N-02	384912.2	7432204.6	1382.5	115	RC	70	270
N-06	384873.7	7432349.4	1382.6	93	RC	50	270
N-08	384862.5	7432398.6	1384.4	43	RC	50	270
N-08A	384861.0	7432417.8	1384.5	100.5	RC	50	270
N-11	384820.7	7432916.2	1390.4	115	RC	37	270
N-12	384838.1	7432950.0	1387.1	43	RC	40	270
N-12A	384837.8	7432950.0	1387.0	109	RC	40	270
N-13	384839.1	7432949.9	1387.1	124	RC	57	270
N-14	384837.2	7432900.0	1387.8	100	RC	40	270
N-15	384838.1	7432900.0	1387.7	123	RC	57	270
N-16	384840.5	7432850.1	1387.7	100	RC	40	270
N-17	384841.4	7432850.1	1387.4	126	RC	57	270
N-18	384843.8	7432800.1	1386.4	89.5	RC	40	270
N-32	384907.3	7432501.8	1378.3	121	RC	69	270
N-34	384831.3	7432499.3	1386.6	184	RC	13	270
N-35	384831.9	7432499.4	1386.2	151	RC	50	270
N01-08	384787.1	7432700.4	1254.6	22	RC	0	300
N02-08	384892.3	7432085.8	1248.6	59.5	RC	0	225
N03-08	384882.6	7432176.8	1248.6	50.5	RC	0	225
N04-08	384786.8	7434025.0	1400.1	53.5	RC	60	270
N05-08	384818.6	7434025.0	1401.7	55	RC	71	270
N06-08	384830.0	7432500.0	1389.2	17.5	RC	90	0
N07-08	384840.0	7432500.0	1386.9	25	RC	42	270
N08-08	384841.0	7432475.0	1386.9	19	RC	80	270
N09-08	384848.0	7432400.0	1385.9	8.5	RC	90	0
N11-08	384763.5	7434025.0	1399.3	61	RC	50	90
N12-08	384784.8	7434025.0	1400.2	62	RC	50	90
NIDTH-01	384826.0	7432615.0	1250.0	45	UG	35	260
NIDTH-02	384822.0	7432598.0	1250.0	40	UG	35	260
NIDTH-03	384837.0	7432570.0	1250.0	43.5	UG	35	260
NIDTH-04	384842.0	7432545.0	1250.0	45	UG	35	260
NIDTH-05	384842.0	7432524.0	1249.0	42	UG	35	260

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
NIDTH-06	384841.0	7432496.0	1250.0	45	UG	35	260
NIDTH-07	384826.0	7432615.0	1250.0	40.5	UG	50	260
NIDTH-08	384829.0	7432596.0	1250.0	45	UG	35	260
NIDTH-09	384837.0	7432570.0	1250.0	40.5	UG	50	260
NIDTH-10	384842.0	7432545.0	1250.0	40.5	UG	50	260
NIDTH-11	384842.0	7432524.0	1249.0	37.5	UG	50	260
NIDTH-14	384806.0	7432655.0	1250.0	45	UG	0	260
NIDTH-15	384801.0	7432675.0	1253.0	45	UG	0	270
NIDTH-16	384823.0	7432679.0	1253.0	45	UG	0	90
NIDTH-17	384787.0	7432697.0	1254.0	45	UG	0	260
NIDTH-18	384853.0	7432421.0	1249.0	36	UG	35	260
NIDTH-19	384853.0	7432421.0	1249.0	30	UG	50	260
NIDTH-20	384849.0	7432447.0	1250.0	42	UG	35	260
NIDTH-21	384849.0	7432447.0	1249.0	31.5	UG	50	260
NIDTH-22	384787.0	7432697.0	1253.0	45	UG	45	260
NIDTH-23	384823.0	7432679.0	1253.0	45	UG	40	90
NIDTH-24	384799.0	7432675.0	1250.0	45	UG	45	270
NIDTH-25	384806.0	7432655.0	1250.0	45	UG	45	260
NIDTH-26	384858.0	7432398.0	1250.0	45	UG	35	260
NIDTH-27	384858.0	7432398.0	1250.0	24	UG	50	260
NIDTH-28	384867.0	7432343.0	1250.0	21	UG	35	260
NIDTH-29	384867.0	7432343.0	1250.0	6	UG	50	260
NIDTH-30	384872.0	7432310.0	1248.0	45	UG	35	260
NIDTH-31	384878.0	7432288.0	1248.0	45	UG	35	260
NIDTH-32	384823.0	7432679.0	1253.0	70.5	UG	20	90
NIDTH-33	384806.0	7432655.0	1250.0	66	UG	20	260
NIDTH-34	384833.0	7432620.0	1250.0	90	UG	0	80
NIDTH-35	384835.0	7432597.0	1250.0	90	UG	0	80
NIDTH-36	384845.0	7432570.0	1250.0	90	UG	0	80
NINDTH-01	384669.0	7433420.0	1340.0	30	UG	60	250
NINDTH-02	384678.0	7433420.0	1340.0	30.6	UG	85	250
NINDTH-03	384669.0	7433341.0	1340.0	30.6	UG	60	80
NINDTH-04	384669.0	7433341.0	1340.0	30.6	UG	80	80
NINDTH-05	384697.0	7433266.0	1340.0	30	UG	60	80
NINDTH-06	384697.0	7433266.0	1340.0	30.6	UG	80	80
NINDTH-07	384731.0	7433192.0	1340.0	30.6	UG	60	250
NINDTH-08	384731.0	7433192.0	1340.0	30.6	UG	85	250
NINDTH-09	384760.0	7433059.0	1340.0	30.6	UG	60	80
NINDTH-10	384760.0	7433059.0	1340.0	30.6	UG	80	80
NINDTH-11	384781.0	7432988.0	1340.0	30	UG	60	80
NINDTH-12	384781.0	7432988.0	1340.0	30.6	UG	80	80

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
NINDTH-13	384794.0	7432906.0	1340.0	39.6	UG	75	260
NINDTH-14	384794.0	7432906.0	1340.0	36	UG	50	260
NINDTH-15	384802.0	7432836.0	1340.0	30.6	UG	60	80
NINDTH-16	384802.0	7432836.0	1340.0	30.6	UG	80	80
NINDTH-17	384829.0	7432782.0	1340.0	39.6	UG	60	80
NINDTH-18	384829.0	7432782.0	1340.0	39.6	UG	85	80
NINDTH-19	384671.0	7433421.0	1370.0	26	UG	25	260
NINDTH-20	384671.0	7433421.0	1370.0	30	UG	40	260
NINDTH-21	384681.0	7433314.0	1370.0	30.6	UG	25	80
NINDTH-22	384681.0	7433314.0	1370.0	30.6	UG	40	80
NINDTH-23	384722.0	7433189.0	1370.0	30	UG	25	80
NINDTH-24	384722.0	7433189.0	1370.0	30	UG	40	80
NINDTH-25	384746.0	7433100.0	1370.0	30.6	UG	25	80
NINDTH-26	384746.0	7433100.0	1370.0	36	UG	40	80
NINDTH-27	384761.0	7433029.0	1370.0	30	UG	25	80
NINDTH-28	384761.0	7433029.0	1370.0	30	UG	40	80
NO-1	384780.1	7432135.6	1414.3	140.5	RC	45	229
NO-2	384775.9	7432120.0	1415.9	129	RC	45	205
NO-3	384856.8	7432132.0	1394.7	111	RC	45	205
NO-4	384852.2	7432198.4	1389.0	130	RC	20	263
NO-5	384714.9	7432257.2	1432.6	120	RC	40	222
NO-6	384639.3	7432331.3	1413.7	129	RC	32	222
NS-01	384896.3	7432146.1	1388.4	90	RC	53	255
NS-02	384936.3	7432157.0	1382.5	106	RC	44	255
NS-02A	384914.8	7432150.8	1385.5	138	RC	69	255
NS-03	384931.8	7432101.1	1383.7	91	RC	40	255
NS-04	384958.7	7432108.2	1379.6	113.5	RC	60	255
NS-04A	384933.6	7432101.6	1383.6	126	RC	60	253
NS-05	384933.4	7432050.0	1383.3	129	RC	36	270
NS-06	384934.4	7432049.9	1383.2	148	RC	54	270
NS-07	384937.3	7432000.1	1386.5	79	RC	40	270
NS-08	384938.9	7431999.6	1386.6	100	RC	65	270
NS-09	384925.4	7431999.8	1389.7	178	RC	17	270
NS-10	384934.8	7431999.9	1387.1	178	RC	57	270
NS-11	384940.0	7431950.1	1390.4	77.5	RC	12	270
NS-12	384944.0	7431950.1	1389.4	154	RC	45	270
NS-12A	384982.7	7431842.0	1381.8	151	RC	62	270
NS-13	384957.1	7431900.2	1385.9	151	RC	12	270
NS-14	384958.3	7431900.2	1385.8	160	RC	40	270
NS-14A	384959.3	7431900.2	1385.6	166	RC	62	270
NS-14B	384981.3	7431842.1	1381.8	110.5	RC	39	270

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
NS-16A	384964.3	7431847.8	1386.6	107	RC	17	265
NS-17	384973.3	7431799.6	1384.8	100	RC	11	260
NS-17A	384975.1	7431800.4	1384.3	151	RC	45	260
NS-18	385002.6	7431743.2	1379.8	155.5	RC	18	265
NS-18A	385004.8	7431743.0	1379.7	170.5	RC	40	260
NS-19	385016.1	7431698.1	1377.3	121	RC	15	260
NS-19A	385017.5	7431698.3	1377.0	181	RC	40	260
NS-20	385030.2	7431648.9	1374.6	121	RC	17	260
NS-20A	385031.1	7431649.1	1374.5	170.5	RC	40	260
NS-21	385039.7	7431599.6	1373.3	110.5	RC	24	260
NS-21A	385041.6	7431600.1	1373.2	185.5	RC	43	260
P-00	386278.3	7429849.8	1228.2	111	RC	50	270
P-00A	386278.9	7429849.9	1228.0	88	RC	71	270
P-00B	386280.2	7429852.5	1227.9	135	RC	69	270
P-01	386230.4	7429850.2	1237.8	108	UG	30	275
P-02	386232.2	7429850.2	1237.6	24	UG	82	310
P-03	386268.7	7429949.6	1251.7	79.5	UG	25	273
P-03A	386268.4	7429949.9	1253.0	121.5	UG	-4	270
P-04	386269.3	7429949.7	1251.5	97.5	UG	69	278
P-05	386277.8	7430059.0	1266.5	150	UG	7	274
P-06	386277.3	7430049.8	1265.2	72	UG	58	270
P-07	386278.0	7430049.9	1265.2	100.5	UG	90	360
P-08	386316.3	7430171.8	1280.9	91.5	UG	56	272
P-09	386274.8	7430194.6	1289.7	100.5	UG	14	336
P-10	386275.3	7430192.4	1288.7	81	UG	69	324
P-11	386255.1	7430349.1	1354.9	87	UG	55	270
P-12	386257.2	7430349.6	1354.8	120	UG	69	270
P-24	386267.5	7430599.7	1375.0	130.5	UG	60	284
PD-01	385272.0	7429070.0	1169.6	120	UG	0	246
PD-02	385282.0	7429088.0	1169.6	129	UG	0	270
PD-18	385495.0	7429555.0	1221.0	112.5	UG	0	270
PD-19	385495.0	7429555.0	1221.0	120	UG	40	270
PD-20	385495.0	7429555.0	1221.0	99	UG	64	270
PD-45	385545.0	7429992.0	1207.0	52.5	UG	27	270
PD-46	385545.0	7429992.0	1207.0	64.5	UG	80	270
PN-2	385522.5	7429850.0	1210.0	50	RC	72	270
PN-3	385545.0	7429900.0	1210.0	54.5	RC	81	270
PS-1	385505.0	7429537.0	1208.0	46.5	RC	20	126
PS-2	385505.0	7429537.0	1208.0	79.5	RC	5	140
Q-01-10	386272.4	7430780.3	1332.9	67	RC	10	84
Q-1	386282.3	7430288.7	1367.5	100	RC	80	228

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
Q-2	386282.3	7430288.7	1372.3	81	RC	50	228
Q-4	386313.5	7430717.3	1347.0	68.5	RC	50	228
Q-5	386360.3	7430850.2	1399.4	45	RC	50	263
-R1	385600.0	7430627.0	1356.5	31	RC	50	83
-R2	385600.6	7430626.8	1356.6	32.5	RC	70	83
-R3	385599.7	7430661.8	1353.5	32.5	RC	55	83
-R4	385600.2	7430661.9	1356.6	38.5	RC	75	83
-R5	385599.4	7430627.2	1351.6	99	RC	40	278
-R6	385601.7	7430663.4	1348.6	104.5	RC	57	270
RB-01	385529.9	7430200.2	1347.7	92	RC	58	299
RB-02	385538.7	7429132.9	1328.0	70	RC	43	260
RC-01	385500.3	7428482.4	1223.2	300	UG	45	270
RC-02	385443.0	7428797.0	1245.3	300	UG	60	270
RC-03	385469.9	7429098.5	1252.3	308	UG	62	270
RC-04	385603.7	7429449.3	1262.7	380	UG	65	270
RC-05	385864.7	7430305.6	1384.1	380	UG	65	270
RC-06	385897.0	7431289.4	1416.6	300	UG	65	270
RC-07	385750.8	7431705.3	1372.5	300	UG	72	270
RC-08	386192.0	7430707.4	1390.1	276	UG	72	270
RC-09	386023.4	7431443.7	1394.3	280	UG	75	270
RC-10	386553.9	7429994.6	1208.1	114	UG	60	270
RC-11	385229.4	7430203.0	1302.1	150	UG	90	360
RC-12	384903.9	7432892.9	1379.1	60	UG	60	270
RC-12A	384903.9	7432892.9	1379.1	300	UG	60	270
RC-13	384989.0	7432304.8	1371.0	278	UG	60	270
RC-14	385223.8	7429976.9	1291.8	150	UG	90	360
RC-15	385240.2	7429747.0	1281.9	138	UG	84	270
RC6-1	385649.9	7429100.0	1240.2	360	UG	60	269
RC6-10	386643.7	7431221.4	1246.6	300	UG	60	255
RC6-11	386303.4	7431763.2	1282.9	260	UG	60	255
RC6-12	385975.4	7431779.7	1372.5	350	UG	60	250
RC6-13	385821.9	7432402.8	1370.0	150	UG	66	270
RC6-14	385838.5	7433149.8	1389.1	200	UG	60	270
RC6-15	384832.7	7433298.8	1396.9	360	UG	60	270
RC6-16	384754.4	7433298.7	1405.4	144	UG	50	270
RC6-17	384380.1	7430136.5	1455.7	140	UG	60	300
RC6-18	384706.6	7429687.6	1334.1	216	UG	60	220
RC6-19	384896.0	7433288.0	1396.6	230	UG	65	270
RC6-2	385730.2	7429484.7	1264.4	354	UG	64	263
RC6-20	384934.2	7432769.3	1375.4	264	UG	50	270
RC6-21	385130.9	7430650.0	1340.6	192	UG	60	270

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
RC6-22	385154.2	7430900.0	1341.5	180	UG	60	270
RC6-23	385107.9	7430500.1	1334.5	180	UG	60	270
RC6-24	385233.1	7430574.8	1326.3	320	UG	60	270
RC6-25	384859.1	7429700.1	1320.7	170	UG	60	270
RC6-26	384938.6	7429900.0	1319.4	190	UG	60	270
RC6-27	385769.6	7430843.5	1371.6	256	UG	90	0
RC6-28	384874.0	7433079.7	1388.9	260	UG	58	270
RC6-29	386235.4	7431656.6	1306.1	250	UG	60	239
RC6-3	384901.8	7430688.0	1375.8	264	UG	60	268
RC6-30	385843.0	7431986.4	1309.7	240	UG	45	250
RC6-31	385635.4	7432126.4	1325.1	120	UG	50	250
RC6-4	385755.2	7430707.2	1360.0	220	UG	76	289
RC6-5	385130.3	7430774.2	1342.1	250	UG	52	290
RC6-6A	385230.8	7430711.0	1327.1	274	UG	60	296
RC6-6B	385105.8	7430763.4	1101.6	96	UG	59	293
RC6-7	385768.7	7430843.5	1371.6	230	UG	70	271
RC6-8	386235.3	7431092.4	1419.2	292	UG	55	270
RC6-9	385850.1	7431050.0	1398.4	200	UG	70	270
RC6-C-2	385446.6	7423497.4	1174.5	100	UG	45	250
RC6-C-3	385530.4	7423395.0	1172.6	100	UG	45	250
RC6-C-5	385412.5	7423617.4	1177.1	90	UG	45	250
RC6-C-6	385920.8	7423418.9	1176.4	96	UG	55	290
RC6-C-7	385970.1	7423534.0	1184.0	102	UG	55	290
RC6-C-8	385875.2	7423302.0	1172.7	90	UG	55	290
RC6-LL-1	385476.2	7428008.6	1221.8	134	UG	90	0
RC6-LL-2	386260.3	7428459.8	1191.1	168	UG	90	0
RC6-LL-3	386537.2	7427470.1	1163.6	140	UG	90	0
RC6-LL-4	386087.7	7426176.8	1155.6	102	UG	90	0
RC6-LL-5	387683.0	7428882.8	1166.6	84	UG	90	0
RC6-LL-6	387504.5	7430244.6	1178.4	114	UG	90	0
RC6-SA-1	384607.6	7431079.9	1508.9	150	UG	45	260
RC6-SA-10	384739.8	7431606.1	1484.1	252	UG	60	270
RC6-SA-11	384729.7	7431724.0	1473.9	220	UG	50	270
RC6-SA-12	384698.3	7431889.4	1469.0	160	UG	65	270
RC6-SA-13	384695.3	7431889.3	1468.7	124	UG	50	270
RC6-SA-14	384700.4	7432008.6	1453.9	150	UG	45	270
RC6-SA-15	384702.5	7432008.7	1453.9	174	UG	70	270
RC6-SA-16	384626.2	7430979.2	1503.6	150	UG	50	259
RC6-SA-2	384476.7	7431140.5	1509.1	190	UG	47	79
RC6-SA-3	384607.3	7431219.3	1487.0	202	UG	45	260
RC6-SA-4	384734.0	7431246.0	1502.5	300	UG	50	258

