ASX ANNOUNCEMENT

15th January 2026

RED DAM – HIGH GRADE GOLD DRILL RESULTS

Savannah Goldfields Limited ("Savannah" or "the Company") (ASX:SVG) is pleased to announce high grade gold assay results received for samples from the five Reverse Circulation holes (RC) recently drilled at the Red Dam Prospect, which is the northern most Prospect in the Company's Georgetown Gold Project.

HIGHLIGHTS

- Five RC holes for 648m were drilled at Red Dam in November 2025
- All five holes intersected significant gold mineralisation within the Red Dam structure
- Best assay result is **3m @ 14.86 g/t Au from 104m** in hole RD25DD1044
- Downhole intercepts and assay results for the five holes include:
    - RD25RC1043, 91m to 92m, **1m @ 8.88 g/t Au**
    - RD25RC1044, 103m to 106m, **3m @ 14.86 g/t Au**
    - RD25RC1045, 106m to 108m, **2m @ 3.59 g/t Au**
    - RD25RC1046, 104m to 106m, **2m @ 17.21 g/t Au**
    - RD25RC1047, 127m to 131m, **4m @ 8.70 g/t Au**
- These five (RC) holes successfully tested the down dip continuity of the Red Dam structure.
- The RC drilling programme was completed after Savannah drilled three diamond drill holes at Red Dam to obtain core for metallurgical test work and results from the diamond drilling programme were released to the ASX on the 18 December 2025 in an announcement titled "Georgetown Gold Project: Exploration Update"

Brad Sampson the CEO of Savannah commented, "*We are very encouraged by these results from Red Dam. The results indicate that the Red Dam gold mineralisation extends at depth well beyond the current pit limits and validates the Inferred Mineral Resource model. We intend to update the Mineral Resource ahead of undertaking further exploration at Red Dam.*"

RED DAM

The Red Dam Prospect is located approximately 80 km north of the Company's Georgetown Gold Processing Plant (GGPP), Figure 1. The Prospect is contained within ML30203 with strike extension to the known gold mineralisation cropping out into the surrounding EPM (EPM 9158) and both tenements are held by Savannah.

The Red Dam gold Deposit lies along an east west shear approximately 500m north of the outcropping Lubrina Granite. Aerial magnetics suggest that the granite plunges north beneath the Red Dam lode. The lode occupies a narrow shear zone with alteration commonly extending into the enclosing rock types for some 5 to 10 m. The shear zone can be traced at surface for 2km with aerial magnetics suggesting a strike length of up to 20km (5km east of Red Dam and 16km to the west). The shear zone cuts across metasediments and a meta-dolerite with gold mineralisation best developed in the meta-dolerite. Minor gold mineralisation occurs within metasediments. The lode is considered to be typical of the Georgetown gold lodes with high sulphide content, particularly arsenopyrite and galena, and is therefore likely to be of Siluro -Devonian in age.

Shear hosted mineralisation at Red Dam in the regional East West structure is steeply dipping between 80 to 85 degrees to the south.

Exploration at Red Dam has been intermittently undertaken since CRAE first explored the prospect in the late 1980's and early 1990's. Since that time the property has been held by several explorers who have drilled approximately 180 drill holes (RC, Percussion, Diamond) at the prospect comprising in excess of 9,000m of drilling.

Deutsche Rohstoff Australia Pty Ltd (DRAU) mined a small open pit at Red Dam to exploit the oxide resource in 2010. They mined a total of 22,600t of oxide ore at a grade of 13.6 g/t Au. The ore was mined from an open pit which is approximately 200m long and 15m deep.

The Red Dam Inferred Mineral Resource is 201,000t @ 5.7 g/t Au containing 37,000 oz Au. Details of this Mineral Resource are included in two announcements to the ASX dated 10 October 2025 titled "Mineral Resource Update for Jubilee Plunger Deposit" and of 7 February 2022 titled "Georgetown Project Mineral Resources". Details of the Red Dam Mineral Resource as part of the larger Georgetown Mineral Resource are included as Appendix 1.

RED DAM EXPLORATION DRILLING UPDATE

Five Reverse Circulation (RC) drill holes for 648m were drilled at Red Dam in November 2025. The RC holes were drilled to test the down dip extension of the gold mineralised zone which is hosted in an east – west shear zone, beneath the Red Dam historic open pit. All of the five holes intersected gold sulphide mineralisation down dip of the previously drilled extent of the mineralisation confirming the continuity of the gold mineralisation to a vertical depth of over 100m metres. The gold mineralisation at Red Dam remains open down dip and along strike.

Whilst the gold mineralisation is hosted within a very narrow shear zone, which has a width of between 1.3 to 3.0m, the gold grade is considered to be high.

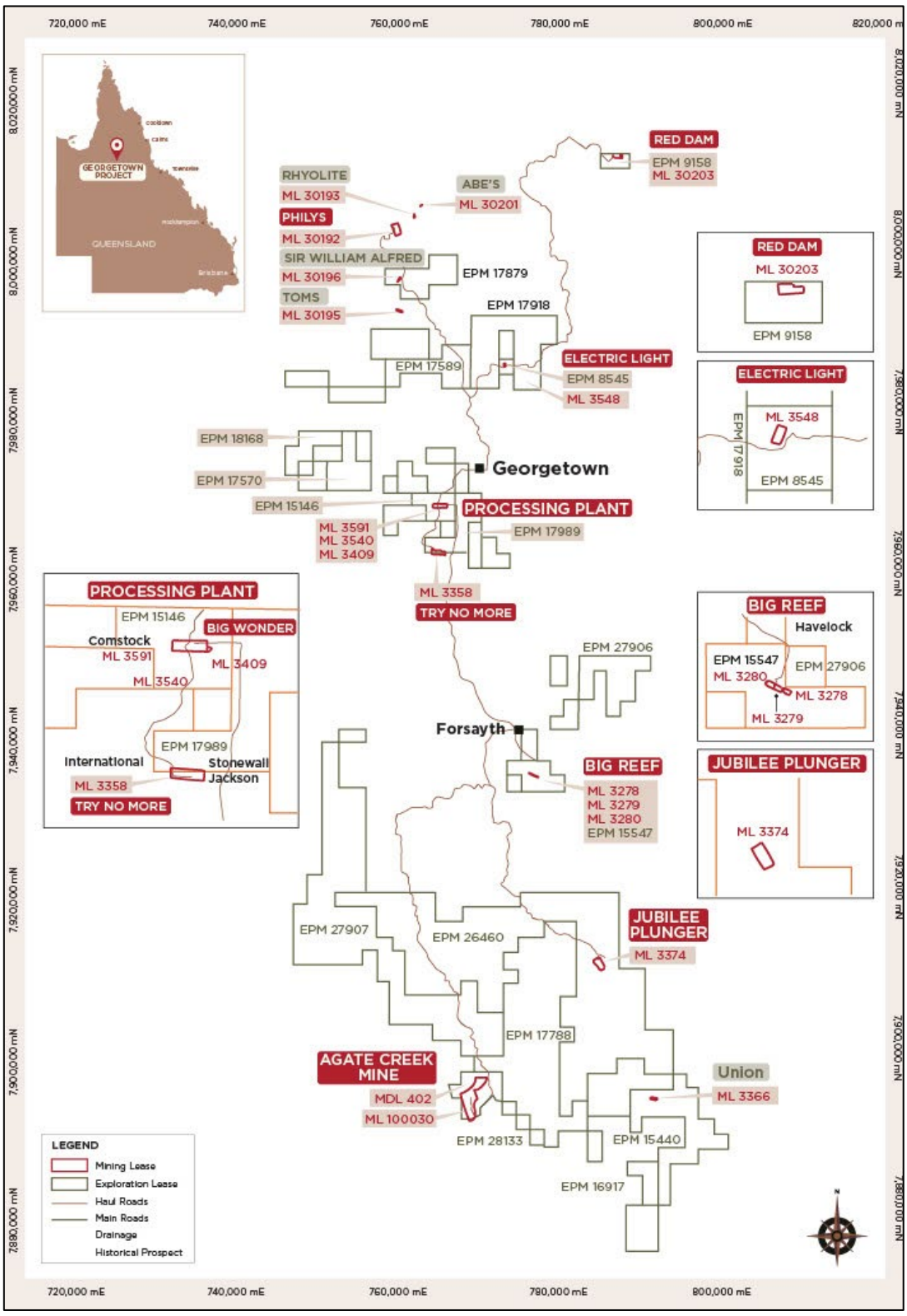

Figure 1: Red Dam Location Map

The RC drill hole parameters are presented in Table 1 and the location of the diamond and RC holes drilled by Savannah in November 2025 as well as all the historical drill hole locations are presented in Figure 2.