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
RC6-SA-5	384497.9	7431352.6	1472.5	150	UG	45	258
RC6-SA-6	384681.1	7431345.8	1483.4	280	UG	45	259
RC6-SA-7	384676.6	7431498.7	1470.8	240	UG	50	269
RC6-SA-8	384516.9	7431665.4	1483.4	170	UG	45	290
RC6-SA-9	384678.6	7431498.5	1471.0	200	UG	66	270
RC6-TS-1	384186.2	7431120.2	1489.2	204	UG	60	266
RC6-TS-2	384276.0	7431085.9	1472.9	110	UG	70	259
RC6-TS-3	384276.8	7431086.1	1472.9	140	UG	90	0
RC6-TS-4	383982.2	7431396.1	1522.3	120	UG	55	248
RC6-TS-5	384185.5	7431341.9	1526.2	170	UG	50	270
RC6-V-1	389209.4	7431394.5	1226.4	200	UG	80	135
RC7-SM-01	386518.5	7430098.5	1212.9	258	UG	45	310
RC7-SM-02	386257.3	7429826.6	1230.5	170	UG	85	313
RC7-SM-03	386350.8	7429826.5	1212.6	166	UG	50	289
RC7-SM-04	386412.0	7429983.2	1219.1	168	UG	45	275
RC7-SM-05	386351.3	7430930.9	1395.6	260	UG	45	245
RC7-SM-06	384544.8	7432437.6	1418.0	160	UG	50	215
RC7-SM-07	384568.7	7432421.5	1420.4	160	UG	50	215
RC7-SM-08	384598.9	7432400.6	1424.5	160	UG	45	215
RC7-SM-09	384597.4	7432399.0	1424.7	150	UG	70	215
RC7-SM-10	386354.1	7430936.7	1395.5	400	UG	45	275
RCH093-001	385376.8	7429383.0	1264.4	270	UG	60	272
RCH093-002	385473.3	7428650.5	1234.9	300	UG	62	264
RCH093-003	385302.4	7430194.2	1306.2	300	UG	60	270
RCH093-004	385900.7	7429346.9	1231.8	300	UG	60	273
RCH093-005	385895.5	7430197.6	1360.6	400	UG	59	270
RCH093-006	385068.0	7430950.1	1360.5	300	UG	58	271
RCH093-007	385438.3	7432449.3	1341.1	300	UG	59	275
RCH093-008	385297.0	7432771.2	1358.8	300	UG	60	273
RCH093-009	385723.2	7431687.9	1370.8	300	UG	59	270
RCH093-010	384798.8	7433913.3	1425.0	300	UG	61	274
RM-1	386104.8	7430276.9	1165.8	108	RC	5	297
RM-2	385979.7	7430341.5	1156.2	70.5	RC	2	297
RM-3	385923.0	7430371.3	1155.3	21	RC	90	297
RM-4	385923.0	7430371.3	1159.0	109.5	RC	0	297
RM-5	385707.0	7430486.0	1140.9	165	RC	3	297
RP-00-01	385440.7	7429424.3	1262.4	200	RC	61	302
RP-00-02	385444.7	7429422.0	1261.7	248	RC	73	305
RP-00-04	385406.2	7429357.1	1263.3	200	RC	58	299
RP-00-05	385407.0	7429356.0	1263.3	210	RC	79	295
RP-00-06	385493.1	7429361.5	1257.3	252	RC	59	273

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
RP-00-07	386020.5	7429400.5	1226.2	200	RC	61	286
RP-01-01	385499.5	7429522.1	1265.6	180	RC	61	272
RP-01-01A	385368.6	7429297.6	1264.1	218	RC	64	301
RP-01-02	385504.7	7429522.0	1265.6	170	RC	73	273
RP-01-02A	385415.9	7429266.7	1259.2	140	RC	65	300
RP-01-03	385543.1	7429510.2	1264.2	180	RC	67	300
RP-01-04	385512.2	7429563.5	1272.6	110	RC	68	301
RP-02-01	385563.8	7429604.1	1286.5	250	RC	59	301
RP-02-02	386138.4	7429614.6	1220.7	200	RC	61	286
RP-02-03	386276.4	7429580.6	1205.5	200	RC	61	286
RP-03-01	385534.2	7429712.3	1295.2	260	RC	59	265
RP-03-01A	386145.5	7429127.2	1214.7	152	RC	61	286
RP-03-02	386270.8	7429710.5	1213.0	236	RC	60	285
RP-03-02A	385292.7	7429085.5	1263.9	150	RC	61	300
RP-04-01	385891.1	7429769.8	1319.2	220	RC	59	306
RP-04-02	385535.2	7429802.8	1315.8	170	RC	60	273
RP-04-03	385535.6	7429802.7	1315.6	196	RC	81	277
RP-05-01	386002.3	7429930.6	1342.0	220	RC	57	295
RP-05-03	385501.6	7429910.6	1316.9	180	RC	61	278
RP-05-07	385524.8	7429939.7	1324.7	202	RC	64	291
RP-06-01	386411.7	7429988.3	1218.8	172	RC	59	285
RP-06-02	386274.2	7429974.1	1256.0	180	RC	61	287
RP-06-07	385513.5	7429997.1	1310.3	190	RC	60	291
RP-06-08	385518.1	7429995.8	1310.6	190	RC	90	360
RP-07-01	386275.2	7430100.1	1274.1	140	RC	60	287
RP-07-02	386117.6	7430135.5	1352.5	200	RC	61	286
RP-07-05	385593.3	7430108.1	1342.5	200	RC	60	291
RP-07-06	385597.0	7430105.9	1342.5	204	RC	90	360
RP-08-01	385237.8	7430198.6	1302.1	100	RC	60	270
RP-08-06	385571.1	7430214.9	1361.7	250	RC	60	270
RP-08-07	385573.1	7430215.1	1361.8	200	RC	90	360
RP-08-08	385197.7	7430201.1	1305.7	236	RC	61	90
RP-08-10	386500.0	7430195.6	1220.7	198	RC	59	285
RP-09-01	386122.3	7430301.8	1348.5	226	RC	68	273
RP-09-02	386022.2	7430319.9	1389.0	192	RC	64	94
RP-09-03	386015.9	7430319.9	1389.6	250	RC	80	92
RP-09-04	385825.3	7430297.5	1387.0	226	RC	60	270
RP-09-05	385618.9	7430332.6	1356.7	250	RC	70	270
RP-09-06	385620.5	7430332.7	1356.8	210	RC	90	360
RP-09-07	385618.7	7430271.7	1360.0	192	RC	58	269
RP-1	386088.9	7429700.2	1189.2	107.5	RC	7	250

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
RP-10-01	386114.7	7430428.9	1354.2	156	RC	58	270
RP-10-02	386006.8	7430404.8	1398.4	200	RC	55	83
RP-10-04	385660.5	7430413.0	1350.2	216	RC	60	270
RP-10-05	385665.7	7430413.5	1350.2	254	RC	75	270
RP-11-01	386173.8	7430487.2	1347.8	220	RC	56	266
RP-11-03	385686.1	7430499.1	1342.8	94	RC	60	279
RP-11-04	385687.4	7430499.1	1342.6	222	RC	75	281
RP-12-01	386167.3	7430628.8	1380.3	200	RC	58	271
RP-12-02	386168.5	7430628.7	1380.2	200	RC	80	267
RP-12-03	385675.2	7430572.3	1367.6	220	RC	60	268
RP-12-04	385678.9	7430572.3	1367.8	250	RC	74	272
RP-12-05	386266.1	7430590.7	1376.0	230	RC	60	284
RP-12-06	386040.4	7430637.0	1382.8	246	RC	60	93
RP-13-01	385644.2	7430663.6	1359.9	140	RC	60	257
RP-14-01	385681.3	7430816.9	1358.8	270	RC	63	265
RP-14-02	385682.3	7430816.9	1358.8	272	RC	76	275
RP-14-03	386186.5	7430792.4	1395.6	180	RC	60	270
RP-15-01	385430.0	7430946.6	1353.0	162	RC	59	256
RP-16-01	385724.2	7430979.5	1371.4	302	RC	61	264
RP-16-02	385734.1	7430986.1	1372.0	222	RC	71	260
RP-16-03	385572.2	7430969.6	1390.0	200	RC	60	255
RP-18-01	385819.7	7431166.5	1371.8	150	RC	60	254
RP-19-01	386170.4	7431292.3	1401.3	280	RC	60	255
RP-19-03	385807.6	7431269.0	1392.7	208	RC	59	256
RP-20-01	385821.8	7431362.4	1396.6	220	RC	59	254
RP-20-02	385898.0	7431391.4	1409.4	230	RC	60	254
RP-20-03	386099.8	7431423.1	1410.8	282	RC	59	255
RP-21-01	385742.1	7431514.9	1380.0	148	RC	59	255
RP-23-01	385838.6	7431700.9	1378.6	180	RC	61	255
RP-24-01	385596.9	7431815.3	1369.3	150	RC	60	256
RP-26-01	385583.4	7431935.7	1370.7	200	RC	60	255
RP-27-01	385536.6	7432090.8	1353.1	200	RC	59	255
RP-29-01	384885.6	7432309.8	1381.8	200	RC	61	240
RP-30-01	385463.2	7432355.0	1336.1	150	RC	60	255
RP-35-01	384836.1	7432918.4	1388.0	150	RC	60	270
SA-01	384494.3	7431023.7	1521.7	28	RC	50	90
SA-02	384514.4	7431023.6	1517.5	30	RC	50	90
SA-03	384534.3	7431023.8	1514.0	28	RC	50	90
SA-04	384554.3	7431023.8	1511.5	28	RC	50	90
SA-05	384574.2	7431023.5	1510.6	28	RC	50	100
SA-06	384594.5	7431023.9	1509.3	28	RC	50	90

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
SA-07	384494.5	7431043.7	1520.2	28	RC	50	90
SA-08	384514.3	7431043.8	1515.9	25	RC	50	90
SA-09	384534.2	7431043.8	1512.3	28	RC	50	90
SA-10	384554.2	7431043.8	1509.4	28	RC	46	90
SA-11	384574.1	7431043.8	1509.5	28	RC	45	90
SA-12	384594.1	7431043.8	1509.9	27	RC	48	90
SA-13	384494.0	7431064.2	1517.9	27	RC	50	90
SA-14	384513.8	7431063.2	1513.6	28	RC	50	100
SA-15	384534.2	7431063.7	1510.3	28	RC	54	100
SA-16	384554.5	7431063.6	1506.9	28	RC	53	100
SA-17	384573.9	7431062.6	1508.2	28	RC	50	100
SA-18	384594.1	7431063.9	1508.4	27	RC	45	90
SA-19	384494.2	7431083.7	1514.7	28	RC	50	90
SA-23	384574.7	7431083.7	1506.5	28	RC	55	100
SA-24	384594.0	7431083.8	1506.8	26	RC	50	100
SADDH-01	386309.1	7429963.4	1242.5	110	DD	56	282
SADDH-02	386197.9	7430951.7	1208.8	20	DD	90	0
SADDH-03	386199.9	7430952.2	1209.2	34	DD	35	73
SADDH-04	386256.2	7430806.6	1191.1	40	DD	0	259
SADDH-06	386250.9	7430826.7	1157.0	108	DD	62	115
SADDH-07	386253.7	7429986.2	1250.4	80	DD	67	290
SADDH-08	386250.6	7430826.5	1156.9	94	DD	67	183
SADDH-09	386256.3	7430011.0	1262.7	72.9	DD	50	269
SADDH-10	386251.6	7430831.0	1157.1	102	DD	65	34
SADDH-11	386248.9	7430830.3	1156.9	82	DD	70	302
SADDH-12	386269.5	7430027.5	1263.5	95.6	DD	68	279
SADDH-13	386279.0	7430758.8	1158.6	100	DD	67	77
SADDH-14	386276.0	7430759.1	1158.7	54	DD	82	243
SADDH-15	386226.2	7430902.3	1191.8	50	DD	0	70
SADDH-16	386297.0	7429996.0	1252.4	94.25	DD	48	267
SADDH-17	386219.3	7430900.0	1191.6	24	DD	0	252
SADDH-18	386242.6	7430855.1	1191.5	50	DD	-1	72
SADDH-19	386236.5	7430853.2	1191.5	42	DD	0	254
SADDH-20	386262.9	7430808.2	1191.2	42	DD	1	78
SADDH-21	386270.2	7430762.4	1190.9	74	DD	15	71
SADDH-22	386263.9	7430760.2	1190.7	48	DD	15	254
SADDH-23	386285.3	7430038.0	1262.9	122	DD	48	272
SADDH-24	386245.0	7430894.0	1158.3	66	DD	46	70
SADDH-25	386237.2	7430891.0	1157.8	58	DD	56	258
SADDH-26	385785.4	7431525.9	1298.8	20	DD	1	252
SADDH-27	385791.3	7431527.9	1298.8	22	DD	1	71

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
SADDH-28	386371.1	7430495.8	1332.7	164	DD	45	270
SADDH-29	385798.0	7431483.6	1297.5	30	DD	59	249
SADDH-30	385800.4	7431484.5	1297.4	26	DD	73	65
SADDH-31	385747.9	7431507.2	1299.2	84	DD	25	66
SADDH-32	385761.7	7431452.5	1298.7	96	DD	28	65
SADDH-33	386090.8	7430285.1	1072.6	68	DD	65	270
SADDH-34	386069.2	7430297.9	1070.5	70	DD	66	89
SADDH-35	386035.5	7430152.2	1070.3	74	DD	62	85
SADDH-36	386017.0	7430096.9	1070.2	70	DD	63	87
SADDH-37	385726.5	7430451.0	1143.3	50	DD	66	280
SADDH-38	386369.7	7430495.8	1333.7	100	DD	14	272
SADDH-39	386021.1	7430101.6	1070.4	50	DD	65	265
SADDH-40	385713.0	7430400.0	1137.3	40	DD	70	277
SADDH-41	386003.9	7430016.8	1069.9	64	DD	71	97
SADDH-42	385715.8	7430400.1	1137.4	52	DD	70	85
SADDH-43	385986.1	7429930.7	1070.0	60	DD	71	74
SADDH-44	385673.5	7430261.1	1132.5	40	DD	66	279
SADDH-45	385990.6	7429919.9	1070.4	60	DD	70	265
SADDH-46	385693.2	7430325.8	1133.8	40	DD	69	269
SADDH-47	385683.4	7430292.0	1134.0	40	DD	66	267
SADDH-48	386001.4	7429972.4	1070.0	60	DD	67	259
SADDH-49	386017.1	7430054.0	1070.2	60	DD	58	261
SADDH-50	385707.5	7430372.2	1135.3	40	DD	66	278
SADDH-51	386047.1	7430197.6	1070.7	62	DD	65	269
SADDH-52	385747.8	7430479.3	1147.8	40	DD	69	276
SADDH-53	386057.7	7430235.7	1070.3	60	DD	71	265
SADDH-54	386078.5	7430355.2	1071.3	60	DD	74	243
SADDH-55	386355.3	7430426.0	1333.5	136.2	DD	61	270
SADDH-56	386083.7	7430355.2	1071.3	60	DD	69	93
SADDH-57	386093.0	7430555.2	1071.0	54	DD	72	274
SADDH-58	386100.8	7430598.2	1071.0	56	DD	71	85
SADDH-59	386090.7	7430536.1	1071.0	60	DD	65	86
SADDH-60	386091.4	7430490.3	1070.9	60	DD	74	86
SADDH-61	386090.3	7430469.4	1070.4	60	DD	71	262
SADDH-62	386089.2	7430424.9	1072.3	45	DD	10	93
SADDH-63	386085.0	7430424.9	1071.2	54	DD	73	290
SADDH-64	386361.6	7430452.4	1334.0	120	DD	49	270
SADDH-65	386222.2	7430400.0	1346.9	132	DD	66	90
SADDH-66	386352.9	7430400.0	1334.1	120	DD	51	270
SADDH-67	386361.5	7430452.4	1334.2	120	DD	29	270
SADDH-68	386367.5	7430474.8	1334.3	100	DD	19	270

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
SADDH-70	386271.0	7430789.6	1158.4	300	DD	59	90
SADDH-71	386233.7	7430879.6	1190.1	100	DD	28	90
SADDH-72	386103.3	7430740.0	1070.8	60	DD	69	264
SADDH-73	386106.7	7430740.9	1070.9	64	DD	59	55
SADDH-74	386102.0	7430727.5	1070.4	60	DD	68	103
SADDH-75	386107.0	7430708.4	1071.3	60	DD	63	86
SADDH-76	386103.9	7430702.0	1071.5	60	DD	58	274
SADDH-77	386100.9	7430666.9	1070.9	60	DD	64	93
SADDH-78	386098.8	7430647.5	1071.3	60	DD	62	271
SADDH-79	386104.2	7430628.8	1071.4	60	DD	71	108
SADDH-80	386100.1	7430578.6	1071.0	54	DD	65	86
SADDH-82	386141.3	7430332.6	1153.1	68	DD	48	93
SADDH-83	386147.2	7430385.1	1153.6	50	DD	37	79
SADDH-84	386182.8	7430436.0	1145.3	26	DD	27	82
SD-01	385802.3	7430687.2	1125.9	88	DD	0	60
SD-02	386101.5	7430583.6	1301.5	42	DD	45	290
SD-03	386099.3	7430564.8	1301.9	24	DD	44	300
SD-04	386099.3	7430564.8	1302.0	23.7	DD	-30	300
SD-05	386109.7	7430648.3	1216.5	20	DD	0	65
SD-06	386114.3	7430585.6	1213.6	28	DD	0	235
SD-09	386106.5	7430582.5	1341.9	10	DD	45	260
SD-09 A	386106.5	7430582.5	1342.0	6.85	DD	40	260
SD-11	386099.2	7430565.1	1301.0	11.9	DD	47	270
SD-12	386165.8	7430767.9	1206.7	48	DD	0	260
SD-13	386169.8	7430778.0	1206.3	40	DD	0	90
SD-14	386178.8	7430698.0	1209.1	36	DD	0	55
SD-15	386205.5	7430655.0	1211.3	13.45	DD	0	90
SD-16	386337.4	7430514.3	1204.4	50	DD	0	65
SD-17	386229.7	7430511.0	1210.8	8	DD	0	236
SD-19	384850.5	7432370.7	1385.8	30	DD	46	271
SD-20	384850.5	7432370.7	1385.8	19.2	DD	61	271
SD-21	386123.8	7430739.3	1388.9	20	DD	50	278
SD-22	386127.3	7430730.2	1386.3	8	DD	48	276
SD-23	386081.8	7431259.0	1397.8	46	DD	50	249
SD-24	386081.1	7431222.5	1394.4	48	DD	46	264
SD-26	386161.6	7430034.3	1237.0	33.45	DD	0	267
SD-26A	386161.6	7430034.3	1236.8	32	DD	0	267
SD-27	386167.8	7430034.8	1236.7	38	DD	0	84
SD-28	386335.0	7430315.1	1209.6	38	DD	0	230
SD-29	386119.7	7430880.3	1400.7	30.5	DD	41	271
SD-30	386119.5	7430902.1	1400.2	34	DD	43	270

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
SD-31	386112.7	7430932.6	1398.8	34	DD	32	262
SD-32	386110.5	7430957.1	1394.8	20	DD	45	267
SD-33	384511.1	7432382.9	1405.1	36	DD	33	229
SD-34	384530.3	7432358.2	1409.3	36	DD	42	217
SD-35	384535.3	7432334.6	1412.9	26	DD	40	224
SDD-01	385630.8	7430837.1	1350.9	182	DD	43	260
SDD-02	385635.6	7430845.3	1351.4	25.05	DD	44	318
SDD-04	385355.6	7429321.0	1178.3	98	DD	52	289
SDD-05	385355.4	7429320.2	1178.3	122	DD	52	260
SDD-06	385355.6	7429321.0	1178.3	134	DD	54	330
SDD-07	385355.4	7429320.2	1178.3	132	DD	90	0
SDD-10	385374.0	7429321.2	1197.3	198	DD	65	240
SDD-11	385374.0	7429321.2	1197.3	152	DD	90	0
SDD-12	386290.0	7429748.5	1215.8	206	DD	51	285
SDD-13	386267.3	7429721.7	1215.0	934	DD	53	290
SDD-14	385381.3	7429428.9	1163.9	116	DD	41	268
SDD-15	386263.5	7429676.2	1213.2	122	DD	58	282
SDD-16	385381.3	7429428.9	1163.9	102	DD	70	268
SDD-17	386030.8	7431440.2	1395.3	60	DD	48	223
SDD-18	386048.1	7431398.7	1403.6	88	DD	49	235
SDD-20	386293.9	7430328.1	1208.0	26	DD	37	300
SDD-21	386293.3	7430336.2	1208.4	5	DD	11	346
SDD-22	386318.4	7430330.3	1179.6	26	DD	44	281
SDD-23	385100.0	7430574.0	1341.6	216	DD	60	270
SDD-24	385135.6	7430649.7	1340.5	218	DD	90	0
SDD-25	385219.2	7430701.1	1329.2	234	DD	59	270
SI-01	386032.5	7430291.8	1255.0	121.5	RC	0	298
SI-02	386082.5	7430269.9	1259.2	109.5	RC	40	330
SI-03	386082.1	7430266.5	1258.9	33	RC	60	298
SI-03A	386082.7	7430266.3	1259.1	111	RC	60	298
SI-04	386104.4	7430259.1	1263.0	117	RC	0	343
SI-04A	386104.4	7430259.1	1262.9	30	RC	0	343
SI-05	386101.2	7430253.0	1262.9	120	RC	0	245
SI-06	386134.3	7430242.9	1265.5	99	RC	80	360
SI-07	386137.5	7430242.8	1266.9	91.5	RC	0	60
SI-08	386173.0	7430220.3	1269.9	100.5	RC	75	263
SI-09	386202.6	7430201.7	1274.5	70.5	RC	0	240
SI-10	386177.5	7430235.4	1268.0	91	RC	0	60
SI-11	386064.4	7430380.1	1255.6	180	RC	0	86
SI-12	386058.3	7430379.8	1255.5	180	RC	0	267
SI-13	386065.0	7430429.8	1254.9	180	RC	0	89

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
SI-14	386091.2	7430301.8	1256.8	160.5	RC	0	83
SI-15	386164.1	7430218.0	1271.0	144	RC	3	252
SI-16	386067.0	7430262.4	1257.2	160.5	RC	-7	142
SL-01	385620.6	7430599.9	1355.9	61	RC	57	262
SL-02	385621.5	7430587.4	1357.7	58	RC	53	263
SL-03	385622.5	7430574.9	1358.9	54	RC	54	265
SL-04	385623.6	7430562.3	1359.9	70	RC	55	262
SL-05	385623.6	7430550.0	1360.3	55	RC	58	265
SL-06	385619.6	7430612.5	1355.1	63	RC	56	264
SL-07	385618.6	7430625.1	1354.6	39	RC	62	289
SL-08	385599.8	7430625.2	1351.4	40	RC	60	270
SL-09	385600.0	7430612.5	1352.0	19	RC	60	270
SL-10	385599.6	7430600.1	1349.1	38	RC	58	270
SL-11	385599.7	7430587.3	1350.3	48	RC	56	263
SL-12	385600.0	7430574.3	1350.8	46	RC	57	268
SL-13	385600.1	7430562.6	1351.9	44	RC	56	267
SL-14	385599.8	7430550.2	1353.0	41	RC	56	275
SLDTH-13	385473.0	7429315.0	1175.1	30	UG	90	0
SLDTH-14	385451.0	7429285.0	1175.2	30	UG	90	0
SLDTH-15	385475.0	7429286.0	1175.7	30	UG	90	0
SLDTH-16	385500.0	7429272.0	1176.4	30	UG	50	270
SLDTH-17	385460.0	7429300.0	1145.4	30	UG	0	90
SLDTH-18	385490.0	7429285.0	1143.8	30	UG	25	90
SLDTH-19	385480.0	7429300.0	1213.4	33	UG	25	295
SLDTH-20	385480.0	7429300.0	1213.4	33	UG	25	255
SLDTH-21	385485.0	7429300.0	1213.8	30	UG	25	215
SM-01	385890.3	7430392.9	1110.1	65.5	RC	3	270
SM-01-09	386050.2	7430098.8	1219.1	54	RC	90	0
SM-02	385903.6	7430310.2	1109.9	91	RC	2	267
SM-02-09	386077.8	7430098.6	1222.8	64	RC	67	271
SM-111-09	384848.3	7434075.7	1414.8	74.2	RC	53	262
SM-112-09	384844.2	7433943.5	1420.2	116.35	RC	54	267
SMR-001	385899.1	7431099.7	1389.5	102	UG	45	249
SMR-003	386129.3	7431174.7	1395.2	33	UG	46	252
SMR-009	386061.4	7431256.0	1402.4	68	UG	59	256
SMR-010	386085.1	7431270.1	1397.7	120	UG	60	249
SMR-011	386080.7	7431315.2	1409.4	120	UG	59	251
SMR-012	385819.3	7431227.8	1389.6	120	UG	63	244
SMR-015	385760.0	7431261.9	1378.0	90	UG	58	250
SMR-016	385826.6	7431276.4	1393.8	120	UG	65	250
SMR-017	386064.0	7431364.5	1413.9	120	UG	60	249

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
SMR-020	385780.1	7431321.9	1379.4	121	UG	60	251
SMR-023	386015.2	7431399.8	1401.1	113	UG	59	259
SMR-025	385769.2	7431369.5	1384.6	120	UG	61	249
SMR-026	386020.3	7431454.0	1393.6	120	UG	61	253
SMR-028	385801.3	7431431.5	1392.2	120	UG	47	248
SMR-030	386008.2	7431502.1	1391.6	85	UG	60	246
SMR-031	385801.6	7431484.9	1386.7	121	UG	58	249
SMR-033	385999.5	7431549.4	1393.3	120	UG	44	250
SMR-034	385720.6	7431511.3	1381.7	60	UG	49	253
SMR-035	385789.7	7431534.1	1376.7	120	UG	60	248
SMR-036	385963.9	7431591.9	1388.1	120	UG	50	245
SMR-038	385764.2	7431579.5	1372.4	116	UG	61	248
SMR-038B	385728.4	7431566.1	1373.3	102	UG	56	247
SMR-038D	385749.1	7431626.3	1384.7	120	UG	57	247
SMR-039	385950.3	7431639.9	1388.1	105	UG	50	252
SMR-041	385681.9	7431655.7	1371.7	120	UG	57	250
SMR-043	385671.5	7431757.6	1387.9	120	UG	59	250
SMR-046	385651.9	7431857.1	1373.1	120	UG	68	247
SMR-061	385466.8	7429542.2	1257.3	120	UG	64	302
SMR-062	385523.9	7429468.3	1257.3	100	UG	53	300
SMR-097	385447.7	7429950.0	1301.0	79	UG	59	274
SMR-101	385459.0	7430200.3	1340.1	100	UG	57	271
SMR-102	385526.6	7430100.1	1331.0	60	UG	88	202
SMR-103	385577.6	7430299.9	1342.7	100	UG	65	267
SMR-104	385483.9	7429700.0	1281.6	85	UG	53	273
SMR-105	385651.8	7430600.1	1363.8	120	UG	59	271
SMR-106	385607.6	7430400.0	1339.9	25	UG	56	268
SMR-107	385673.9	7430749.9	1349.5	120	UG	58	271
SMR-108	385675.3	7430850.1	1356.0	120	UG	41	268
SMR-109	385638.8	7430800.0	1349.4	120	UG	59	270
SMR-110	385647.6	7430700.1	1353.9	120	UG	58	272
SMR-111	385877.8	7430450.1	1374.0	119	UG	47	271
SMR-112	385893.5	7430550.1	1379.0	120	UG	50	271
SMR-113	385881.3	7430650.0	1364.0	100	UG	50	266
SMR-114	385889.2	7430800.0	1403.5	100	UG	54	274
SMR-115	385628.8	7431000.0	1375.1	120	UG	47	268
SMR-116	385694.5	7430900.1	1365.1	120	UG	49	275
SMR-117	385671.3	7430949.9	1359.7	120	UG	49	268
SMR-118	385882.9	7430950.0	1404.5	120	UG	49	273
SMR-129	385310.2	7429101.9	1263.4	120	UG	90	360
SMR-129A	385309.2	7429102.4	1263.5	76	UG	65	294

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
SMR-130	385289.1	7429056.9	1262.6	120	UG	90	360
SMR-131	385309.9	7429419.9	1270.8	65	UG	90	360
SMR-132	385309.9	7429444.0	1271.1	120	UG	90	360
SMR-133	385309.9	7429395.1	1269.4	61	UG	90	360
SMR-134	385289.8	7429113.9	1264.5	120	UG	90	360
SMR-135	385266.7	7429128.2	1268.4	120	UG	90	360
SMR-136	385294.8	7429025.8	1260.8	100	UG	90	360
SMR-137	385269.0	7429183.9	1269.3	118	UG	90	360
SMR-138	385316.3	7429986.6	1260.8	120	UG	90	360
SMR-139	385283.0	7429002.5	1261.1	120	UG	90	360
SMR-140	385546.6	7429628.9	1284.2	120	UG	51	297
SMR-141	385484.8	7429607.7	1280.6	100	UG	90	360
SMR-142	385517.3	7429645.4	1282.3	80	UG	42	296
SMR-142A	385517.7	7429645.2	1282.2	100	UG	62	299
SMR-143	385223.1	7429152.6	1271.7	120	UG	90	360
SMR-144	385246.1	7429138.8	1269.9	120	UG	90	360
SMR-145	385507.0	7429451.9	1255.5	120	UG	69	294
SMR-147	385475.6	7429411.3	1258.1	90	UG	61	298
SMR-152	385669.0	7430450.1	1341.9	120	UG	60	262
SMR-153	385685.5	7430497.0	1341.3	100	UG	44	264
SMRC-060	385497.8	7429541.6	1268.7	170	UG	65	269
SMRC-065	385502.4	7429422.2	1255.7	68	UG	61	309
SMRC-065A	385512.9	7429417.5	1254.8	150	UG	63	301
SMRC-066	385478.1	7429435.7	1258.2	192	UG	58	298
SMRC-067	385459.7	7429446.5	1259.5	19	UG	52	302
SMRC-068	385424.3	7429446.0	1262.7	80	UG	64	250
SMRC-069	385466.7	7429386.2	1258.2	120	UG	65	306
SMRC-070	385405.8	7429422.3	1262.8	168	UG	60	299
SMRC-070A	385402.0	7429424.5	1262.9	130	UG	44	299
SMRC-071	385425.6	7429350.5	1260.1	150	UG	79	297
SMRC-072	385384.8	7429379.2	1264.3	180	UG	59	299
SMRC-072A	385369.2	7429383.2	1264.2	156	UG	43	299
SMRC-073	385414.0	7429302.6	1259.3	144	UG	64	298
SMRC-074	385375.7	7429321.3	1263.0	204	UG	62	301
SMRC-075	385342.2	7429341.8	1265.8	130	UG	63	299
SMRC-076	385327.2	7429291.3	1265.4	156	UG	64	298
SMRC-077	385369.1	7429211.2	1261.2	223	UG	63	300
SMRC-078	385336.7	7429231.5	1263.6	230	UG	63	301
SMRC-079	385313.3	7429242.6	1265.8	120	UG	64	298
SMRC-079A	385310.8	7429243.6	1265.9	180	UG	49	302
SMRC-080	385349.5	7429165.2	1262.1	186	UG	66	299