Table 1: Red Dam Drill Hole Parameters

Hole_ID	GDA_E	GDA_N	RL	Drilling Type	Dip	GDA94 Azimuth	Final Depth (m)	Sample Recovery (%)
RD25RC1043	786,140	8,014,988	315	RC	-60	001	120	98.37
RD25RC1044	786,186	8,014,980	311	RC	-60	002	120	99.25
RD25RC1045	786,251	8,014,992	305	RC	-60	355	130	99.31
RD25RC1046	786,298	8,014,994	303	RC	-60	357	138	99.49
RD25RC1047	786,349	8,015,002	298	RC	-60	004	140	99.32

ASSAY RESULTS

Assay results have been received for all five of the RC holes. All five holes intersected gold mineralisation associated with sulphides which comprise predominantly arsenopyrite, with minor galena and sphalerite. The best gold intercept was in hole RD25DD1044 which intersected 3m @ 14.83 g/t Au (true thickness 1.93m). Sampling of the RC holes was restricted to the mineralised zone and to the areas immediately adjacent to the mineralisation which exhibited alteration or contained trace sulphides. The dominant hanging wall and footwall lithologies are unmineralized schists, gneisses, meta dolerites or granite.

The mineralisation at Red Dam is associated with a regional east – west shear zone which dips steeply (between 80 to 90 degrees) to the south. The mineralisation is characterised by strong fracturing and moderate quartz – sericite alteration associated with sulphides, which are predominantly in the form of arsenopyrite and galena.

A summary of the assay results is included in Table 2 and a complete list of gold assay results and what are considered to be significant elements for metallurgical purposes for the individual sample intervals are included in Appendix 2.

Geological sections for Red Dam with historical holes and Holes RD25DD1040, RD25RC1044 and 1047 are presented in Figures 3 and 4 and a long section of the Red Dam prospect showing the location of both the historical holes and the RC holes drilled by Savannah is included as Figure 5.

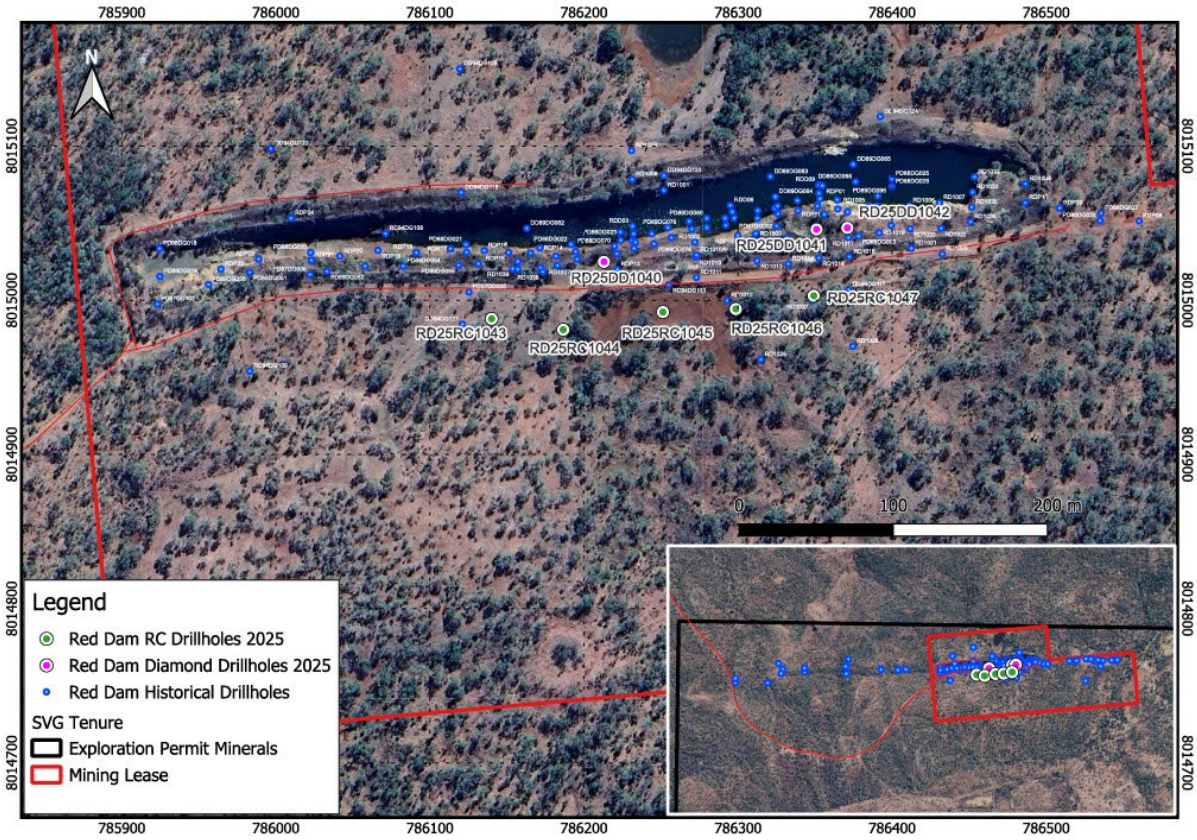

Figure 2: Red Dam Drill Hole Locations

Table 2: Assay Results for RD25RC1043 to RD25RC1047

Hole No.	From (m)	To (m)	Width (m)	True Width (m)	Au g/t	Ag g/t	As (%)	Cu (ppm)	Fe (%)	Pb (%)	S (%)	Zn (%)
RD25RC1043	91	92	1.0	0.64	8.21	2.13	5.26	56	8.57	0.03	5.73	0.02
RD25RC1044	103	106	3.0	1.93	14.83	8.93	5.84	631	9.54	0.11	6.86	0.16
RD25RC1045	99	100	1.0	0.64	1.15	4.3	'_	26	3.84	'_	LD	0.005
and	106	108	2.0	1.28	3.59	2.12	2.18	102	4.45	0.03	2.84	0.04
RD25RC1046	104	106	2.0	1.28	17.23	4.60	6.98	0.03	14.62	0.03	10.47	0.03
RD25RC1047	127	131	4.0	2.57	8.70	3.73	3.93	0.02	7.45	0.04	6.0	0.05

Intercepts calculated using a 1.0 g/t Au COG, with no internal dilution, no top cut has been applied. Barren metasediments / gneiss, amphibolite and granite intersected above and below the mineralised zone were not assayed.