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
SMRC-081	385317.7	7429182.0	1265.3	150	UG	66	298
SMRC-082	385288.6	7429200.8	1267.1	140	UG	63	299
SMRC-083	385339.4	7429115.3	1262.7	180	UG	64	300
SMRC-084	385309.6	7429130.1	1265.3	162	UG	63	299
SMRC-085	385276.5	7429151.9	1268.2	150	UG	64	300
SMRC-086	385324.4	7429065.3	1261.3	200	UG	64	300
SMRC-087	385299.6	7429025.1	1260.8	200	UG	64	299
SMRC-088	385259.7	7429045.2	1264.7	150	UG	65	299
SMRC-089	385239.5	7428940.1	1262.7	219	UG	65	300
SMRC-090	385184.1	7428855.4	1265.0	216	UG	64	300
SMRC-092	385127.9	7428772.7	1267.3	250	UG	59	292
SMRC-094	385330.8	7429003.3	1258.8	210	UG	65	301
SMRC-095	385359.2	7429043.2	1258.1	200	UG	64	299
SMRC-096	385486.2	7429999.9	1308.4	21	UG	50	267
SMRC-096A	385470.2	7429999.7	1307.0	90	UG	48	264
SMRC-098	385526.1	7429750.0	1299.1	144	UG	60	270
SMRC-099	385551.1	7429899.7	1323.4	230	UG	60	269
SMRC-100	385525.1	7429849.8	1315.8	200	UG	59	268
SMRC-120	385487.3	7429950.0	1308.7	156	UG	59	270
SMRC-121	385556.7	7429949.8	1333.7	250	UG	63	267
SMRC-122	385560.6	7429949.8	1333.7	240	UG	79	263
SMRC-123	385555.9	7430000.0	1313.3	192	UG	64	268
SMRC-124	385593.3	7429999.9	1317.8	250	UG	64	270
SMRC-125	385635.7	7430049.8	1324.5	220	UG	59	267
SMRC-126	385579.0	7430049.9	1329.1	234	UG	59	269
SMRC-127	385639.5	7430099.9	1337.0	168	UG	58	270
SMRC-128	385594.7	7430149.8	1345.7	114	UG	64	269
SPD-01	385217.9	7429440.8	1278.4	80	RC	90	360
SPD-02	385236.7	7429381.7	1276.7	103	RC	75	270
SPD-03	385270.9	7429557.7	1276.5	73	RC	45	270
SPD-04	385263.9	7429317.1	1271.3	83.5	RC	60	270
SPD-05	385237.5	7429268.5	1273.1	66	RC	75	270
SPD-06	385247.3	7429226.7	1270.1	84	RC	75	270
SPD-07	385267.0	7429185.0	1270.1	81	RC	70	270
SPD-08	385222.0	7429152.3	1271.4	58	RC	70	300
SPD-09	385206.1	7429122.4	1272.2	35.5	RC	75	300
SPD-10	385178.9	7429093.0	1273.4	61	RC	80	300
V-07	385473.5	7430004.0	1293.0	94.5	UG	15	275
V-08	385473.5	7430004.0	1292.0	85.5	UG	57	275
V-09	385473.5	7430004.0	1292.0	72	UG	45	305
V-14	385586.1	7430244.9	1211.5	133	UG	-5	289

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
V-15	385586.2	7430245.0	1211.6	140.5	UG	-5	1
V-16	385601.0	7430273.4	1212.4	140.5	UG	5	1
VAL-01	385451.7	7432297.9	1345.9	11	UG	90	0
VAL-02	385452.8	7432295.7	1345.9	11	UG	90	0
VAL-03	385453.7	7432293.8	1345.9	11	UG	90	0
VAL-04	385454.8	7432291.2	1345.9	11	UG	90	0
VAL-05	385450.1	7432290.2	1345.9	11	UG	90	0
VAL-06	385448.1	7432289.2	1345.9	11	UG	90	0
VAL-07	385442.5	7432290.2	1345.9	11	UG	90	0
VAL-08	385372.7	7432313.2	1352.2	11	UG	90	0
VAL-09	385374.3	7432310.7	1351.8	11	UG	90	0
VAL-10	385367.1	7432307.4	1353.2	11	UG	90	0
VAL-100	385415.3	7432277.3	1350.8	8.6	UG	80	0
VAL-101	385415.6	7432271.7	1351.8	9.2	UG	80	0
VAL-102	385417.2	7432269.1	1351.8	9	UG	80	0
VAL-103	385418.7	7432266.6	1351.7	9.3	UG	80	0
VAL-104	385420.3	7432264.0	1351.4	9.3	UG	80	0
VAL-105	385421.8	7432261.4	1351.1	9.2	UG	80	0
VAL-106	385410.8	7432274.6	1352.3	8.9	UG	80	0
VAL-107	385416.8	7432274.8	1351.1	10	UG	80	0
VAL-108	385409.6	7432271.6	1352.9	9.8	UG	80	0
VAL-109	385411.2	7432269.0	1352.9	9.6	UG	80	0
VAL-11	385368.7	7432304.9	1353.4	11	UG	90	0
VAL-110	385412.7	7432266.4	1352.7	9.6	UG	80	0
VAL-111	385418.4	7432272.2	1351.1	9.4	UG	80	0
VAL-112	385419.9	7432269.6	1351.1	9.2	UG	80	0
VAL-113	385421.5	7432267.0	1351.0	9.5	UG	80	0
VAL-114	385414.1	7432274.3	1351.7	9.4	UG	80	0
VAL-115	385427.9	7432240.3	1347.7	9.3	UG	80	0
VAL-116	385429.4	7432237.7	1346.6	9.2	UG	80	0
VAL-117	385431.0	7432235.2	1345.6	9.8	UG	80	0
VAL-118	385450.6	7432300.2	1345.1	9.7	UG	90	0
VAL-119	385449.2	7432292.2	1345.9	9.5	UG	90	0
VAL-12	385370.3	7432302.3	1353.6	11	UG	90	0
VAL-120	385451.2	7432288.3	1345.9	9.6	UG	90	0
VAL-121	385444.9	7432296.6	1347.1	9.6	UG	90	0
VAL-122	385451.8	7432300.6	1344.6	9.6	UG	90	0
VAL-123	385440.0	7432297.1	1347.8	9.6	UG	90	0
VAL-124	385440.3	7432294.7	1347.8	9.4	UG	90	0
VAL-125	385438.0	7432293.5	1347.9	9.7	UG	90	0
VAL-126	385437.8	7432291.1	1345.9	9.6	UG	90	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-127	385439.9	7432290.7	1345.9	9.5	UG	90	0
VAL-128	385453.4	7432298.8	1345.9	9.6	UG	90	0
VAL-129	385435.4	7432295.2	1348.0	9.7	UG	90	0
VAL-13	385371.9	7432299.8	1353.5	11	UG	90	0
VAL-130	385432.8	7432293.9	1347.5	9.7	UG	90	0
VAL-131	385454.6	7432296.7	1345.9	9.6	UG	90	0
VAL-132	385447.1	7432303.1	1346.1	9.5	UG	90	0
VAL-133	385448.5	7432301.9	1345.7	8.4	UG	90	0
VAL-134	385368.6	7432300.1	1353.8	8.2	UG	90	0
VAL-135	385370.2	7432297.5	1353.6	10	UG	90	0
VAL-136	385367.5	7432297.0	1353.8	10	UG	90	0
VAL-137	385369.1	7432294.5	1353.4	10	UG	90	0
VAL-138	385370.7	7432291.9	1353.2	9.8	UG	90	0
VAL-139	385364.2	7432297.3	1353.6	9.6	UG	90	0
VAL-14	385373.5	7432297.2	1353.5	11	UG	90	0
VAL-140	385357.4	7432328.0	1353.3	9.7	UG	90	0
VAL-141	385365.8	7432294.8	1353.5	9.6	UG	90	0
VAL-142	385358.8	7432325.3	1353.4	9.4	UG	90	0
VAL-143	385367.4	7432292.2	1353.2	9.5	UG	90	0
VAL-144	385360.3	7432322.7	1353.2	9.7	UG	90	0
VAL-145	385369.0	7432289.7	1353.0	9.8	UG	90	0
VAL-146	385361.7	7432320.1	1353.3	9.5	UG	90	0
VAL-147	385363.1	7432317.4	1353.3	9.4	UG	90	0
VAL-148	385364.6	7432314.8	1353.2	9.3	UG	90	0
VAL-149	385352.4	7432320.7	1353.5	9.1	UG	90	0
VAL-15	385375.1	7432294.7	1353.7	11	UG	90	0
VAL-150	385353.9	7432318.1	1353.6	9.2	UG	90	0
VAL-151	385355.3	7432315.4	1353.7	9.2	UG	90	0
VAL-152	385377.8	7432292.0	1353.7	9.6	UG	80	0
VAL-153	385379.4	7432289.5	1353.6	9.2	UG	80	0
VAL-154	385381.0	7432286.9	1353.4	9	UG	80	0
VAL-155	385373.4	7432289.3	1353.2	8.8	UG	80	0
VAL-156	385375.0	7432286.7	1353.2	9.1	UG	80	0
VAL-157	385376.5	7432284.2	1353.0	9.3	UG	80	0
VAL-158	385371.7	7432287.0	1353.0	9	UG	80	0
VAL-159	385373.3	7432284.5	1352.9	8.9	UG	80	0
VAL-16	385375.9	7432308.1	1351.9	11	UG	90	0
VAL-160	385394.5	7432276.4	1353.7	8.6	UG	80	0
VAL-161	385394.9	7432266.0	1352.7	8.7	UG	80	0
VAL-162	385396.1	7432273.9	1353.7	9.1	UG	80	0
VAL-163	385396.5	7432263.5	1352.7	9.9	UG	80	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-164	385398.0	7432261.0	1352.7	10	UG	80	0
VAL-165	385387.4	7432273.1	1353.1	9.7	UG	80	0
VAL-166	385388.9	7432270.6	1353.0	9.3	UG	80	0
VAL-167	385390.5	7432268.1	1352.8	9.2	UG	80	0
VAL-168	385397.7	7432271.3	1353.5	9.2	UG	80	0
VAL-169	385393.6	7432258.2	1351.8	9.1	UG	80	0
VAL-17	385365.5	7432305.2	1353.5	11	UG	90	0
VAL-170	385395.2	7432255.7	1351.6	8.9	UG	80	0
VAL-171	385404.0	7432261.2	1353.0	9.2	UG	80	0
VAL-172	385406.9	7432256.9	1352.7	9.2	UG	90	0
VAL-173	385408.5	7432254.4	1352.4	9	UG	90	0
VAL-174	385407.3	7432246.5	1351.2	8.7	UG	90	0
VAL-175	385408.9	7432244.0	1350.5	9.7	UG	90	0
VAL-176	385410.5	7432241.5	1349.6	8.7	UG	90	0
VAL-177	385410.1	7432251.8	1352.2	8.7	UG	90	0
VAL-178	385399.8	7432253.6	1351.9	8.5	UG	90	0
VAL-179	385401.4	7432251.1	1351.5	9.1	UG	90	0
VAL-18	385367.1	7432302.6	1353.6	11	UG	90	0
VAL-180	385403.0	7432248.6	1351.4	9	UG	90	0
VAL-181	385414.9	7432244.2	1350.2	8.8	UG	90	0
VAL-182	385416.5	7432241.7	1349.4	8.6	UG	90	0
VAL-183	385418.1	7432239.1	1348.6	8.3	UG	90	0
VAL-184	385356.0	7432301.9	1353.2	8.2	UG	80	0
VAL-185	385346.4	7432312.4	1353.3	8.2	UG	80	0
VAL-186	385342.1	7432314.4	1352.8	9.5	UG	80	0
VAL-187	385354.0	7432310.1	1353.7	8	UG	80	0
VAL-188	385355.9	7432297.0	1353.0	9	UG	80	0
VAL-189	385375.7	7432319.5	1352.2	8.9	UG	90	0
VAL-19	385371.8	7432295.0	1353.4	11	UG	90	0
VAL-190	385374.4	7432316.5	1352.4	8.7	UG	90	0
VAL-191	385394.8	7432297.6	1353.0	8.4	UG	90	0
VAL-192	385396.3	7432295.1	1352.6	8.1	UG	90	0
VAL-193	385390.5	7432299.7	1353.2	7.8	UG	90	0
VAL-194	385392.0	7432297.2	1353.4	7.6	UG	90	0
VAL-195	385387.6	7432294.5	1354.2	9.4	UG	90	0
VAL-196	385389.1	7432291.9	1354.0	9.4	UG	90	0
VAL-197	385412.4	7432272.1	1352.4	9.2	UG	80	0
VAL-198	385413.9	7432269.5	1352.4	9	UG	80	0
VAL-199	385415.5	7432266.9	1352.3	9.3	UG	80	0
VAL-20	385357.3	7432333.6	1353.2	11	UG	90	0
VAL-200	385417.0	7432264.4	1352.0	9.4	UG	80	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-201	385418.5	7432261.8	1351.8	8.7	UG	80	0
VAL-202	385420.1	7432259.2	1351.5	8.6	UG	80	0
VAL-203	385421.6	7432256.6	1351.3	8.3	UG	80	0
VAL-204	385414.3	7432263.9	1352.5	8.1	UG	80	0
VAL-205	385415.8	7432261.3	1352.3	7.7	UG	80	0
VAL-206	385417.3	7432258.7	1352.0	7	UG	80	0
VAL-207	385418.9	7432256.2	1351.6	6.2	UG	80	0
VAL-208	385420.4	7432253.6	1351.3	5.4	UG	80	0
VAL-209	385406.4	7432272.0	1353.4	4.7	UG	80	0
VAL-21	385373.4	7432292.5	1353.4	11	UG	90	0
VAL-210	385407.9	7432269.4	1353.2	8.4	UG	80	0
VAL-211	385409.4	7432266.8	1352.9	8.2	UG	80	0
VAL-212	385401.9	7432269.3	1353.6	8	UG	80	0
VAL-213	385403.4	7432266.7	1353.5	7.8	UG	80	0
VAL-214	385405.0	7432264.1	1353.3	7.2	UG	80	0
VAL-215	385422.9	7432253.6	1351.0	6.5	UG	80	0
VAL-216	385423.2	7432248.0	1350.3	5.6	UG	80	0
VAL-217	385424.8	7432245.4	1349.5	4.6	UG	80	0
VAL-218	385426.3	7432242.9	1348.7	8.2	UG	80	0
VAL-219	385418.4	7432251.0	1351.3	7.9	UG	80	0
VAL-22	385358.7	7432331.0	1353.0	11	UG	90	0
VAL-220	385420.0	7432248.4	1350.8	7.5	UG	80	0
VAL-221	385421.5	7432245.8	1350.0	7.4	UG	80	0
VAL-222	385423.1	7432243.3	1349.2	7.1	UG	80	0
VAL-223	385424.6	7432240.7	1348.3	6.3	UG	80	0
VAL-224	385426.1	7432238.1	1347.2	5.5	UG	80	0
VAL-225	385427.7	7432235.5	1346.1	4.4	UG	80	0
VAL-226	385421.9	7432240.2	1348.5	7.6	UG	80	0
VAL-227	385423.4	7432237.6	1347.4	7.3	UG	80	0
VAL-228	385424.9	7432235.1	1346.3	6.9	UG	80	0
VAL-229	385433.5	7432246.0	1347.2	6.7	UG	80	0
VAL-23	385360.1	7432328.3	1352.8	11	UG	90	0
VAL-230	385435.1	7432243.5	1347.0	6.3	UG	80	0
VAL-231	385436.6	7432240.9	1346.1	5.4	UG	80	0
VAL-232	385438.2	7432238.3	1345.1	4.5	UG	80	0
VAL-233	385448.8	7432304.3	1345.3	7	UG	90	0
VAL-234	385454.9	7432289.2	1345.9	6.9	UG	90	0
VAL-235	385444.9	7432302.0	1346.7	6.6	UG	90	0
VAL-236	385446.4	7432300.5	1346.7	6.1	UG	90	0
VAL-237	385447.0	7432297.8	1346.5	5.7	UG	90	0
VAL-238	385447.8	7432294.1	1345.9	4.8	UG	90	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-239	385450.5	7432303.2	1344.8	4	UG	90	0
VAL-24	385361.6	7432325.7	1353.2	11	UG	90	0
VAL-240	385444.5	7432299.2	1347.2	6.2	UG	90	0
VAL-241	385442.7	7432300.4	1347.5	5.4	UG	90	0
VAL-242	385442.7	7432298.1	1347.6	4.6	UG	90	0
VAL-243	385443.1	7432295.8	1347.4	9.7	UG	90	0
VAL-244	385445.2	7432293.4	1345.9	9.5	UG	90	0
VAL-245	385446.8	7432291.1	1345.9	9.4	UG	90	0
VAL-246	385440.4	7432299.7	1347.7	9.5	UG	90	0
VAL-247	385438.0	7432298.5	1347.8	9.2	UG	90	0
VAL-248	385437.8	7432296.3	1348.0	9.2	UG	90	0
VAL-249	385435.7	7432297.5	1348.3	9.1	UG	90	0
VAL-25	385377.5	7432305.6	1352.2	11	UG	90	0
VAL-250	385432.9	7432296.4	1347.6	9.3	UG	90	0
VAL-251	385430.5	7432294.8	1347.6	9.3	UG	90	0
VAL-252	385430.4	7432292.3	1347.3	9.6	UG	90	0
VAL-253	385428.0	7432293.2	1347.0	9.2	UG	90	0
VAL-254	385455.7	7432294.8	1345.9	9	UG	90	0
VAL-255	385456.4	7432292.3	1345.9	8.9	UG	90	0
VAL-256	385373.1	7432307.6	1352.3	8.8	UG	90	0
VAL-257	385374.7	7432305.1	1352.7	9.6	UG	90	0
VAL-258	385376.3	7432302.5	1353.0	9	UG	90	0
VAL-259	385377.9	7432300.0	1353.2	8.8	UG	90	0
VAL-26	385363.0	7432323.1	1352.8	11	UG	90	0
VAL-260	385368.3	7432310.5	1352.6	9.7	UG	90	0
VAL-261	385369.9	7432307.9	1352.7	9.7	UG	90	0
VAL-262	385371.5	7432305.4	1353.1	9.4	UG	90	0
VAL-263	385373.1	7432302.8	1353.3	9.4	UG	90	0
VAL-264	385374.6	7432300.3	1353.4	9.5	UG	90	0
VAL-265	385376.2	7432297.8	1353.4	9.4	UG	90	0
VAL-266	385363.9	7432307.7	1353.4	9.4	UG	90	0
VAL-267	385362.7	7432304.6	1353.6	9.2	UG	90	0
VAL-268	385364.3	7432302.1	1353.7	9.1	UG	90	0
VAL-269	385365.9	7432299.6	1353.8	9	UG	90	0
VAL-27	385364.4	7432320.4	1352.9	11	UG	90	0
VAL-270	385359.5	7432305.0	1353.5	8.9	UG	90	0
VAL-271	385361.1	7432302.4	1353.6	9.3	UG	90	0
VAL-272	385362.6	7432299.9	1353.5	9.4	UG	90	0
VAL-273	385366.0	7432312.2	1352.9	9.3	UG	90	0
VAL-274	385355.6	7432325.8	1353.6	2.6	UG	90	0
VAL-275	385357.0	7432323.2	1353.6	2.5	UG	90	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-276	385358.4	7432320.6	1353.4	3	UG	90	0
VAL-277	385359.9	7432317.9	1353.5	3.2	UG	90	0
VAL-278	385361.3	7432315.3	1353.4	2.7	UG	90	0
VAL-279	385362.8	7432312.7	1353.3	2.1	UG	90	0
VAL-28	385365.9	7432317.8	1353.0	11	UG	90	0
VAL-280	385364.2	7432310.0	1353.2	1.9	UG	90	0
VAL-281	385351.4	7432328.1	1353.8	4	UG	90	0
VAL-282	385352.8	7432325.5	1353.7	3.8	UG	90	0
VAL-283	385354.2	7432322.8	1353.5	3.9	UG	90	0
VAL-284	385355.7	7432320.2	1353.6	4.1	UG	90	0
VAL-285	385357.1	7432317.6	1353.6	3.7	UG	90	0
VAL-286	385358.6	7432314.9	1353.6	3.2	UG	90	0
VAL-287	385360.0	7432312.3	1353.6	3	UG	90	0
VAL-288	385361.4	7432309.7	1353.4	2.6	UG	90	0
VAL-289	385349.6	7432326.0	1353.7	1.9	UG	90	0
VAL-29	385367.3	7432315.2	1352.9	11	UG	90	0
VAL-290	385351.0	7432323.3	1353.6	7.5	UG	90	0
VAL-291	385356.8	7432312.8	1353.7	7.6	UG	90	0
VAL-292	385358.2	7432310.2	1353.6	8	UG	90	0
VAL-293	385359.6	7432307.5	1353.5	8.3	UG	90	0
VAL-294	385370.0	7432312.7	1352.4	7.9	UG	90	0
VAL-295	385371.6	7432310.2	1352.2	8.2	UG	90	0
VAL-296	385382.2	7432294.8	1354.0	8.3	UG	80	0
VAL-297	385383.8	7432292.2	1353.8	7.9	UG	80	0
VAL-298	385377.7	7432287.3	1353.3	8.4	UG	80	0
VAL-299	385379.3	7432284.7	1353.1	8.2	UG	80	0
VAL-30	385368.8	7432312.5	1352.6	11	UG	90	0
VAL-300	385380.9	7432282.2	1353.2	7.4	UG	80	0
VAL-301	385385.4	7432289.7	1353.6	6.9	UG	80	0
VAL-302	385394.9	7432270.8	1353.3	7.1	UG	80	0
VAL-303	385396.5	7432268.3	1353.2	7.2	UG	80	0
VAL-304	385398.1	7432265.7	1353.2	6.4	UG	80	0
VAL-305	385399.7	7432263.2	1353.1	6.7	UG	80	0
VAL-306	385401.3	7432260.6	1352.9	7.6	UG	80	0
VAL-307	385399.6	7432258.4	1352.5	8.3	UG	80	0
VAL-308	385392.1	7432265.5	1352.6	8.7	UG	80	0
VAL-309	385393.7	7432263.0	1352.3	9	UG	80	0
VAL-31	385353.1	7432335.9	1353.6	11	UG	90	0
VAL-310	385395.3	7432260.4	1352.2	8.6	UG	80	0
VAL-311	385396.9	7432257.9	1352.2	6.9	UG	80	0
VAL-312	385398.5	7432255.3	1352.0	7.7	UG	80	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-313	385388.9	7432265.8	1352.7	8.6	UG	80	0
VAL-314	385390.5	7432263.3	1352.4	9.2	UG	80	0
VAL-315	385392.0	7432260.7	1352.1	9.4	UG	80	0
VAL-316	385399.3	7432268.8	1353.4	7.1	UG	80	0
VAL-317	385400.9	7432266.3	1353.4	7.1	UG	80	0
VAL-318	385402.4	7432263.7	1353.2	7.6	UG	80	0
VAL-319	385391.8	7432275.9	1353.3	8.5	UG	80	0
VAL-32	385354.5	7432333.2	1353.8	11	UG	90	0
VAL-320	385393.4	7432273.4	1353.4	9.4	UG	80	0
VAL-321	385404.2	7432256.4	1352.6	9.8	UG	90	0
VAL-322	385405.8	7432253.9	1352.3	9.9	UG	90	0
VAL-323	385407.4	7432251.3	1352.1	9.9	UG	90	0
VAL-324	385409.0	7432248.8	1351.7	7.3	UG	90	0
VAL-325	385410.6	7432246.2	1351.0	7.6	UG	90	0
VAL-326	385412.2	7432243.7	1350.2	7.8	UG	90	0
VAL-327	385413.7	7432241.1	1349.4	8.7	UG	90	0
VAL-328	385415.3	7432238.6	1348.7	9.4	UG	90	0
VAL-329	385412.1	7432238.9	1348.6	9.8	UG	90	0
VAL-33	385355.9	7432330.6	1353.5	11	UG	90	0
VAL-330	385404.6	7432246.0	1351.1	10.2	UG	90	0
VAL-331	385406.2	7432243.5	1350.3	10	UG	90	0
VAL-332	385407.7	7432240.9	1349.5	7.1	UG	90	0
VAL-333	385409.3	7432238.4	1348.4	6.8	UG	90	0
VAL-334	385411.7	7432249.3	1351.6	7.8	UG	90	0
VAL-335	385401.3	7432246.3	1350.7	7.8	UG	90	0
VAL-336	385402.9	7432243.8	1350.3	7.7	UG	90	0
VAL-337	385404.5	7432241.2	1349.4	7.4	UG	90	0
VAL-338	385406.1	7432238.7	1348.5	7.1	UG	90	0
VAL-339	385413.3	7432246.8	1350.9	6.9	UG	90	0
VAL-34	385379.1	7432303.1	1352.6	11	UG	90	0
VAL-340	385400.2	7432243.3	1349.7	6.7	UG	90	0
VAL-341	385401.7	7432240.7	1348.8	8.3	UG	90	0
VAL-342	385403.3	7432238.2	1348.0	8.4	UG	90	0
VAL-343	385348.1	7432314.6	1353.4	8.4	UG	80	0
VAL-344	385349.7	7432312.1	1353.5	7.1	UG	80	0
VAL-345	385344.8	7432315.0	1353.3	8.3	UG	80	0
VAL-346	385352.8	7432302.2	1353.0	8	UG	80	0
VAL-347	385354.4	7432299.7	1352.9	7.8	UG	80	0
VAL-348	385350.8	7432315.2	1353.6	7.5	UG	80	0
VAL-349	385350.0	7432301.7	1352.8	7.3	UG	80	0
VAL-35	385352.7	7432331.1	1354.0	11	UG	90	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-350	385352.4	7432312.6	1353.7	8.9	UG	80	0
VAL-351	385358.8	7432302.5	1353.5	8.9	UG	80	0
VAL-352	385360.3	7432299.8	1353.4	8.7	UG	80	0
VAL-353	385360.7	7432294.1	1353.1	8.5	UG	80	0
VAL-354	385357.4	7432294.5	1352.9	8.3	UG	80	0
VAL-355	385361.9	7432297.2	1353.3	7.1	UG	80	0
VAL-356	385363.4	7432294.7	1353.4	8	UG	80	0
VAL-357	385357.5	7432299.2	1353.3	7.6	UG	80	0
VAL-358	385374.6	7432326.9	1351.5	7.3	UG	90	0
VAL-359	385376.0	7432324.2	1351.6	9.4	UG	90	0
VAL-36	385354.1	7432328.5	1353.8	11	UG	90	0
VAL-360	385377.5	7432321.6	1352.0	9.2	UG	90	0
VAL-361	385378.9	7432319.0	1352.3	8.9	UG	90	0
VAL-362	385380.4	7432316.3	1351.9	9	UG	90	0
VAL-363	385377.1	7432316.9	1352.3	8.8	UG	90	0
VAL-364	385378.6	7432314.2	1351.9	8.5	UG	90	0
VAL-365	385375.8	7432313.9	1352.2	8.1	UG	90	0
VAL-366	385377.2	7432311.2	1351.4	7.1	UG	90	0
VAL-367	385382.1	7432324.1	1350.9	7.8	UG	90	0
VAL-368	385383.5	7432321.5	1351.1	9.4	UG	90	0
VAL-369	385384.9	7432318.8	1351.2	9.2	UG	90	0
VAL-37	385380.6	7432300.5	1353.2	11	UG	90	0
VAL-370	385387.1	7432310.5	1350.4	9.3	UG	90	0
VAL-371	385388.6	7432307.9	1350.7	9.1	UG	90	0
VAL-372	385390.2	7432305.4	1351.6	8.8	UG	90	0
VAL-373	385391.7	7432302.8	1352.3	8.4	UG	90	0
VAL-374	385393.2	7432300.2	1352.7	8	UG	90	0
VAL-375	385385.9	7432307.4	1350.9	7.4	UG	90	0
VAL-376	385387.4	7432304.9	1351.7	9.6	UG	90	0
VAL-377	385389.0	7432302.3	1352.6	7	UG	90	0
VAL-378	385385.7	7432302.7	1352.5	9.5	UG	90	0
VAL-379	385387.2	7432300.1	1353.4	9.3	UG	90	0
VAL-38	385383.7	7432287.5	1354.0	11	UG	80	0
VAL-380	385388.8	7432297.5	1353.8	9.1	UG	90	0
VAL-381	385390.3	7432295.0	1353.9	8.9	UG	90	0
VAL-382	385391.9	7432292.4	1353.9	8.6	UG	90	0
VAL-383	385383.0	7432302.2	1352.7	8.3	UG	90	0
VAL-384	385384.5	7432299.6	1353.4	7.9	UG	90	0
VAL-385	385386.0	7432297.1	1353.8	6.6	UG	90	0
VAL-386	385385.5	7432313.1	1351.1	6.3	UG	90	0
VAL-387	385423.3	7432258.8	1350.9	6.2	UG	80	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-388	385424.9	7432256.3	1350.7	7.7	UG	80	0
VAL-389	385411.0	7432264.3	1353.0	6.1	UG	80	0
VAL-39	385385.3	7432284.9	1354.0	11	UG	80	0
VAL-390	385412.5	7432261.7	1352.8	5.9	UG	80	0
VAL-391	385414.1	7432259.1	1352.5	4.6	UG	80	0
VAL-392	385415.6	7432256.5	1352.1	4.5	UG	80	0
VAL-393	385417.2	7432254.0	1351.8	3.5	UG	80	0
VAL-394	385405.2	7432268.9	1353.4	2.6	UG	80	0
VAL-395	385406.7	7432266.3	1353.2	1.6	UG	80	0
VAL-396	385408.3	7432263.8	1353.3	7	UG	80	0
VAL-397	385409.8	7432261.2	1353.1	6.5	UG	80	0
VAL-398	385411.3	7432258.6	1352.8	5.2	UG	80	0
VAL-399	385412.9	7432256.1	1352.4	5.3	UG	80	0
VAL-40	385386.9	7432282.4	1353.8	11	UG	80	0
VAL-400	385414.4	7432253.5	1352.0	5.8	UG	80	0
VAL-401	385416.0	7432250.9	1351.4	4.4	UG	80	0
VAL-402	385406.5	7432261.6	1353.1	3.4	UG	80	0
VAL-403	385408.1	7432259.0	1352.9	2.3	UG	80	0
VAL-404	385409.6	7432256.4	1352.6	1.3	UG	80	0
VAL-405	385411.2	7432253.9	1352.3	6.6	UG	80	0
VAL-406	385412.7	7432251.3	1351.9	6.3	UG	80	0
VAL-407	385423.0	7432264.5	1350.6	5.5	UG	80	0
VAL-408	385424.5	7432261.9	1350.3	4.7	UG	80	0
VAL-409	385426.1	7432259.3	1350.2	3.7	UG	80	0
VAL-41	385388.5	7432279.8	1353.6	11	UG	80	0
VAL-410	385427.3	7432256.3	1350.1	2.6	UG	80	0
VAL-411	385427.7	7432250.7	1349.9	5.3	UG	80	0
VAL-412	385429.2	7432248.1	1348.6	1.6	UG	80	0
VAL-413	385430.8	7432245.6	1348.5	7.3	UG	80	0
VAL-414	385432.3	7432243.0	1347.5	6.8	UG	80	0
VAL-415	385433.9	7432240.4	1346.6	6	UG	80	0
VAL-416	385435.4	7432237.8	1345.6	5.2	UG	80	0
VAL-417	385424.4	7432251.1	1350.5	4.3	UG	80	0
VAL-418	385426.0	7432248.5	1349.2	3.2	UG	80	0
VAL-419	385427.5	7432245.9	1349.3	2.1	UG	80	0
VAL-42	385382.5	7432284.4	1353.5	11	UG	80	0
VAL-420	385428.9	7432253.8	1349.8	4.5	UG	80	0
VAL-421	385429.1	7432243.4	1348.4	4.5	UG	80	0
VAL-422	385430.6	7432240.8	1347.4	3.4	UG	80	0
VAL-423	385432.1	7432238.2	1346.3	2.3	UG	80	0
VAL-424	385433.7	7432235.6	1345.3	3.2	UG	80	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-425	385421.7	7432250.6	1350.6	3	UG	80	0
VAL-426	385430.4	7432251.2	1349.3	2.1	UG	80	0
VAL-427	385432.0	7432248.6	1348.5	1.1	UG	80	0
VAL-428	385426.1	7432253.3	1350.3	6.3	UG	80	0
VAL-43	385384.1	7432281.8	1353.7	11	UG	80	0
VAL-44	385385.7	7432279.3	1353.5	11	UG	80	0
VAL-45	385376.1	7432289.8	1353.4	11	UG	80	0
VAL-46	385378.1	7432281.6	1352.8	11	UG	80	0
VAL-47	385379.7	7432279.1	1353.1	8.2	UG	80	0
VAL-48	385381.3	7432276.5	1353.3	8.3	UG	80	0
VAL-49	385374.9	7432282.0	1352.6	8.7	UG	80	0
VAL-50	385376.5	7432279.4	1352.7	9	UG	80	0
VAL-51	385378.1	7432276.9	1353.1	9.2	UG	80	0
VAL-52	385380.5	7432292.6	1353.9	8.6	UG	80	0
VAL-53	385382.1	7432290.0	1354.0	8.7	UG	80	0
VAL-54	385390.1	7432273.7	1353.2	9.1	UG	80	0
VAL-55	385391.7	7432271.1	1353.2	9.3	UG	80	0
VAL-56	385393.3	7432268.6	1353.0	7.8	UG	80	0
VAL-57	385385.7	7432270.9	1353.0	9.4	UG	80	0
VAL-58	385387.3	7432268.4	1352.9	9.4	UG	80	0
VAL-59	385402.5	7432254.2	1352.2	9.2	UG	90	0
VAL-60	385404.1	7432251.6	1352.0	9.4	UG	90	0
VAL-61	385405.7	7432249.1	1351.8	9.6	UG	90	0
VAL-62	385398.1	7432251.4	1351.3	9.5	UG	90	0
VAL-63	385399.7	7432248.9	1350.9	9.5	UG	90	0
VAL-64	385395.4	7432250.9	1351.0	9.7	UG	90	0
VAL-65	385397.0	7432248.3	1350.6	7.9	UG	90	0
VAL-66	385398.6	7432245.8	1350.1	9.4	UG	90	0
VAL-67	385347.6	7432320.3	1353.7	9.5	UG	80	0
VAL-68	385346.5	7432317.2	1353.5	9.6	UG	80	0
VAL-69	385354.4	7432304.5	1353.2	9.8	UG	80	0
VAL-70	385343.2	7432317.5	1353.1	9.6	UG	80	0
VAL-71	385349.2	7432317.7	1353.6	9.4	UG	80	0
VAL-72	385351.2	7432304.8	1353.2	9.2	UG	80	0
VAL-73	385348.4	7432304.3	1353.0	9.4	UG	80	0
VAL-74	385355.6	7432307.5	1353.4	9	UG	80	0
VAL-75	385357.2	7432305.0	1353.4	9.6	UG	80	0
VAL-76	385344.9	7432319.7	1353.4	8.8	UG	80	0
VAL-77	385359.1	7432296.7	1353.2	9.7	UG	80	0
VAL-78	385431.7	7432268.6	1346.6	9.2	UG	80	0
VAL-79	385433.2	7432266.1	1346.5	9.8	UG	80	0