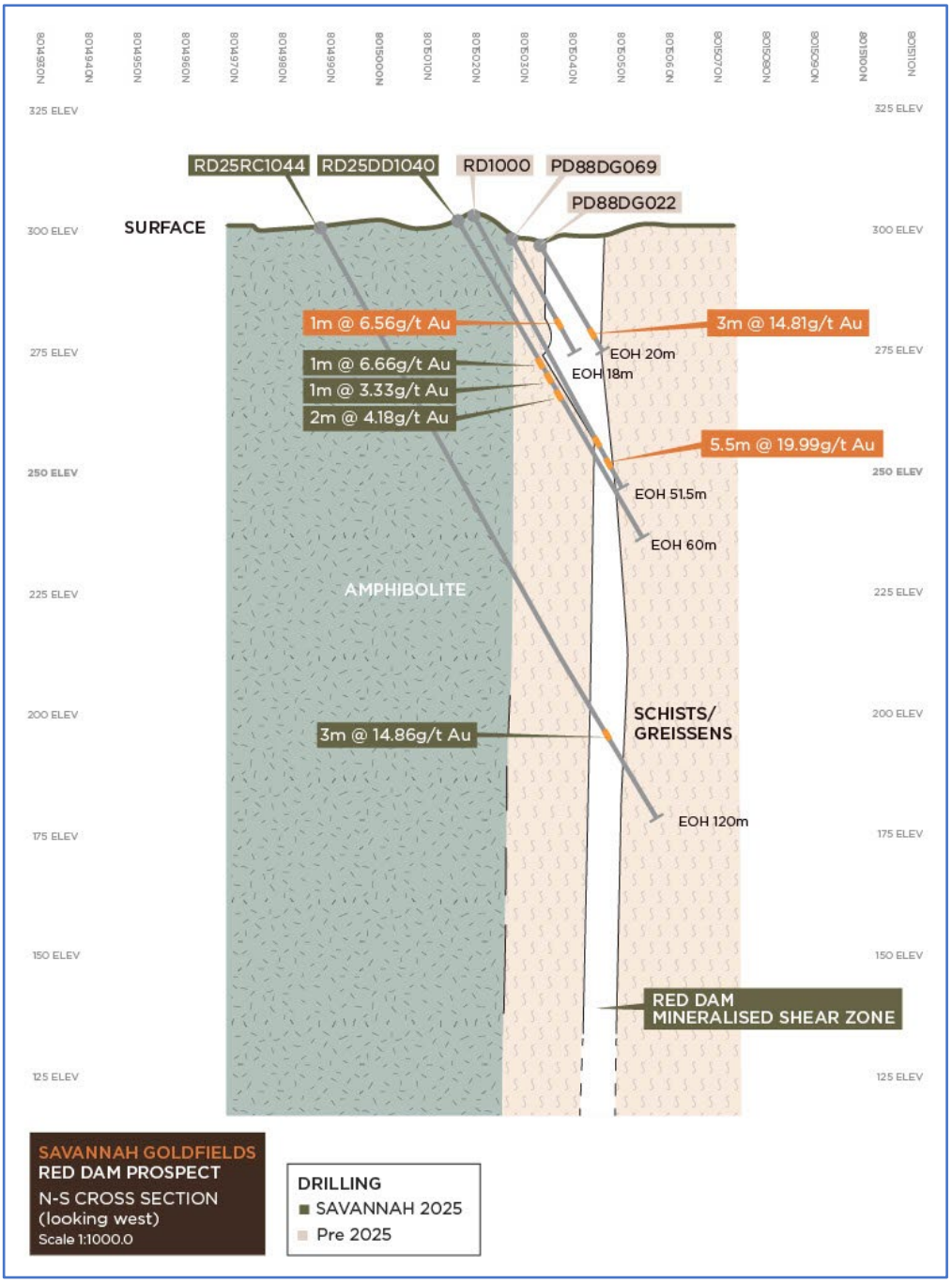

Figure 3: Idealised cross section with SVG holes RD25DD1040 and RD25RC1044

HISTORICAL DRILLING DATA

The historical drill data for Red Dam has not been previously released to the ASX by earlier explorers, presumably because the data was not considered material by large companies like CRAE or the tenement holder was a private company who is not required to release drill hole results.

Savannah has included the drill hole parameters as well as the significant assay results for the historical drilling for completeness and to support the display of some of this data in the cross sections in Figures 3, 4 and 5.

Exploration drilling commenced at Red Dam in the late 1980's with CRAE undertaking the bulk of the drilling. Other explorers who drilled at Red Dam include GMT, Planex and DRAU. In total, 178 holes were drilled for approximately 9,000m

A review of the historical data highlights the narrowness of the Red Dam shear zone and underscores the very high-grade nature of the gold mineralisation at Red Dam

The drill hole parameters for all the historical holes and significant assay results are included as Appendix 3.

It should be noted that intercepts with high gold values in the top 15m of the hole were mined out by the DRAU open pit.

Significant historical high grade gold intercepts for holes beneath the DRAU open pit include:

- RD015, 49.6m to 53.10m, 3.5m (2.24m true width) @ 36.76 g/t Au
- RD018, 80.0m to 81.40m, 1.4m (0.90m true width) @ 20.62 g/t Au
- RDP12, 46.0m to 49.0m, 3.0m (1.92m true width) @ 18.73 g/t Au
- RD1000, 44.1m to 47.0m, 2.9m (1.86m true width) @ 26.14 g/t Au
- DD94DG123, 59.93m to 58.80m 1.87m (1.20m true width) @ 17.79 g/t Au

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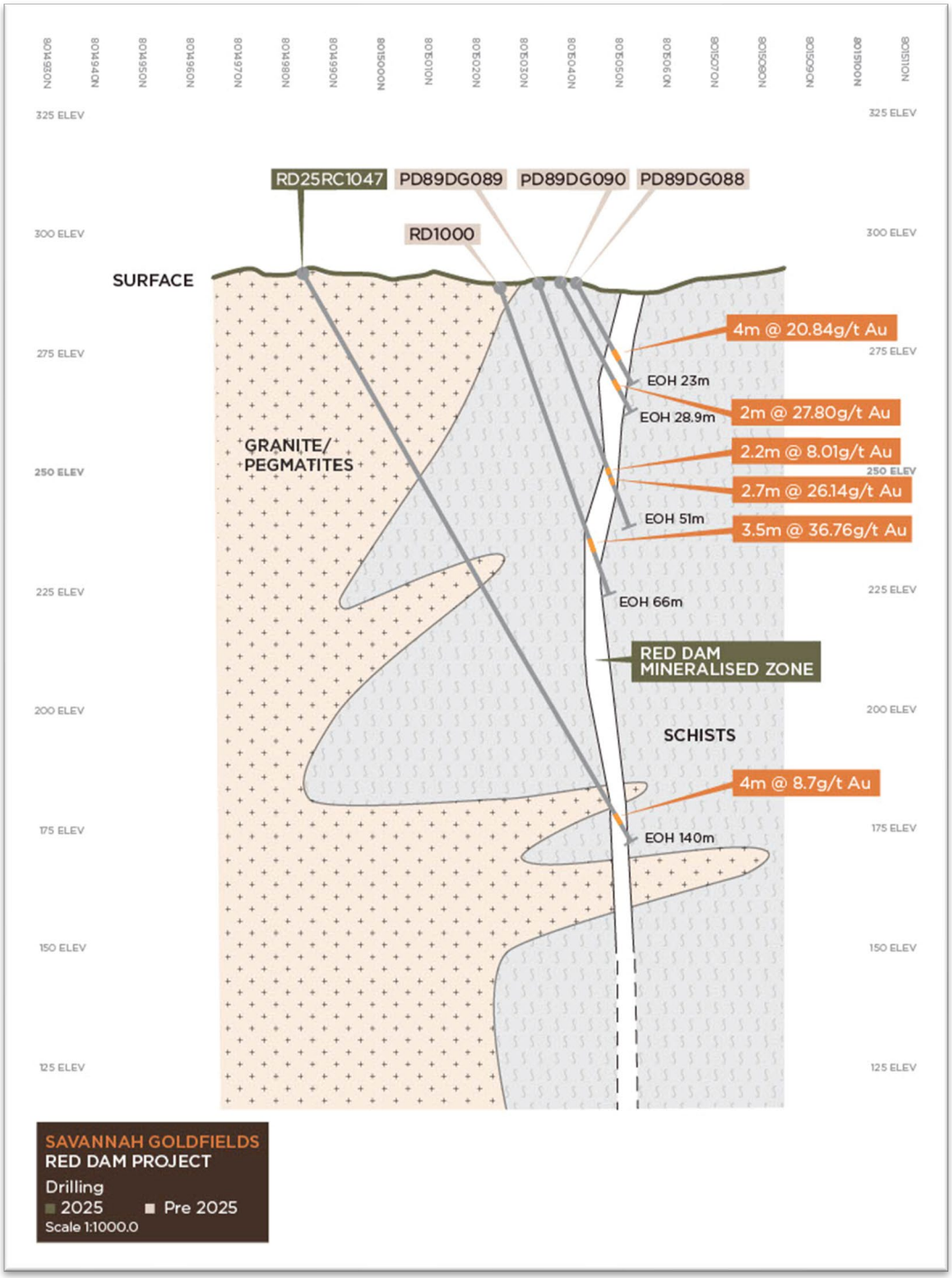