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
VAL-80	385434.7	7432263.5	1347.0	8.2	UG	80	0
VAL-81	385436.3	7432260.9	1347.2	8.8	UG	80	0
VAL-82	385437.8	7432258.4	1346.7	9.8	UG	80	0
VAL-83	385439.4	7432255.8	1346.1	8.9	UG	80	0
VAL-84	385440.9	7432253.2	1345.9	9.4	UG	80	0
VAL-85	385428.9	7432268.2	1348.0	9	UG	80	0
VAL-86	385430.5	7432265.6	1347.8	9.2	UG	80	0
VAL-87	385432.0	7432263.0	1347.9	8.9	UG	80	0
VAL-88	385433.6	7432260.4	1348.1	8.6	UG	80	0
VAL-89	385435.1	7432257.9	1347.7	9.5	UG	80	0
VAL-90	385436.6	7432255.3	1347.2	9.6	UG	80	0
VAL-91	385438.2	7432252.7	1347.0	9.6	UG	80	0
VAL-92	385439.7	7432250.2	1346.6	9.8	UG	80	0
VAL-93	385441.3	7432247.6	1345.9	9.5	UG	80	0
VAL-94	385381.1	7432310.4	1351.1	9.5	UG	90	0
VAL-95	385382.6	7432307.8	1351.1	9.6	UG	90	0
VAL-96	385384.2	7432305.3	1351.6	9.3	UG	90	0
VAL-97	385378.3	7432309.9	1351.3	9.5	UG	90	0
VAL-98	385379.9	7432307.3	1351.6	9.4	UG	90	0
VAL-99	385381.4	7432304.8	1351.8	9.2	UG	90	0
VN-0	385467.4	7432220.2	1321.0	130	UG	7	270
VO-11	385454.3	7430067.1	1315.0	70.5	UG	90	360
VO-12	385454.3	7430065.1	1315.0	108	UG	90	360
X-1	385615.7	7430765.4	1352.7	35.5	RC	45	83
X-2	385616.4	7430765.3	1352.7	40	RC	65	83
X-3	385655.0	7430908.9	1364.0	61	RC	30	83
X-4	385653.8	7430909.2	1360.0	61	RC	0	83
X-5	385656.7	7430890.9	1358.7	70	RC	70	83
X-6	385635.3	7430858.7	1354.1	65.5	RC	-5	83
X-7	385635.9	7430858.6	1352.9	79	RC	15	83
X-8	385640.1	7430858.1	1352.1	55	RC	40	82
XC-1	386079.7	7430236.2	1161.1	91	RC	64	280
XC-2	386080.3	7430236.0	1161.2	111	RC	78	277
XC-3	386081.5	7430235.7	1161.1	130	RC	86	248
XC-4	385942.0	7431297.0	1341.0	103.5	RC	-2	75
XM-1	385800.1	7430443.4	1113.9	110	RC	49	237
XM-2	385828.6	7430459.6	1109.6	140.5	RC	51	309
XM-3	385827.6	7430460.4	1110.4	100	RC	10	308
XM-4	385829.1	7430459.0	1109.1	154	RC	7	305
XM-5	385799.5	7430442.5	1114.5	106	RC	16	237
XM-6	385800.9	7430443.6	1113.8	140.5	RC	69	240

Hole ID	East	North	Elevation	Depth	Type	Dip	Azimuth
XR-1	386086.1	7430232.6	1162.2	130	RC	8	116
XR-2	386086.2	7430232.6	1161.6	141	RC	26	116
XR-3	386085.8	7430232.7	1161.5	160	RC	35	116
XR-4	386060.7	7430174.3	1160.0	151	RC	5	117
XR-5	386060.7	7430174.6	1159.7	162	RC	20	117
XR-6	386060.5	7430174.0	1160.0	160.5	RC	35	117
XR-7	386101.4	7430599.1	1151.0	171	RC	0	51
XR-8	386102.6	7430552.4	1153.9	66	RC	0	6
XV-1	385521.0	7430132.0	1199.0	76	RC	7	270
XV-2	385521.0	7430131.6	1199.0	70	RC	28	270
XV-3	385521.8	7430135.0	1198.0	56.5	RC	6	314

Hole	From	To	CuT%	Length
M1090220	0	4.2	19.3	4.2
SMRC-086	67	85	4.1	18
M1090259	0	4.2	15.5	4.2
M1260472	0	6	10.1	6
SMR-134	45	73	2.1	28
SADDH-70	2	22	2.7	20
M1260204	0	6	8.4	6
M1070223	0	4.2	11.8	4.2
ARC27_M5	0	2.5	18.3	2.5
XC-2	100	109	5.1	9
M1260160	0	6	7.3	6
M1090137	0	2.6	16.2	2.6
M1170124	0	4.8	8.7	4.8
M1090114	0	4.2	9.4	4.2
M1090125	0	4.2	9.4	4.2
SMR-129	89	103	2.7	14
M1150124	0	6	6.1	6
M117016	0	6	5.9	6
M109077	0	5.5	6.4	5.5
CHS-1	12	27	2.2	15
M1370244	0	5.6	6	5.6
M1370192	0	5	6.5	5
M1370205	0	5.6	5.8	5.6
SMRC-098	79	93	2.3	14
M1150125	0	6	5.4	6
M127013	0	5	6.4	5

Hole	From	To	CuT%	Length
M13	0	2.113	15.1	2.113
M1370110	0	5	6.4	5
M1090126	0	4.2	7.2	4.2
RP-09-01	198	202	7.5	4
M1370220	0	5.1	5.5	5.1
SM-02-09	46	58	2.3	12
M121018	0	5.2	5.4	5.2
RP-06-08	48	58	2.8	10
M1370215	0	5	5.5	5
M1070218	0	4.2	6.5	4.2
M1290183	0	4.2	6.3	4.2
M1370249	0	5.5	4.8	5.5
M134059	0	5.9	4.5	5.9
011-RC7-03	164	172	3.3	8
M1070144	0	4.2	6.3	4.2
M1320285	0	5.5	4.8	5.5
M1090136	0	4.2	6.3	4.2
M1070226	0	4.2	6.2	4.2
079-RC7-01	294	306	2.1	12
M1210744	0	3	8.5	3
M1090337	0	4.2	6.1	4.2
M121024	0	4.2	5.9	4.2
RP-01-01	32	36	6	4
M1210629	0	5.6	4.3	5.6
M1090167	0	3.7	6.5	3.7
M1320270	0	6.1	3.9	6.1

Hole	From	To	CuT%	Length
SMR-129A	56	65	2.6	9
M11907	0	4.2	5.6	4.2
M12703	0	5	4.7	5
016-RC7-01	94	104	2.3	10
M14006	0	4.2	5.3	4.2
M109027	0	5.5	4	5.5
M1070221	0	4.2	5.2	4.2
M1260483	0	6	3.6	6
SADDH-46	16	20	5.4	4
M1090218	0	4.2	5.1	4.2
SADDH-40	20	30	2.1	10
M1130103	0	5	4.2	5
M1320279	0	6.8	3.1	6.8
RP-01-02	44	52	2.6	8
M117045	0	5.1	4.1	5.1
M1090271	0	4.2	4.9	4.2
M117097	0	5.1	4	5.1
M1370222	0	5	4.1	5
M117088	0	5.1	4	5.1
M127022	0	5	4	5
SADDH-36	26	30	5	4
RC6-SA-6	186	188	10	2
M127038	0	5	4	5
M1290186	0	4.2	4.7	4.2
M127028	0	5	3.9	5
SMRC-066	55	62	2.8	7
DTH-EXP-25	37	46	2.1	9
M1090293	0	6	3.2	6
M1290190	0	4.2	4.5	4.2
RC-12A	250	252	9.5	2
M1320323	0	4.6	4.1	4.6
M-10	229	234	3.7	5
M117032	0	8.9	2.1	8.9
M1090260	0	4.2	4.4	4.2
M1340279	0	4	4.5	4
M121042	0	4.2	4.2	4.2
M1210666	0	6.2	2.8	6.2
M1320218	0	4.2	4.2	4.2
M1070219	0	4.2	4.1	4.2
M119031	0	4.8	3.6	4.8
M1210187	0	4.2	4.1	4.2

Hole	From	To	CuT%	Length
M121041	0	4.2	4.1	4.2
DTH-EXP-16	20.5	23.5	5.6	3
M132042	0	4	4.2	4
M127016	0	5	3.4	5
M1320264	0	6.5	2.6	6.5
M1210490	0	5.6	3	5.6
M1090166	0	4.2	3.9	4.2
M127019	0	5	3.3	5
M1090239	0	4.2	3.9	4.2
M132043	0	4.2	3.9	4.2
M1320128	0	5.2	3.2	5.2
M121043	0	4.2	3.9	4.2
M1210336	0	5.3	3.1	5.3
M1150230	0	4	4	4
RC-12A	78	80	8	2
M1150180	0	4	4	4
M1370210	0	5.6	2.9	5.6
M121028	0	4.2	3.8	4.2
ARC65_M4	0	3.03	5.2	3.03
M1320294	0	6.3	2.5	6.3
SADDH-50	28	32	3.9	4
M1320263	0	6.5	2.4	6.5
M126010	0	4.2	3.7	4.2
M1090132	0	4.2	3.7	4.2
M1070178	0	2.1	7.4	2.1
M1340255	0	4	3.9	4
M1370112	0	5	3.1	5
M1290187	0	4.2	3.7	4.2
N06-08	11.5	17.5	2.6	6
ARC61_M3	0	3.13	4.9	3.13
M1070148	0	4.2	3.6	4.2
M117067	0	4.2	3.6	4.2
M1260450	0	6	2.5	6
M1090236	0	4.2	3.6	4.2
M1370245	0	5.5	2.7	5.5
RP-00-01	106	110	3.7	4
SADDH-72	0	2	7.5	2
M121082	0	5.5	RC-112.7	5.5
M1320247	0	5.4	2.7	5.4
SADDH-57	8	10	7.4	2

Hole	From	To	CuT%	Length
M1090120	0	4.2	3.5	4.2
M117095	0	5.1	2.9	5.1
RP-20-03	192	196	3.6	4
SMRC-070	44	51	2.1	7
M1130132	0	3.1	4.7	3.1
M1150409	0	4.2	3.5	4.2
M134064	0	5.7	2.5	5.7
SADDH-76	0	2	7.2	2
M1340109	0	4	3.6	4
SADDH-60	34	40	2.4	6
M107023	0	4.2	3.4	4.2
M134021	0	7	2.1	7
M121033	0	4.2	3.4	4.2
M1090219	0	4.2	3.4	4.2
SADDH-36	58	64	2.4	6
M1090208	0	4.2	3.4	4.2
SADDH-43	20	24	3.6	4
M1210716	0	3	4.7	3
RP-10-04	40	44	3.6	4
M1340294	0	4	3.5	4
RP-06-07	42	44	7.1	2
M1370178	0	5.4	2.6	5.4
M1370221	0	5	2.8	5
M1210550	0	5.3	2.6	5.3
M1070222	0	4.2	3.3	4.2
M1070156	0	5.1	2.7	5.1
M1260486	0	6	2.3	6
M1090264	0	4.2	3.3	4.2
M1320326	0	4.6	3	4.6
M1070163	0	4.2	3.3	4.2
M1090128	0	4.2	3.2	4.2
M1090237	0	4.2	3.2	4.2
M1260203	0	6	2.3	6
M1370247	0	5.5	2.5	5.5
SMR-129	116	120	3.4	4
M121025	0	4.2	3.2	4.2
M1150203	0	4	3.4	4
M1150204	0	4	3.4	4
M107078	0	2.7	4.9	2.7
RC6-15	338	340	6.7	2
M132012	0	4.5	2.9	4.5

Hole	From	To	CuT%	Length
M1090188	0	2.1	6.3	2.1
M1150394	0	4.2	3.1	4.2
M1150407	0	4.2	3.1	4.2
M1150221	0	4	3.3	4
M134044	0	5	2.6	5
M1370108	0	5.2	2.5	5.2
M1130137	0	4.2	3.1	4.2
M1320241	0	6	2.2	6
M1210492	0	5.6	2.3	5.6
M117011	0	4.5	2.9	4.5
M1090262	0	4.2	3.1	4.2
M1370262	0	4.6	2.8	4.6
M1260447	0	6	2.1	6
M1090204	0	4.2	3	4.2
M1090287	0	4.2	3	4.2
M1320444	0	4	3.2	4
RC-08	256	260	3.2	4
M1070158	0	3.5	3.6	3.5
ARC31_M7	0	2	6.3	2
M117044	0	5.1	2.5	5.1
M1370138	0	5.1	2.5	5.1
M121023	0	4.3	2.9	4.3
SMRC-084	61	65	3.1	4
M1090307	0	4.2	3	4.2
SMR-015	75	81	2.1	6
M1210477	0	5.6	2.2	5.6
M1070138	0	4.8	2.6	4.8
M_VILMA_6	0	2.336	5.3	2.336
M121032	0	4.2	2.9	4.2
M1290185	0	4.2	2.9	4.2
M132023	0	4.2	2.9	4.2
SADDH-34	10	14	3.1	4
M134047	0	5	2.5	5
M1340200	0	4	3.1	4
M1260157	0	6	2	6
M1130102	0	5	2.4	5
M1290199	0	4.2	2.9	4.2
M1340222	0	4	3	4
M1070139	0	5.2	2.3	5.2
M1260484	0	6	2	6
M134075	0	5	2.4	5

Hole	From	To	CuT%	Length
SADDH-35	66	70	3	4
M121034	0	5.2	2.3	5.2
M1070117	0	2.2	5.4	2.2
M1290207	0	4.2	2.8	4.2
C-04A	23.5	28	2.6	4.5
M1210781	0	3	3.9	3
M1320216	0	4.2	2.8	4.2
M1070115	0	4.2	2.8	4.2
M1150397	0	4.2	2.8	4.2
M1370186	0	4.9	2.4	4.9
M1070141	0	4.2	2.8	4.2
M1340197	0	4	2.9	4
M107056	0	4.2	2.7	4.2
SADDH-61	0	4	2.9	4
M1370243	0	5.6	2.1	5.6
M1070159	0	4.2	2.7	4.2
SA-13	23	27	2.9	4
M1370248	0	5.5	2.1	5.5
M1090342	0	4.2	2.7	4.2
M1370214	0	5	2.3	5
M121039	0	4.2	2.7	4.2
SMRC-072	92	97	2.3	5
M1190222	0	4.2	2.7	4.2
M1370274	0	4.6	2.5	4.6
M117068	0	4.2	2.7	4.2
M1210475	0	5.6	2	5.6
M1370111	0	5.6	2	5.6
M1130101	0	5	2.2	5
M1320420	0	4	2.8	4
M117089	0	4.3	2.6	4.3
M1320223	0	4.2	2.6	4.2
M1340219	0	4	2.8	4
M1340315	0	4	2.8	4
SI-15	90	94.5	2.4	4.5
M1090138	0	4.2	2.6	4.2
M1090345	0	4.2	2.6	4.2
M1150393	0	4.2	2.6	4.2
M1290148	0	4.2	2.6	4.2
M1290201	0	3.8	2.9	3.8
M115082	0	3	3.6	3
M1320442	0	4	2.7	4

Hole	From	To	CuT%	Length
M1210731	0	3	3.6	3
M121027	0	4.2	2.6	4.2
M1190290	0	5	2.2	5
M1210768	0	3	3.6	3
M1210734	0	3	3.6	3
ARC77_M4	0	3.34	3.2	3.34
M121050	0	4.2	2.5	4.2
M1370259	0	4.6	2.3	4.6
M119082	0	4.2	2.5	4.2
M129072	0	2.2	4.7	2.2
M1320322	0	4.6	2.3	4.6
M1170103	0	5	2.1	5
M1090129	0	4.2	2.5	4.2
M1090217	0	4	2.6	4
ARC23_M3	0	2.3	4.5	2.3
M1090165	0	4.2	2.5	4.2
M1210393	0	4.7	2.2	4.7
M1150389	0	4.2	2.4	4.2
M1150226	0	4	2.6	4
M1370160	0	4.9	2.1	4.9
M1090258	0	2.1	4.9	2.1
M107014	0	4.2	2.4	4.2
M119097	0	4.2	2.4	4.2
M127027	0	5	2	5
082-RC7-01	84	86	5.1	2
M1090286	0	4.2	2.4	4.2
M1340223	0	4	2.5	4
M119095	0	4.3	2.4	4.3
M1320465	0	4	2.5	4
M107030	0	4.2	2.4	4.2
011-RC7-03	264	266	5	2
M121031	0	4.2	2.4	4.2
M1320443	0	4	2.5	4
M1290203	0	4.2	2.4	4.2
RP-10-05	56	58	5	2
M1370125	0	4.8	2.1	4.8
M1070147	0	4.2	2.3	4.2
M1370361	0	4.2	2.3	4.2
M1340265	0	4	2.5	4
M1090209	0	4.2	2.3	4.2
M1150402	0	4.2	2.3	4.2

Hole	From	To	CuT%	Length
M1340280	0	4	2.4	4
M1090202	0	4.2	2.3	4.2
M1070207	0	4.2	2.3	4.2
M1370389	0	4.2	2.3	4.2
SMR-009	59	63	2.4	4
M132013	0	4.5	2.1	4.5
M1340112	0	4	2.4	4
M1070205	0	4.2	2.3	4.2
M1090189	0	4.2	2.3	4.2
M1090127	0	4.2	2.3	4.2
M1290200	0	4.2	2.3	4.2
M1340338	0	4	2.4	4
M1190108	0	2.7	3.5	2.7
M1090300	0	4.2	2.3	4.2
M1290150	0	3.7	2.6	3.7
M1320319	0	4.6	2.1	4.6
M1070213	0	4.2	2.2	4.2
M1340107	0	4	2.4	4
RP-07-06	138	142	2.3	4
M1370398	0	4.2	2.2	4.2
M113043	0	4	2.3	4
M107093	0	4.2	2.2	4.2
M121026	0	4.2	2.2	4.2
M121046	0	4.2	2.2	4.2
SI-04	19.5	24	2.1	4.5
M1150406	0	4.2	2.2	4.2
M119081	0	4.2	2.2	4.2
VN-0	40	43	3.1	3
RM-1	49	52	3.1	3
M1070143	0	4.2	2.2	4.2
M1070160	0	4.2	2.2	4.2
M1090162	0	4.2	2.2	4.2
M1320225	0	4.2	2.2	4.2
SL-14	22	25	3	3
M1170168	0	4.2	2.2	4.2
M1320446	0	4	2.3	4
M1340217	0	4	2.3	4
ARC69_M4	0	3.23	2.8	3.23
M1290202	0	4.2	2.1	4.2
RP-11-04	130	132	4.5	2
M1070146	0	4.2	2.1	4.2

Hole	From	To	CuT%	Length
M1090244	0	4.2	2.1	4.2
M1090194	0	4.2	2.1	4.2
M1130161	0	4.2	2.1	4.2
M1150276	0	4.2	2.1	4.2
M121022	0	4.2	2.1	4.2
M1320437	0	4	2.2	4
M1130147	0	4.2	2.1	4.2
M1190225	0	4.2	2.1	4.2
M113013	0	4	2.2	4
M1150222	0	4	2.2	4
M1290204	0	4.2	2.1	4.2
M1290205	0	4.2	2.1	4.2
M107027	0	4.2	2.1	4.2
M1090168	0	4.2	2.1	4.2
M1090246	0	4.2	2.1	4.2
M109099	0	4.2	2.1	4.2
M1340148	0	4	2.2	4
M1190320	0	3	2.9	3
M1090123	0	4.2	2	4.2
M129071	0	4.2	2	4.2
M1090212	0	3.4	2.5	3.4
ARC77_M1	0	2.3	3.7	2.3
086-RC7-02	278	282	2.1	4
M1320460	0	4	2.1	4
M1320463	0	4	2.1	4
M1340147	0	4	2.1	4
M1340191	0	4	2.1	4
M1340241	0	4	2.1	4
M1090115	0	4.2	2	4.2
M14004	0	2	4.2	2
M1320378	0	4	2.1	4
SM-01-09	46	49	2.8	3
M1090139	0	2.8	3	2.8
RC6-SA-9	146	148	4.1	2
M1340202	0	4	2.1	4
ARC41_M3	0	2.59	3.2	2.59
RP-00-05	96	98	4	2
M1370321	0	3.3	2.4	3.3
M113044	0	4	2	4
M1320421	0	4	2	4
M1090116	0	2.1	3.8	2.1

Hole	From	To	CuT%	Length
SMRC-099	204	207	2.7	3
M1090193	0	3.1	2.6	3.1
RC-11	128	130	4	2
SL-02	38	40	3.9	2
M1290181	0	2.5	3.1	2.5
M1190316	0	3	2.6	3
ARC29_M4	0	2.4	3.2	2.4
M1090210	0	2	3.9	2
ARC57_M3	0	3.42	2.3	3.42
M1370397	0	3.2	2.4	3.2
M1090133	0	2.7	2.9	2.7
012-RC7-01	222	224	3.9	2
085-RC7-02	102	104	3.8	2
RP-04-02	80	82	3.8	2
SI-11	37.5	40.5	2.5	3
M129073	0	2.1	3.6	2.1
F12-08	58	61	2.5	3
SADDH-44	24	26	3.7	2
SADDH-15	36	38	3.7	2
M1070189	0	2.2	3.3	2.2
M1090187	0	2.7	2.7	2.7
RC6-SA-7	90	92	3.6	2
M-09	56	58	3.6	2
SMRC-066	43	45	3.5	2
SDD-13	76.6	79	2.9	2.4
RP-01-02	12	14	3.5	2
SMRC-084	117	120	2.3	3
M129078	0	2.1	3.3	2.1
080-RC7-01	230	232	3.4	2
RP-04-02	92	94	3.4	2
067-RC7-01	168	170	3.4	2
N-15	80.5	83.5	2.2	3
RP-00-02	42	44	3.3	2
SDD-13	446.5	448.85	2.8	2.35
RC6-25	152	154	3.3	2
ARC47_M3	0	3.12	2.1	3.12
M132048	0	2.1	3.1	2.1
ARC61_M4	0	3.13	2	3.13
M1070136	0	2.2	2.8	2.2
A-007	0	3	2.1	3
M1070116	0	2.2	2.8	2.2

Hole	From	To	CuT%	Length
DTHMG-02-03	98	100	3.1	2
016-RC7-01	232	234	3	2
SADDH-67	118	120	3	2
M1190221	0	2.1	2.8	2.1
RC6-11	218	220	3	2
RC-04	192	194	2.9	2
SMRC-087	148	150	2.9	2
RP-09-06	138	140	2.9	2
ARC25_M4	0	2.72	2.1	2.72
SDD-13	69.6	71.6	2.9	2
RP-12-05	56	58	2.9	2
RP-11-04	72	74	2.9	2
SADDH-03	26	28	2.9	2
SADDH-44	0	2	2.9	2
M1090285	0	2.1	2.7	2.1
SADDH-04	0	2	2.8	2
RC6-12	210	212	2.8	2
RC6-SA-8	64	66	2.8	2
DTHTS-02-01	58	60	2.8	2
RP-00-02	174	176	2.8	2
RC-05	216	218	2.8	2
SL-01	37	39	2.7	2
M1090269	0	2	2.7	2
SADDH-41	40	42	2.7	2
M119058	0	2.7	2	2.7
M33	0	2.087	2.6	2.087
M1190232	0	2.5	2.1	2.5
087-RC7-01	224	226	2.7	2
SADDH-54	6	8	2.7	2
082-RC7-02	196	198	2.7	2
RP-06-01	146	148	2.7	2
RP-01-02	32	34	2.7	2
RC6-5	112	114	2.6	2
RC6-SA-7	102	104	2.6	2
079-RC7-01	312	314	2.6	2
SDD-25	221	223	2.6	2
M1290191	0	2.1	2.4	2.1
SADDH-59	40	42	2.5	2
RP-08-06	64	66	2.5	2
M1070131	0	2.2	2.3	2.2
RC-04	184	186	2.5	2

Hole	From	To	CuT%	Length
SADDH-12	4	6	2.4	2
M1370347	0	2.1	2.3	2.1
RP-19-03	132	134	2.4	2
RP-09-07	106	108	2.4	2
SMR-134	86	88	2.4	2
SADDH-33	36	38	2.4	2
RP-00-05	80	82	2.3	2
M1070187	0	2.2	2.1	2.2
SADDH-77	12	14	2.3	2
087-RC7-01	218	220	2.3	2
RP-12-02	64	66	2.3	2
M1150507	0	2.2	2.1	2.2
RP-10-05	122	124	2.3	2
080-RC7-01	138	140	2.3	2
082-RC7-02	102	104	2.3	2
RC6-SA-9	156	158	2.2	2
RP-06-02	46	48	2.2	2
RP-20-03	136	138	2.2	2
RP-11-04	190	192	2.2	2
RC6-SA-2	48	50	2.2	2
SADDH-59	28	30	2.2	2

Hole	From	To	CuT%	Length
SADDH-44	6	8	2.2	2
M14002	0	2.1	2.1	2.1
AL-02-01	116	118	2.2	2
RP-07-05	84	86	2.2	2
RC-07	54	56	2.2	2
RP-20-03	232	234	2.2	2
RCH093-001	81	83	2.2	2
RC-09	182	184	2.1	2
SMRC-077	156	158	2.1	2
SADDH-64	106	108	2.1	2
SADDH-06	0	2	2.1	2
RP-01-04	28	30	2.1	2
SADDH-11	0	2	2.1	2
087-RC7-01	144	146	2.1	2
RC6-SA-12	74	76	2.1	2
SADDH-37	22	24	2.1	2
AL-02-01	46	48	2	2
RC-08	184	186	2	2
012-RC7-02	144	146	2	2
RC6-8	176	178	2	2

Criteria	JORC Code explanation	Commentary
Data aggregation methods	▪ In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. ▪ Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. ▪ The assumptions used for any reporting of metal equivalent values should be clearly stated.	▪ Data is not known to have been aggregated with grade truncations. ▪ Metal equivalents were not calculated for the project.

Criteria	JORC Code explanation	Commentary
Relationship between mineralisation widths and intercept lengths	▪ These relationships are particularly important in the reporting of Exploration Results. ▪ If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. ▪ If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	▪ Drill holes at the project were generally oriented to cut across the mineralised zone at a high angle to the mineralisation, but drill intersections are not true thicknesses. ▪ Mineralisation is interpreted to dip steeply to the east in general, at angles of 70 to 80 degrees, with the orientation of mineralisation in the volcanic units immediately east of the granodiorite at a lower angle dipping towards the east. Drilling is predominantly towards the west.
Diagrams	▪ Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	▪ Maps and tables are shown in the body of report and in the supporting NI 43-101 report. ▪ Drill intersections
Balanced reporting	▪ Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	▪ Given the quantity of assays it is not possible to report the assay results from pre 2021 historical drilling samples. ▪ Graphics are provided in the announcement showing relevant information. ▪ In the opinion of the CP the Information provided gives a balanced view of the project and the potential.
Other substantive exploration data	▪ Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	▪ High resolution ground magnetic survey data was obtained over the project, as was Aster satellite data. ▪ The project is an operating mine, with SX-EW production of cathode copper. Historically metallurgical testing has been conducted. ▪ The groundwater level is very deep in this location in the Atacama Desert of northern Chile, with groundwater not observed in mine workings. ▪ Limited bulk density samples were analysed historically and this will be resolved in the upcoming exploration program.
Further work	▪ The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). ▪ Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	▪ Planned work on the project includes an evaluation of current mining operations, with a view to optimising the production. In addition, there will be evaluation of the potential to extract mineralisation with expanded open pit operations; an evaluation of the potential production from the deeper sulphide mineralisation; evaluation of any residual potential from historical leach heaps and evaluation of exploration potential in the much less explored concessions in the south.

APPENDIX 2
JORC Code, 2012 Edition – Table 1 continued

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in the preceding section also apply to this section.)
The resource discussed is historical, foreign and non JORC compliant.

Criteria	JORC Code explanation	Commentary
Database integrity	▪ Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. ▪ Data validation procedures used.	▪ Data for the project was compiled in excel sheets. This data was revised by Geoinvest, as part of their verification sampling in 2025, preparing information for resource estimation. ▪ Data was plotted to check the spatial location and relationship to drill hole locations on historical maps.
Site visits	▪ Comment on any site visits undertaken by the Competent Person and the outcome of those visits. ▪ If no site visits have been undertaken indicate why this is the case.	▪ A company representative visited the project during January and February, and confirmed the presence of original drill core and associated information. Multiple visits to site by consultants in supporting disciplines of geology, structural geology and mining engineering have been conducted, as part of the technical program to support changes to the mine.
Geological interpretation	▪ Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. ▪ Nature of the data used and of any assumptions made. ▪ The effect, if any, of alternative interpretations on Mineral Resource estimation. ▪ The use of geology in guiding and controlling Mineral Resource estimation. ▪ The factors affecting continuity both of grade and geology.	▪ The project is a manto-style deposit that is possibly related to porphyry intrusives. This type of mineralisation is common in the coastal belt of northern Chile. However, in the SA mineralisation, a significant part of the mineralisation is present as oxide copper minerals within Jurassic intrusive rocks, with mineralisation outcropping at surface over extensive strike length. The structures hosting mineralisation are clear from the extensive underground workings. However, a more detailed structural geological evaluation is being undertaken to increase the level of detail of information for updated domaining of the geology and resource estimation. ▪ A significant part of the information is historical and the level of documentation regarding information collection is not exhaustive. The assumptions made are that the survey, assay and geological data were fit for the purpose of the original resource estimation. The survey, assay and geological data will be evaluated further as part of the validation activities related to the resource update. ▪ An alternative interpretation of the geology, and hence mineral resource, would have some impact on the final estimate number, as the interpretation depends on the tightness of the estimation around drilling and underground intersection points. The validation activities are planned to compare the results of the upcoming drilling with historical drilling and underground sampling.

Criteria	JORC Code explanation	Commentary
Geological interpretation **continued**	■ Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. ■ Nature of the data used and of any assumptions made. ■ The effect, if any, of alternative interpretations on Mineral Resource estimation. ■ The use of geology in guiding and controlling Mineral Resource estimation. ■ The factors affecting continuity both of grade and geology.	■ Geology is used in guiding the vein and fracture hosted mineralisation in the mineralisation model for the resource estimate. More detailed structural information and drilling between the known mineralised structures will allow more detailed control of the structurally controlled mineralisation in the estimation. ■ Continuity in grade depends on the location within the deposit, with the highest continuity vertically and laterally along the controlling vein/fault structures. ■ Continuity in the geology depends on the faulting and fracturing in the host rocks.
Dimensions	■ The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.	■ The deposit has been drilled in three principal mine areas, with oxide mineralisation predominant and deep holes intersecting sulphide mineralisation with chalcopyrite, with the deepest drillhole approximately 900m long. ■ The mineral resource dimensions consist of the Roxana deposit extending 1800m N to S; Chabuca–Rebeca extending 1600m N to S and Nicolasa extending 1900m N to S. ■ The mineralisation consists of different structural zones that dip in a generally eastern orientation, though varying between deposits, shallowing from the granodiorite in the west to the volcanics in the east. Mineralisation is related to the principal fracture zones and appears to be less developed between these structures, with drilling to establish what subsidiary structures exist between the principal structures in the resource drilling program. ■ Mineralisation varies from 200m to more than 500m in defined vertical extent, though the true depth extent may be much deeper in the sulphide zone, which has not been fully defined. Mineralisation also extends north and south of the mining area, which will be a evaluated further in the future, following estimation of resources in the mining area.