Figure 4: Red Dam – Idealised Cross Section with SVG hole RD25RC1047

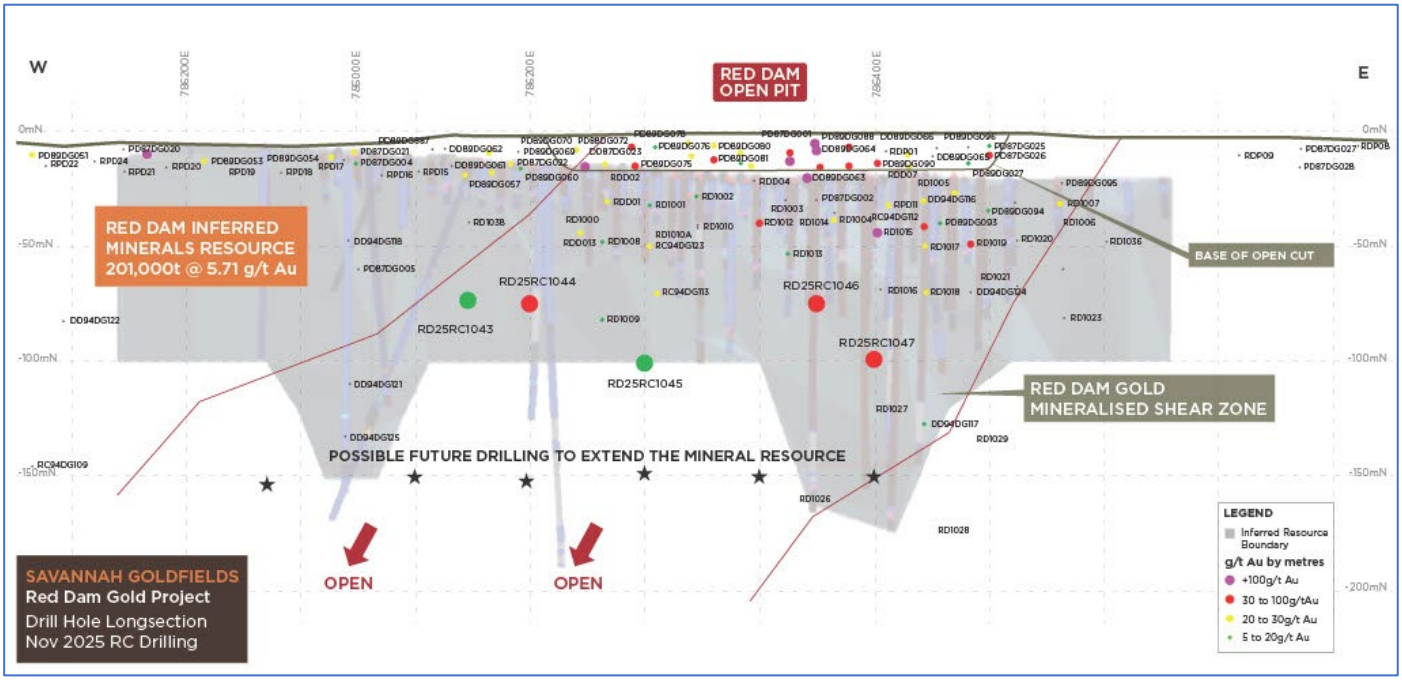

Figure 5: Idealised Long Section (West – East) through the Red Dam Prospect

This Report is Authorised by the Board of Directors

For further information, please contact:
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Competent Persons Statements

The information in this report that relates to Exploration Results compiled by Mr Patrick Smith, a Competent Person who is a Member of the Australian Institute of Mining and Metallurgy. Mr Smith is the owner and sole Director of PSGS Pty Ltd and is contracted to Savannah Goldfields Ltd as their Exploration Manager. Mr Smith confirms there is no potential for a conflict of interest in acting as the Competent Person. Mr Smith has sufficient experience that is relevant to the style of mineralisation and type of deposits under consideration and to the activity being undertaken to qualify as a Competent Person as defined in the 2012 Edition of the "Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves". Mr Smith consents to the inclusion of this information in the form and context in which it appears in this release.

The information relating to Mineral Resource at the Georgetown Gold Project is extracted from ASX Announcements of 10 October 2025 titled "Mineral Resource Update for Jubilee Plunger Deposit" and of 7 February 2022 titled "Georgetown Project Mineral Resources".

The reports are available to view on the Savannah Goldfields website www.savannahgoldfields.com. The reports were issued in accordance with the 2012 Edition of the JORC Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. The company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcements and, in the case of estimates of Mineral Resource or Ore Reserve that all material assumptions and technical parameters underpinning the estimates in the relevant market

Appendix 1

Georgetown Mineral Resource

Deposit	Tonnage	Gold Grade	Silver Grade	Density	Contained Gold	Tenement
	t	g/t	g/t	t/m^3	oz Au	
Red Dam	201,000	5.7	12	2.89	37,000	**ML30203** *EPM9158*
Electric Light	388,000	3.7	0.7	2.59	46,000	**ML3548** *EPM8545*
Jubilee Plunger Indicated	98,000	2.4	16	2.58	7,560	
Jubilee Plunger Inferred	198,000	2.0	17	2.58	12,440	**ML3374**
Jubilee Plunger Total	296,000	2.1	17	2,58	20,000	
Big Reef	107,000	3.0	-	2.44	10,000	**ML3278** **ML3279** **ML3280** *EPM15547*
Union	167,000	3.2	-	2.4	17,000	**ML3366**
Total Indicated	**98,000**	**2.4**	**16**	**2.58**	**7,560**	
Total Inferred	**1,052,000**	**3.6**	**-**	**-**	**122,440**	
Total Mineral Resource	**1,159,000**	**3.5**	**-**	**-**	**130,000**	

Mineral Resources reported at a cut of grade of 1.0 g/t Au.
Ounces rounded and reported to nearest 1,000 ounces
Ag assays for Big Reef and Union are limited and Ag cannot be estimated

Appendix 2: Red Dam Individual Assay Results – RD25RC1043 to RD25RC1047

Hole No.	Sample No.	From (m)	To (m)	Au ppm	Ag ppm	As ppm	Cu ppm	Fe %	Pb ppm	S %	Sb ppm	Zn ppm
RD25RC1043												
RD25RC1043	V54026	79	80	0.009	0.18	53	37	4.86	54.8	0.73	13.3	167
RD25RC1043	V54027	80	81	0.032	0.38	88.6	65.5	5.27	43.6	1.63	21.17	190
RD25RC1043	V54028	81	82	0.041	0.52	90.6	90.3	4.97	39.3	2.6	24.84	196
RD25RC1043	V54029	82	83	0.013	0.2	40.2	59.1	4.88	32.5	1.22	21.54	188
RD25RC1043	V54030	83	84	X	0.11	22.4	57.1	4.78	24.4	0.55	9.68	105
RD25RC1043	V54031	84	85	X	0.09	17.9	38	4.8	30.1	0.47	4.32	177
RD25RC1043	V54032	85	86	X	0.05	16.5	39.2	5.22	23.1	0.35	1.43	121
RD25RC1043	V54033	86	87	X	0.05	21.2	40.2	5.12	24.9	0.32	1.83	119
RD25RC1043	V54034	87	88	X	X	34.2	42.8	5.46	24.2	0.33	2.09	116
RD25RC1043	V54035	88	89	X	0.07	28.3	52.1	5.13	32.5	0.38	15.03	121
RD25RC1043	V54036	89	90	X	0.06	42	43.8	5.03	27	0.35	37.77	119
RD25RC1043	V54037	90	91	0.179	1.73	1124.7	81.6	4.22	551.2	0.58	54.94	320
RD25RC1043	V54038	91	92	8.215	2.13	52564	55.8	8.57	303.1	5.73	110.29	207
RD25RC1043	V54039	92	93	0.44	0.33	2526.9	36.7	4.97	81.5	0.87	23.43	231
RD25RC1043	V54040	93	94	0.076	0.06	380.5	29.1	4.65	25.4	0.18	24.12	99
RD25RC1043	V54041	94	95	0.026	0.07	141.3	36.8	5.22	24.9	0.18	63.24	104
RD25RC1043	V54042	95	96	0.018	X	104.3	31.6	5.07	24.5	0.21	16.07	104
RD25RC1043	V54043	96	97	0.035	0.06	222.8	23.3	3.82	32.4	0.23	19.96	131
RD25RC1043	V54044	97	98	0.03	0.19	162.5	34.1	3.84	70.4	0.37	7.41	167
RD25RC1043	V54045	98	99	0.043	0.11	298.7	45	4.3	38.3	0.26	4.13	112
RD25RC1043	V54046	99	100	0.008	0.05	65.7	39.6	4.36	22.9	0.2	1.62	102
RD25RC1043	V54047	100	101	0.039	0.1	272.3	21.9	4.89	38.3	0.18	2.42	120
RD25RC1043	V54048	101	102	0.007	0.05	49.8	26.4	4.84	27.2	0.26	1.42	100
RD25RC1043	V54049	102	103	0.024	0.07	145.8	45.7	4.85	22	0.25	1.24	131
RD25RC1043	V54050	103	104	0.007	0.06	66	39.2	5.03	25.6	0.21	1.13	119
RD25RC1044												
RD25RC1044	V54162	91	92	0.015	0.06	99.1	40.4	4.71	24.2	0.21	0.76	110
RD25RC1044	V54163	92	93	0.007	X	3.9	16.2	2.13	11.1	0.1	0.33	55
RD25RC1044	V54164	93	94	X	X	11.3	18.2	2.86	23.6	0.13	0.36	48
RD25RC1044	V54165	94	95	X	0.06	69.2	34.2	4.26	23.7	0.18	1.95	70
RD25RC1044	V54166	95	96	X	X	15.8	20.2	4.56	23	0.09	0.39	81
RD25RC1044	V54167	96	97	X	X	14.4	34.9	4.87	23.1	0.16	0.56	143
RD25RC1044	V54168	97	98	X	0.06	9.8	38.8	4.95	24.2	0.2	0.95	106
RD25RC1044	V54169	98	99	X	0.15	26.4	53.6	4.75	33.2	0.45	4.92	118
RD25RC1044	V54170	99	100	0.015	0.42	122	23.1	3.68	160.6	0.45	6.7	189
RD25RC1044	V54171	100	101	0.054	0.9	374.5	40.9	4.2	367.6	0.88	12.97	444
RD25RC1044	V54172	101	102	0.023	0.54	85.6	27.2	4.46	245.3	0.63	20.2	314
RD25RC1044	V54173	102	103	0.022	0.22	120.7	9.3	4.29	97.2	0.5	23.03	219
RD25RC1044	V54174	103	104	12.554	8.81	80724	290.3	13.13	471.9	10.75	323.17	456

RD25RC1044	V54175	104	105	24.423	13.27	66945	1231.3	8.98	2385.5	6.76	1230.7	3520
RD25RC1044	V54176	105	106	7.529	4.72	27447	370.2	6.51	593.2	3.08	326.92	948
RD25RC1044	V54177	106	107	0.959	3.89	4698.6	110.2	5.02	761.4	1.3	104.22	1756
RD25RC1044	V54178	107	108	0.273	1.98	1614.1	52.7	4.73	530.9	0.99	48.51	910
RD25RC1044	V54179	108	109	0.577	0.7	2456.2	88	5.96	140.8	1.26	73.8	390
RD25RC1044	V54180	109	110	0.131	0.89	674.9	97.9	6.2	228.2	0.75	68.7	502
RD25RC1044	V54181	110	111	0.071	0.13	296.1	31	5.22	46.9	0.23	19.55	150
RD25RC1044	V54182	111	112	0.085	0.13	507.7	21.4	5.15	37.4	0.19	9.52	140
RD25RC1044	V54183	112	113	0.04	0.09	157.3	37.8	5.2	28.5	0.27	7.67	132
RD25RC1044	V54184	113	114	0.015	X	73.3	25.3	4.99	28.9	0.11	1.59	106
RD25RC1044	V54185	114	115	0.551	0.25	2518.7	43.1	5.93	58.4	0.4	14.75	151
RD25RC1045												
RD25RC1045	V54291	96	97	X	0.07	34.1	24.6	3.32	47.5	0.1	0.91	118
RD25RC1045	V54292	97	98	0.031	0.09	210	7.7	4.74	28.9	0.46	3	123
RD25RC1045	V54293	98	99	X	0.08	20.9	15.3	2.28	30.4	0.3	2.47	72
RD25RC1045	V54294	99	100	1.148	4.3	X	26.4	3.84	6	X	0.86	53
RD25RC1045	V54295	100	101	0.013	0.12	20.2	23.3	1.15	36.4	0.26	2.52	58
RD25RC1045	V54296	101	102	X	0.12	7.6	14.7	0.86	43.1	0.18	2.49	42
RD25RC1045	V54297	102	103	0.009	0.1	9.8	8.9	1	30.5	0.23	1.94	51
RD25RC1045	V54298	103	104	0.016	0.16	7.2	12	0.72	63.1	0.28	4.78	29
RD25RC1045	V54299	104	105	0.009	0.13	20	36.2	0.91	40.9	0.31	11.64	38
RD25RC1045	V54300	105	106	X	0.09	19	56.6	1.05	37.5	0.3	7.26	19
RD25RC1045	V54301	106	107	5.299	2.76	30812	114.3	5.16	335.6	3.81	132.82	310
RD25RC1045	V54302	107	108	1.886	1.4	12814	33.1	2.69	278.8	1.57	43.67	529
RD25RC1045	V54303	108	109	0.099	0.16	543.2	7.2	4.45	53	0.25	15.64	170
RD25RC1045	V54304	109	110	0.059	0.59	277	41.2	2.61	167.5	0.62	56.49	288
RD25RC1045	V54305	110	111	0.027	0.18	173.8	83.1	2.42	19.5	0.33	40.81	92
RD25RC1045	V54306	111	112	0.048	0.12	200.3	52	2.87	28.7	0.32	31.78	132
RD25RC1045	V54307	112	113	0.021	0.06	89.8	18.1	1.99	22	0.14	6.6	84
RD25RC1045	V54308	113	114	0.008	0.09	91.7	17.1	1.89	35.5	0.15	5.33	85
RD25RC1045	V54309	114	115	0.015	0.07	296.3	28.3	2.87	26.6	0.32	9.57	407
RD25RC1045	V54310	115	116	0.009	1.55	167.9	35.8	4.4	457.8	0.6	13.76	511
RD25RC1045	V54311	116	117	X	0.13	41.9	16.9	5.05	44.7	0.34	9.8	160
RD25RC1046												
RD25RC1046	V57756	95	96	0.03	1.63	158.3	43.9	4.76	328.5	0.82	6.43	1253
RD25RC1046	V57757	96	97	X	0.06	8.6	6.4	1.62	36.2	0.07	1.9	79
RD25RC1046	V57758	97	98	0.006	0.57	11.2	5.8	0.89	162	0.21	2.39	165
RD25RC1046	V57759	98	99	0.009	2.27	25.6	14.5	0.85	722.6	0.41	5.03	976
RD25RC1046	V57760	99	100	0.009	0.12	8.7	12.8	0.7	55.6	0.06	1.48	38
RD25RC1046	V57761	100	101	0.008	0.08	34.1	15.1	3.9	26.6	0.24	5.67	111
RD25RC1046	V57762	101	102	0.037	0.39	358.2	25.3	4.02	152.9	0.36	9.31	202
RD25RC1046	V57763	102	103	0.006	X	63.9	33.4	4.93	28.5	0.16	12.5	151
RD25RC1046	V57764	103	104	0.048	0.28	300	35.2	4.82	60.1	0.92	22.2	252