Criteria	JORC Code explanation	Commentary
Estimation and modelling techniques	▪ The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parametres and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parametres used. ▪ The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data. ▪ The assumptions made regarding recovery of by-products. ▪ Estimation of deleterious elements or other non-grade variables of economic significance (e.g. sulphur for acid mine drainage characterisation). ▪ In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed. ▪ Any assumptions behind modelling of selective mining units. ▪ Any assumptions about correlation between variables. ▪ Description of how the geological interpretation was used to control the Resource estimates. ▪ Discussion of basis for using or not using grade cutting or capping. ▪ The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.	▪ The estimation undertaken by Geoinvest is considered to be reasonable and appropriate for the deposit style, but improved structural information incorporated in the geological and resource models would allow approvement to domaining and estimation, together with collection of rock density data. ▪ The foreign estimation was undertaken based on the total copper content values, with the average CuS value approximately 0.83 of the CuT value, with this factor applied to obtain the CuS estimate. Future assaying will include both CuT and CuS values. ▪ An average density value of 2.74 t/m³ was considered for all estimation domains and units (comprising granodiorite, diorite and broadly andesitic volcanic rocks). No supporting documentation is available for the application of this value and density measurements will be made on drill core and material from drill cuttings from the upcoming drilling program, to provide more certainty around density in the modelling. ▪ Grade shell: ≥ 0.3% CuT were defined by assays and geological interpretation, with a Vein-style setting. Implicit Leapfrog modelling was geologically constrained by explicit EW cross sections through the deposit. ▪ Estimation was undertaken with ordinary kriging. ▪ Search ellipses were oriented along 350 degrees or 15 degrees, depending on the deposit. The dip of the ellipse depends on the orientation of the mineralisation down dip, varying between -45 and -85 degrees, Search ellipses were isotropic. ▪ The estimation was undertaken with 4 x 4 x 4m blocks for all areas, except for Roxana, where 2.5 x 2.5 x 2.5m blocks where used. ▪ No cutting or capping of mineralisation was undertaken. ▪ The estimate was for copper and no other elements.
Moisture	▪ Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.	▪ It is unknown whether the tonnage was estimated on a dry basis or with natural moisture. Considering the environment, which is hyper-arid it is considered the estimate was on a natural moisture basis and samples were essentially dry.

Criteria	JORC Code explanation	Commentary
Cut-off parametres	■ The basis of the adopted cut-off grade(s) or quality parametres applied.	■ The resource used manually interpreted grade shellso of 0.3% and was presented with a cut-off grade of 0.4% Cu applied for total copper. The 0.3% grade shells are believed to be based on economic parametres from operation of the SA mine. ■ The estimation only encompasses oxide material that can be processed in the site processing plant.
Mining factors or assumptions	■ Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parametres when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.	■ The deposit is amendable to underground and also open pit mining, with an initial pit shell design that suggests a significant part of the oxide mineralisation can be extracted from open pit mining. Current underground mining is in stopes of approximately 6m wide, as a minimum dimension. ■ Given the outcrop of parts of the deposits open pit mining could supplement underground production and this will be an area of detailed study, to define future mining plans. Consideration of current economics would be required to assess the basis of extraction with current commodity prices. ■ A global slope angle for the conceptual pit design was 52 degrees, which has not been subject to optimisation. ■ Initial evaluation of stripping ratio for the potential open pit development suggested a ratio of 5:1 for the Chabuca-Rebeca/Roxana sectors and 6.7: 1 for the Nicolasa sector.
Metallurgical factors or assumptions	■ The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parametres made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	■ Some metallurgy has been conducted on the deposit, which production shows is highly amenable to SX-EX processing and has a high overall proportion of soluble to total copper. The deposit ore is currently being processed from multiple different workings in the project SX-EW plant. ■ Chalcosite material encountered at the base of the oxide zone is considered to be leachable, with optimum results obtained using saline water. Metallurgical assessment of this material is planned to optimise future processing of this ore. ■ Detailed metallurgy has not been conducted on the deeper chalcopyrite sulphide mineralisation, which is an area for further study.

Criteria	JORC Code explanation	Commentary
Environmental factors or assumptions	▪ Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.	▪ Waste disposal currently takes place on site in waste dumps, with the mineralised material laid out on leach pads for acid extraction of the soluble copper. ▪ The process uses sulphuric acid, a well-established processing chemical in Chile and globally. The project currently does not process any sulphide mineralisation and is located in an extremely low rainfall area, so there is essentially no acid drainage risk from the material mined.
Bulk density	▪ Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples. ▪ The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit. ▪ Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.	▪ The specific gravity for the oxide mineralisation was assumed at 2.74 g/cc, throughout the deposit. It is not clear how this value is arrived at, but is a typical density applicable to intrusive or volcanic rocks. ▪ Detailed measurements should be made on future drill core and drill cuttings to improve this aspect of the future resource estimation.
Classification	▪ The basis for the classification of the Mineral Resources into varying confidence categories. ▪ Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data). ▪ Whether the result appropriately reflects the Competent Person's view of the deposit.	▪ The 2025 resource is classified as Measured, Indicated and Inferred Resources. The resource classification is based around the number of drillholes encountered within the search ellipse volume. Input data will be further validated for the next resource estimation, which will include extensive drilling by Cobre. ▪ The classification is considered by the Competent Person to be reasonable, based on the available data, but is a foreign estimate where historical information has only been partially validated. Future estimation will require the addition of focused structural geological data, improved density data and validation of assays which are mostly from the on-site laboratory.

Criteria	JORC Code explanation	Commentary
Audits or reviews	▪ The results of any audits or reviews of Mineral Resource estimates	▪ An audit of the most recent resource estimate will be conducted as part of the work that is planned by Cobre.
Discussion of relative accuracy/confidence	▪ Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the Resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate. ▪ The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used. ▪ These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	▪ Based on the available information (which does not include significant QA/QC sampling, such as standards and duplicates) the estimate appears to be reasonable. However, this will be the subject of an in depth evaluation. ▪ The drill core has been sighted by a company representative and a limited number of intersections have been evaluated. The geological interpretation and assay results rely on the original data, which was partially verified in 2025 by Geoinvest. Consequently, the result is not consistent with the JORC code and cannot be relied upon. ▪ In order to validate the historical resource, a proportion of the historical core and cuttings will be re-assayed in a selection of holes and soluble copper assays will be completed to allow estimation throughout the deposit. ▪ New measurements of specific gravity would be made to check the original results. Location and surveying of drill holes will also be completed in more detail. ▪ The competent person notes the information in this market announcement provided under rules ASX rules 5.12.2 to 5.12.7 is an accurate representation of the available data and studies for the material mining project. This statement include information referred to in rule 5.22(b) and (c).

APPENDIX 2
JORC Code, 2012 Edition – Table 1 continued

Section 4 Estimation and Reporting of Mineral Reserves

(Criteria listed in the preceding section also apply to this section.)
The reserve discussed is foreign and non JORC compliant.

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	▪ Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve. ▪ Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.	▪ The mineral resources used as the basis for the reserve estimation were those derived by Geoinvest in 2025. Some of these estimates were largely based on internal data compilation and estimates. ▪ The Mineral Resources were reported inclusive of the Mineral Reserves. The Mineral Resources were also inclusive of historical extraction, which was not extracted from the resources at the time of estimation, but is required to be undertaken as part of activities to convert the resources to JORC compliance.
Site visits	▪ Comment on any site visits undertaken by the Competent Person and the outcome of those visits. ▪ If no site visits have been undertaken indicate why this is the case.	▪ The JORC Competent Person, has visited the project during February, 2026, following the visit by Cobre's CEO and a team of consulting engineers, who visited the project over a period of 3 weeks during January and February 2026, and confirmed the presence of original drill core and associated information and undertook extensive discussions with the staff on site, evaluation of mining activities, work conducted, past exploration and development activities and workflows.
Study status	▪ The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves. ▪ The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.	▪ The project is a producing mine, which has a long production history of open pit and underground production. It is not known whether studies equivalent to a Pre-Feasibility study were historically completed, given the long mining history of the project. ▪ The project has more recently been subject to third party evaluations of the project geology and estimation of project resources. This included work undertaken by Geoinvest, who partially verified historical data, evaluated the geology and estimated resources. ▪ **This study represents a conceptual-level assessment, carried out based on the quantity and quality of information currently available. It is not intended to support investment decisions nor to be submitted to a stock exchange.** The aim is to identify technical and economic value opportunities for the project and to establish recommendations that can serve as a basis for subsequent phases and more advanced evaluations.

Criteria	JORC Code explanation	Commentary
Study status **continued**	▪ The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves. ▪ The Code requires that a study to at least Pre-Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.	▪ Geoinvest also undertook an initial estimation of reserves, which is considered to be early stage and not optimised, but is based on actual mining cost metrics, which are considered to be of at least Pre-Feasibility confidence. This study is useful for evaluating different options for the project going forward and help identify key areas for further study to advance the project, and additional information on the Modifying Factors to be evaluated for future reserve estimation.
Cut-off parametres	▪ The basis of the cut-off grade(s) or quality parametres applied.	▪ The cut-off grade of 0.4% CuT was used for the resource and the reserve, based on the resource.
Mining factors or assumptions	▪ The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design). ▪ The choice, nature and appropriateness of the selected mining method(s) and other mining parametres including associated design issues such as pre-strip, access, etc. ▪ The assumptions made regarding geotechnical parametres (eg pit slopes, stope sizes, etc), grade control and pre-production drilling. ▪ The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate). ▪ The mining dilution factors used. ▪ The mining recovery factors used. ▪ Any minimum mining widths used. ▪ The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion. ▪ The infrastructure requirements of the selected mining methods.	▪ The Reserve Estimation by Geoinvest was conducted using actual costs provided by the operator CMSA, believed to be based on the mining operation costs and those of comparable operations. ▪ **The mining method selected for the conceptual assessment of Mineral Reserves was open pit mining**, with larger and deeper open pits than previously utilised to extract the oxide material. Strip ratios varied between mining areas, with Chabuca-Rebeca/Roxana sectors with a strip ratio of 4.98 and for the Nicolasa sector a ratio of 6. 70. ▪ **The economic estimates incorporate inferred mineral resources in addition to proven and probable reserves.** Inferred resources are considered too speculative geologically to have economic considerations applied to them that would enable them to be categorized as mineral reserves. ▪ **These estimates are therefore preliminary in nature and should be considered only as part of a conceptual scoping evaluation. Inferred resources are noted to be a significant part of the overall project resource base.** ▪ **Assumptions related to the estimation are summarised below**. Mining dilution, minimum widths and recovery factors are to be clearly defined in future studies. ▪ The project has excellent infrastructure. Open pit mining would require establishment of waste and ore pile areas as part of future mining operations.

Criteria	JORC Code explanation	Commentary
Mining factors or assumptions **continued**	▪ The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design). ▪ The choice, nature and appropriateness of the selected mining method(s) and other mining parametres including associated design issues such as pre-strip, access, etc. ▪ The assumptions made regarding geotechnical parametres (eg pit slopes, stope sizes, etc), grade control and pre-production drilling. ▪ The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate). ▪ The mining dilution factors used. ▪ The mining recovery factors used. ▪ Any minimum mining widths used. ▪ The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion. ▪ The infrastructure requirements of the selected mining methods.	See table below

Economic Parametres	Value	Unit
CuT Recovery	72	%
Cu Price	4.3	US$/lb
Processing Cost	13	US$/ton
Crushing + HL + SX/EW	12.72	US$/ton
Administration Cost	0.28	US$/ton
Mining Cost	2.44	US$/ton
Drilling + Blasting + Loading + Services	2.08	US$/ton
Transportation	0.36	US$/ton
Product Sales Cost	0.06	US$/lb
Geotechnical Parametres		
Overall Slope Angle	52	°

Criteria	JORC Code explanation	Commentary
Metallurgical factors or assumptions	▪ The metallurgical process proposed and the appropriateness of that process to the style of mineralisation. ▪ Whether the metallurgical process is well-tested technology or novel in nature. ▪ The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied. ▪ Any assumptions or allowances made for deleterious elements. ▪ The existence of any bulk sample or pilot scale test work and the degree to which such samples are considered representative of the orebody as a whole. ▪ For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?	▪ The metallurgical process proposed for the processing of the oxide mineralisation is SX-EW processing, which is typical and appropriate for this style of oxide deposit in Chile. Other processing technology would be required to process the deeper sulphide material. ▪ The metallurgical process is well-tested and widely applied globally. ▪ The amount of historical metallurgical test work is unknown, but the project oxide material has been mined over a period of decades, which provides an excellent bulk sample and provides information on the differences within the deposit. ▪ Deleterious elements are not considered as a product of the SX-EW cathode copper output. This will need to be further considered for the sulphide mineralisation.
Environmental	▪ The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.	▪ The project is a permitted mining operation that uses sulphuric acid and SX-EW processing to produce copper. The mineralisation itself is oxide mineralisation and waste material between mineralised structures. ▪ Waste rock is accumulated in waste piles and mineralised material is accumulated on leach pads to which acid is added to liberate the soluble copper. Waste pads do not contain sulphide minerals and the environment is highly arid, with extremely sparse rainfall and extremely deep water table (below the depth of mining).
Infrastructure	▪ The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.	▪ The project is located approximately 50 km to the northeast of Antofagasta, a major mining support and services city on the coast in Northern Chile. The site has power supply (currently generator based), water and is well serviced by roads, with the workforce residing in Antofagasta and in accommodation on-site. ▪ The Antofagasta area includes several ports for the export of mineral products and import of industrial chemicals.

Criteria	JORC Code explanation	Commentary
Costs	▪ The derivation of, or assumptions made, regarding projected capital costs in the study. ▪ The methodology used to estimate operating costs. ▪ Allowances made for the content of deleterious elements. ▪ The derivation of assumptions made of metal or commodity price(s), for the principal minerals and co-products. ▪ The source of exchange rates used in the study. ▪ Derivation of transportation charges. ▪ The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc. ▪ The allowances made for royalties payable, both Government and private.	▪ The Reserve Estimate is preliminary and is not associated with a Pre-Feasibility or Feasibility study that has intensive cost analysis. ▪ The Reserve Estimate is based around costs from the current mining operations. ▪ No deleterious elements are considered, as the mineralisation is oxide in nature and SX-EW is used for extracting the copper. ▪ There are no private royalties. Government royalties are payable on production.
Revenue factors	▪ The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc. ▪ The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.	▪ Costs influencing revenue factors are presented in a table listed above in this table. ▪ Assumptions are based on long-term experience at this mining operation and similar mining operations.
Market assessment	▪ The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future. ▪ A customer and competitor analysis along with the identification of likely market windows for the product. ▪ Price and volume forecasts and the basis for these forecasts. ▪ For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.	▪ Copper is a standard commodity with a well developed and deep market, for which the long term demand forecasts show steady growth. Consequently it is considered a fairly predictable and low-risk commodity. ▪ The mine already has established clients for the mine offtake and copper cathode is a standard product, easily sold commercially. ▪ An average price was applied to the Mineral Reserve estimate.

Criteria	JORC Code explanation	Commentary
Economic	▪ The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc. ▪ NPV ranges and sensitivity to variations in the significant assumptions and inputs.	▪ The assessment resulted in estimated net profits of USD $488 million for the Chabuca-Rebeca/Roxana sectors and USD $201 million for Nicolasa based on the initial estimation of reserves.
Social	▪ The status of agreements with key stakeholders and matters leading to social licence to operate.	▪ The project is a well-established mining operation within 50 km of Antofagasta, in an area that has extensive mines and no other significant source of employment. Mining is the predominant source or income in the province.
Other	▪ To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves: ▫ Any identified material naturally occurring risks. ▫ The status of material legal agreements and marketing arrangements. ▫ The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.	▪ The project is a well-established mine, which holds permits for production and processing. Any permits for additional future operations should be obtainable as a matter of course, providing the appropriate documentation is applied.
Classification	▪ The basis for the classification of the Ore Reserves into varying confidence categories. ▪ Whether the result appropriately reflects the Competent Person's view of the deposit. ▪ The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).	▪ The classification of the Ore Reserves into the different confidence categories grouped reserves as Proven+Probable, without specifying each category in the Geoinvest report. This generalisation in the assessment of minable material is considered appropriate by the CP for this early stage assessment of the economics, without optimisation of pits and other considerations. Further evaluation will be undertaken as part of the full evaluation of all elements of the project by Cobre, incorporating the new drilling by Cobre.

Criteria	JORC Code explanation	Commentary
Audits or reviews	▪ The results of any audits or reviews of Ore Reserve estimates.	▪ The Reserve Estimate has been evaluated by the CP, but has not been fully audited. More detailed evaluation and auditing will be undertaken as part of Cobre's plan to bring the project to JORC compliance for the Resource and Reserve Estimates, with evaluation of historical data and collection of extensive new data by Cobre during drilling and validation activities.
Discussion of relative accuracy/confidence	▪ Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate. ▪ The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used. ▪ Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage. ▪ It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.	▪ The Reserve Estimate is considered to be for planning purposes but is not considered to be of a high level of accuracy and is not JORC 2012 compliant. The company will undertake evaluation of historical data and collection of new data, in order to deliver a JORC compliant resource and reserve. ▪ The Reserve Estimate was a global reserve estimate for the project, including the main mining areas.