RD25RC1046	V57765	104	105	24.292	5.1	97079	346.5	14.11	291.4	10.9	282.28	212
RD25RC1046	V57766	105	106	10.121	3.83	42257	210.4	10.31	215.2	9.13	188.13	145
RD25RC1046	V57767	106	107	0.869	0.84	3739.9	88.6	4.87	131.9	2.23	46.6	484
RD25RC1046	V57768	107	108	0.338	1.41	1613.6	75.7	5.16	225.4	2.66	33.98	646
RD25RC1046	V57769	108	109	0.675	1.29	3376.1	34.4	5.01	386.6	1.54	32.91	770
RD25RC1046	V57770	109	110	0.304	0.84	824.2	17.8	4.95	276.5	1.13	16.85	439
RD25RC1046	V57771	110	111	0.062	0.13	322.1	45.1	4.94	38.5	0.32	16.5	148
RD25RC1046	V57772	111	112	0.129	0.22	769.7	30.6	4.51	66.2	0.76	27.19	153
RD25RC1046	V57773	112	113	0.056	0.21	327.5	41.6	4.57	34	0.92	38.62	141
RD25RC1046	V57774	113	114	0.045	0.06	215	24.4	4.78	30	0.26	8.14	117
RD25RC1046	V57775	114	115	0.013	X	58.2	18.1	4.27	24.4	0.2	3.23	180
RD25RC1047												
RD25RC1046	V57801	99	100	0.024	0.11	37	11.6	0.71	49.6	0.06	1.57	26
RD25RC1046	V57802	104	105	22.358	5.38	>10000.0	447.9	12.53	225.2	9.32	277.74	251
RD25RC1047	V57908	105	106	0.006	X	44.7	9.9	4.58	19	0.06	2.9	87
RD25RC1047	V57909	106	107	0.027	0.15	220.1	19.7	2.99	28.9	0.5	8.76	81
RD25RC1047	V57910	107	108	0.067	0.33	286	23.1	1.25	59	0.39	3.79	88
RD25RC1047	V57911	108	109	0.013	0.34	25.8	28.5	1.28	51.8	0.31	1.96	85
RD25RC1047	V57912	109	110	0.012	0.24	83.8	73	9.03	22.4	0.45	5.65	185
RD25RC1047	V57913	110	111	0.005	0.25	15.8	152.3	11.35	9.6	0.25	3.3	161
RD25RC1047	V57914	111	112	0.007	0.2	13.9	112.9	11.69	7.1	0.08	1.47	161
RD25RC1047	V57915	112	113	X	0.26	11.3	138.1	11.84	6.7	0.07	1.12	159
RD25RC1047	V57922	119	120	0.057	0.26	182.6	40	2.15	47.7	0.38	11.88	79
RD25RC1047	V57923	120	121	0.006	X	9.5	6.6	1.57	28.8	0.06	3.61	36
RD25RC1047	V57924	121	122	X	0.11	16.4	9.2	1.04	41	0.12	7.22	15
RD25RC1047	V57925	122	123	0.012	0.12	35.8	6.3	0.81	44.8	0.13	6.28	23
RD25RC1047	V57926	123	124	0.028	0.2	55.1	14.5	1.14	62.7	0.23	17.84	33
RD25RC1047	V57927	124	125	0.135	0.7	479.4	38.9	1.28	120.7	0.32	44.66	60
RD25RC1047	V57928	125	126	0.017	0.33	65	7.6	1.01	63.7	0.27	7.51	30
RD25RC1047	V57929	126	127	0.012	0.17	27.1	8.7	1.15	44.4	0.21	5.14	50
RD25RC1047	V57930	127	128	1.245	1.68	3367.7	91.1	1.76	451	0.99	83.07	769
RD25RC1047	V57931	128	129	5.054	6.48	15602	344	6.3	487.5	5.59	275.63	395
RD25RC1047	V57932	129	130	22.917	4.49	116253	192.6	15.62	318.8	12.84	265.23	519
RD25RC1047	V57933	130	131	5.586	2.29	22242	48.3	6.14	223.1	4.59	68.31	297
RD25RC1047	V57934	131	132	0.309	0.17	1818.8	13.9	4.76	33	0.36	18.49	104
RD25RC1047	V57935	132	133	0.274	0.18	810	26.9	3.98	28.8	0.23	14.2	120
RD25RC1047	V57936	133	134	0.19	2.27	952.6	51.2	4.13	771.3	1.27	18.83	1624
RD25RC1047	V57937	134	135	0.25	1.53	1194.8	27.3	4.99	517.6	1.26	19.1	1164
RD25RC1047	V57938	135	136	0.021	0.18	127.4	12	2.92	44.7	0.66	8.62	115
RD25RC1047	V57939	136	137	0.015	0.1	50.4	38.1	2.41	29.3	0.17	4.16	68
RD25RC1047	V57940	137	138	0.028	0.13	112.2	23.3	1.16	43	0.25	3.51	26
RD25RC1047	V57941	138	139	0.086	0.14	507.9	17.7	1.27	55.3	0.14	4.22	79
RD25RC1047	V57942	139	140	0.062	0.68	207.5	28	0.89	167.7	0.19	3.8	186

Only the mineralised sections, and zones of alteration immediately adjacent to the mineralisation in each of the five RC holes were assayed. All the gold assays for each sample interval are listed. Other elements considered by the Competent Person to be of significance are also included in this table.

Appendix 3: Red Dam, Historical Drill hole Parameters and Significant Assays

Historical Hole Parameters

CRAE Holes 1987 to 1994										
Hole_ID	Hole typr	Max_Depth	Orig_Grid_ID	NAT_East	NAT_North	NAT_RL	Company	Year Drilled	Orig_Azimuth	Dip
PD87DG001	PERC	50.00	MGA94_54	786,324	8,015,060	289	CRAE	1990	352	-60
PD87DG002	PERC	70.00	MGA94_54	786,325	8,015,048	289	CRAE	1990	352	-60
PD87DG003	PERC	42.00	MGA94_54	786,224	8,015,039	291	CRAE	1990	352	-60
PD87DG004	PERC	50.00	MGA94_54	786,124	8,015,031	295	CRAE	1990	352	-60
PD87DG005	PERC	84.00	MGA94_54	786,125	8,015,005	295	CRAE	1990	352	-60
PD87DG006	PERC	40.00	MGA94_54	786,022	8,015,017	299	CRAE	1990	352	-60
PD87DG007	PERC	120.00	MGA94_54	785,923	8,014,998	305	CRAE	1990	352	-60
PD87DG008	PERC	13.92	MGA94_54	786,450	8,015,044	289	CRAE	1990	281	-60
PD88DG010	PERC	44.00	MGA94_54	785,364	8,015,031	304	CRAE	1990	355	-60
PD88DG011	PERC	24.00	MGA94_54	785,368	8,014,994	301	CRAE	1990	355	-60
PD88DG012	PERC	30.00	MGA94_54	785,364	8,015,037	304	CRAE	1990	355	-60
PD88DG013	PERC	20.00	MGA94_54	785,573	8,015,024	302	CRAE	1990	350	-60
PD88DG014	PERC	30.00	MGA94_54	785,574	8,015,018	302	CRAE	1990	350	-60
PD88DG015	PERC	20.00	MGA94_54	785,673	8,015,021	301	CRAE	1990	352	-60
PD88DG016	PERC	30.00	MGA94_54	785,673	8,015,016	301	CRAE	1990	352	-60
PD88DG017	PERC	20.00	MGA94_54	785,721	8,015,020	301	CRAE	1990	352	-60
PD88DG018	PERC	26.00	MGA94_54	785,924	8,015,034	304	CRAE	1990	355	-60
PD88DG019	PERC	38.00	MGA94_54	785,925	8,015,015	304	CRAE	1990	355	-60
PD88DG020	PERC	20.00	MGA94_54	786,023	8,015,031	299	CRAE	1990	352	-60
PD88DG021	PERC	20.00	MGA94_54	786,123	8,015,036	295	CRAE	1990	352	-60
PD88DG022	PERC	20.00	MGA94_54	786,192	8,015,036	292	CRAE	1990	352	-60
PD88DG023	PERC	20.00	MGA94_54	786,224	8,015,044	291	CRAE	1990	352	-60
PD88DG024	PERC	50.00	MGA94_54	786,324	8,015,060	289	CRAE	1990	352	-60
PD88DG025	PERC	30.00	MGA94_54	786,400	8,015,079	289	CRAE	1990	352	-60
PD88DG026	PERC	30.00	MGA94_54	786,400	8,015,074	289	CRAE	1990	352	-60
PD88DG027	PERC	20.00	MGA94_54	786,536	8,015,057	288	CRAE	1990	5	-60
PD88DG028	PERC	30.00	MGA94_54	786,535	8,015,052	288	CRAE	1990	5	-60
PD88DG029	PERC	20.00	MGA94_54	786,689	8,015,071	286	CRAE	1990	7	-60
PD88DG030	PERC	20.00	MGA94_54	786,732	8,015,076	283	CRAE	1990	18	-60
PD88DG031	PERC	28.00	MGA94_54	786,730	8,015,071	283	CRAE	1990	18	-60
PD88DG032	PERC	20.00	MGA94_54	786,835	8,015,077	282	CRAE	1990	352	-60
PD88DG033	PERC	30.00	MGA94_54	786,835	8,015,072	282	CRAE	1990	352	-60
PD88DG034	PERC	21.00	MGA94_54	786,961	8,015,078	283	CRAE	1990	352	-60
PD88DG035	PERC	29.00	MGA94_54	786,961	8,015,073	283	CRAE	1990	352	-60

PD89DG050	PERC	18.00	MGA94_54	785,956	8,015,010	300	CRAE	1990	348	-60
PD89DG051	PERC	20.00	MGA94_54	785,983	8,015,018	299	CRAE	1990	352	-60
PD89DG052	PERC	24.00	MGA94_54	786,033	8,015,019	296	CRAE	1990	350	-60
PD89DG053	PERC	24.00	MGA94_54	786,058	8,015,022	296	CRAE	1990	350	-60
PD89DG054	PERC	24.00	MGA94_54	786,083	8,015,022	294	CRAE	1990	350	-60
PD89DG055	PERC	24.00	MGA94_54	786,119	8,015,023	293	CRAE	1990	350	-60
PD89DG056	PERC	20.00	MGA94_54	786,131	8,015,024	293	CRAE	1990	350	-60
PD89DG057	PERC	30.00	MGA94_54	786,172	8,015,021	291	CRAE	1990	352	-60
PD89DG058	PERC	18.00	MGA94_54	786,182	8,015,029	291	CRAE	1990	343	-60
PD89DG059	PERC	28.00	MGA94_54	786,183	8,015,023	291	CRAE	1990	343	-60
DD89DG061	DDH	24.80	MGA94_54	786,165	8,015,031	294	CRAE	1990	351	-55
DD89DG062	DDH	25.00	MGA94_54	786,163	8,015,047	294	CRAE	1990	170	-55
DD89DG063	DDH	32.30	MGA94_54	786,321	8,015,080	288	CRAE	1990	169	-55
DD89DG064	DDH	25.00	MGA94_54	786,324	8,015,067	289	CRAE	1990	350	-55
DD89DG065	DDH	24.20	MGA94_54	786,375	8,015,088	289	CRAE	1990	168	-55
DD89DG066	DDH	19.70	MGA94_54	786,376	8,015,077	290	CRAE	1990	349	-55
PD89DG067	PERC	26.50	MGA94_54	786,157	8,015,025	292	CRAE	1990	350	-60
PD89DG068	PERC	23.00	MGA94_54	786,157	8,015,020	292	CRAE	1990	350	-60
PD89DG069	PERC	18.00	MGA94_54	786,195	8,015,032	290	CRAE	1990	340	-60
PD89DG070	PERC	26.00	MGA94_54	786,220	8,015,035	289	CRAE	1990	338	-60
PD89DG071	PERC	27.00	MGA94_54	786,221	8,015,030	289	CRAE	1990	338	-60
PD89DG072	PERC	27.00	MGA94_54	786,231	8,015,039	289	CRAE	1990	340	-60
PD89DG073	PERC	24.00	MGA94_54	786,233	8,015,034	288	CRAE	1990	338	-60
PD89DG074	PERC	18.00	MGA94_54	786,244	8,015,043	287	CRAE	1990	339	-60
PD89DG075	PERC	24.00	MGA94_54	786,246	8,015,037	287	CRAE	1990	339	-60
PD89DG076	PERC	18.00	MGA94_54	786,255	8,015,047	286	CRAE	1990	338	-60
PD89DG077	PERC	20.50	MGA94_54	786,257	8,015,041	286	CRAE	1990	338	-60
PD89DG078	PERC	14.00	MGA94_54	786,268	8,015,051	285	CRAE	1990	338	-60
PD89DG079	PERC	19.00	MGA94_54	786,270	8,015,046	286	CRAE	1990	338	-60
PD89DG080	PERC	15.00	MGA94_54	786,280	8,015,053	286	CRAE	1990	342	-60
PD89DG081	PERC	23.00	MGA94_54	786,280	8,015,047	287	CRAE	1990	342	-60
PD89DG082	PERC	21.00	MGA94_54	786,292	8,015,053	288	CRAE	1990	345	-60
PD89DG083	PERC	24.00	MGA94_54	786,292	8,015,049	288	CRAE	1990	345	-60
PD89DG084	PERC	18.00	MGA94_54	786,313	8,015,058	287	CRAE	1990	350	-60
PD89DG085	PERC	24.00	MGA94_54	786,313	8,015,053	288	CRAE	1990	350	-60
PD89DG086	PERC	18.00	MGA94_54	786,326	8,015,061	287	CRAE	1990	350	-60
PD89DG087	PERC	24.00	MGA94_54	786,326	8,015,056	287	CRAE	1990	350	-60
PD89DG088	PERC	18.00	MGA94_54	786,339	8,015,065	288	CRAE	1990	350	-60
PD89DG089	PERC	24.00	MGA94_54	786,339	8,015,058	288	CRAE	1990	350	-60
PD89DG090	PERC	24.00	MGA94_54	786,351	8,015,061	288	CRAE	1990	350	-60
PD89DG091	PERC	18.00	MGA94_54	786,364	8,015,065	288	CRAE	1990	350	-60
PD89DG092	PERC	24.00	MGA94_54	786,365	8,015,059	289	CRAE	1990	350	-60
PD89DG093	PERC	72.00	MGA94_54	786,378	8,015,042	289	CRAE	1990	350	-60

PD89DG094	PERC	48.00	MGA94_54	786,399	8,015,049	289	CRAE	1990	350	-60
PD89DG095	PERC	34.00	MGA94_54	786,431	8,015,055	288	CRAE	1990	0	-60
PD89DG096	PERC	17.00	MGA94_54	786,391	8,015,068	287	CRAE	1990	350	-60
PD89DG097	PERC	24.00	MGA94_54	786,391	8,015,061	288	CRAE	1990	350	-60
RC92DG101	RC	80.00	MGA94_54	785,381	8,015,080	301	CRAE	1990	172	-60
RC92DG102	RC	60.00	MGA94_54	785,121	8,015,006	301	CRAE	1990	358	-60
RC92DG103	RC	50.00	MGA94_54	785,121	8,015,028	301	CRAE	1990	178	-60
RC92DG104	RC	80.00	MGA94_54	784,712	8,014,941	301	CRAE	1990	178	-60
RC92DG105	RC	40.00	MGA94_54	784,711	8,014,966	301	CRAE	1990	178	-60
RC93DG106	RC	30.00	MGA94_54	773,700	8,009,960	300	CRAE	1990	172	-55
RC93DG107	RC	40.00	MGA94_54	773,700	8,009,991	300	CRAE	1990	172	-55
RC94DG108	RC	201.00	MGA94_54	786,071	8,015,043	297	CRAE	1990	262	-60
RC94DG109	RC	189.00	MGA94_54	785,983	8,014,954	300	CRAE	1990	352	-59
RC94DG110	RC	201.00	MGA94_54	786,873	8,015,039	284	CRAE	1990	262	-60
RC94DG111	RC	201.00	MGA94_54	786,784	8,014,953	301	CRAE	1990	352	-60
RC94DG112	RC	88.00	MGA94_54	786,371	8,015,047	290	CRAE	1990	352	-60
RC94DG113	RC	98.00	MGA94_54	786,255	8,015,010	289	CRAE	1990	352	-60
RC94DG114	RC	197.00	MGA94_54	784,991	8,015,020	301	CRAE	1990	262	-60
RC94DG115	RC	192.00	MGA94_54	784,902	8,014,941	301	CRAE	1990	352	-60
DD94DG116	DDH	80.00	MGA94_54	786,371	8,015,057	290	CRAE	1990	352	-60
DD94DG117	DDH	168.00	MGA94_54	786,372	8,015,007	292	CRAE	1990	352	-60
DD94DG118	DDH	90.10	MGA94_54	786,120	8,015,070	295	CRAE	1990	172	-60
RC94DG119	RC	100.00	MGA94_54	784,967	8,015,055	301	CRAE	1990	0	-90
RC94DG120	RC	46.00	MGA94_54	784,982	8,014,996	301	CRAE	1990	0	-90
DD94DG121	DDH	150.00	MGA94_54	786,121	8,014,984	295	CRAE	1990	352	-60
DD94DG122	DDH	141.10	MGA94_54	785,997	8,015,098	300	CRAE	1990	172	-60
DD94DG123	DDH	69.00	MGA94_54	786,252	8,015,081	290	CRAE	1990	172	-60
DD94DG124	DDH	108.00	MGA94_54	786,392	8,015,119	285	CRAE	1990	172	-60
DD94DG125	DDH	216.00	MGA94_54	786,119	8,015,150	293	CRAE	1990	172	-60
GML Holes 2006										
Hole_ID	Hole Type	Max_Depth	Orig_Grid_ID	NAT_East	NAT_North	NAT_RL	Company	YearDrilled	Orig_ Azimuth	Dip
RDD01	RC	47.00	MGA94_54	786,233	8,015,038	291	GML	2006	351	-70
RDD02	RC	26.00	MGA94_54	786,232	8,015,043	291	GML	2006	351	-70
RDD03	RC	20.00	MGA94_54	786,232	8,015,048	291	GML	2006	351	-70
RDD04	RC	32.00	MGA94_54	786,298	8,015,053	288	GML	2006	341	-70
RDD05	RC	21.50	MGA94_54	786,296	8,015,057	288	GML	2006	341	-70
RDD06	RC	16.00	MGA94_54	786,295	8,015,062	287	GML	2006	341	-70
RDD07	RC	29.00	MGA94_54	786,353	8,015,066	289	GML	2006	351	-70
RDD08	RC	23.00	MGA94_54	786,352	8,015,069	288	GML	2006	347	-70
RDD09	RC	20.00	MGA94_54	786,352	8,015,075	288	GML	2006	348	-70

Plantex Holes 2006										
Hole_ID	Hole_Type	Max_Depth	Orig_Grid_ID	NAT_East	NAT_North	NAT_RL	Company	YearDrilled	Orig_Azimuth	Dip
RDP01	RC	18.00	MGA94_54	786,355	8,015,074	289	Plantex	2006	345	-70
RDP02	RC	27.00	MGA94_54	786,972	8,015,076	282	Plantex	2006	3	-60
RDP03	RC	27.00	MGA94_54	786,938	8,015,074	283	Plantex	2006	359	-60
RDP04	RC	21.00	MGA94_54	786,885	8,015,073	285	Plantex	2006	4	-60
RDP05	RC	21.00	MGA94_54	786,858	8,015,075	283	Plantex	2006	6	-60
RDP06	RC	21.00	MGA94_54	786,815	8,015,080	281	Plantex	2006	36	-60
RDP07	RC	21.00	MGA94_54	786,786	8,015,082	281	Plantex	2006	9	-60
RDP08	RC	21.00	MGA94_54	786,560	8,015,052	289	Plantex	2006	16	-60
RDP09	RC	21.00	MGA94_54	786,509	8,015,060	288	Plantex	2006	7	-60
RDP10	RC	21.00	MGA94_54	786,486	8,015,063	288	Plantex	2006	357	-60
RDP11	RC	51.00	MGA94_54	786,356	8,015,056	289	Plantex	2006	351	-70
RDP12	RC	69.00	MGA94_54	786,300	8,015,042	289	Plantex	2006	341	-75
RDP13	RC	69.00	MGA94_54	786,222	8,015,020	291	Plantex	2006	353	-60
RDP14	RC	21.00	MGA94_54	786,171	8,015,034	294	Plantex	2006	1	-60
RDP15	RC	27.00	MGA94_54	786,151	8,015,031	295	Plantex	2006	8	-60
RDP16	RC	27.00	MGA94_54	786,135	8,015,032	295	Plantex	2006	7	-60
RDP17	RC	21.00	MGA94_54	786,113	8,015,033	295	Plantex	2006	11	-60
RDP18	RC	27.00	MGA94_54	786,091	8,015,031	296	Plantex	2006	357	-60
RDP19	RC	21.00	MGA94_54	786,066	8,015,032	297	Plantex	2006	8	-60
RDP20	RC	21.00	MGA94_54	786,042	8,015,029	298	Plantex	2006	6	-60
RDP21	RC	27.00	MGA94_54	786,023	8,015,026	299	Plantex	2006	4	-60
RDP22	RC	21.00	MGA94_54	785,989	8,015,027	301	Plantex	2006	10	-60
RDP23	RC	27.00	MGA94_54	785,964	8,015,020	302	Plantex	2006	14	-60
RDP24	RC	75.00	MGA94_54	786,010	8,015,053	300	Plantex	2006	271	-60
DRAU Holes 2010										
RD1000	RC	51.50	MGA94_54	786,213	8,015,024	291	DRAU	2010	358	-59.5
RD1001	RC	51.50	MGA94_54	786,252	8,015,071	290	DRAU	2010	182	-60
RD1002	RC	39.60	MGA94_54	786,272	8,015,038	287	DRAU	2010	359	-59.5
RD1003	RC	45.40	MGA94_54	786,312	8,015,043	289	DRAU	2010	360	-58
RD1004	RC	51.50	MGA94_54	786,332	8,015,041	290	DRAU	2010	360	-60
RD1005	RC	47.80	MGA94_54	786,385	8,015,061	290	DRAU	2010	360	-60
RD1006	RC	43.90	MGA94_54	786,411	8,015,061	290	DRAU	2010	360	-60.5
RD1007	RC	46.90	MGA94_54	786,431	8,015,063	290	DRAU	2010	358	-60.5
RD1008	RC	75.40	MGA94_54	786,231	8,015,078	291	DRAU	2010	180	-60
RD1009	RC	108.20	MGA94_54	786,231	8,015,097	291	DRAU	2010	180	-60
RD1010	RC	50.00	MGA94_54	786,273	8,015,028	288	DRAU	2010	0	-60
RD1010A	RC	60.40	MGA94_54	786,273	8,015,029	288	DRAU	2010	359	-60
RD1011	RC	81.30	MGA94_54	786,273	8,015,015	288	DRAU	2010	0	-60
RD1012	RC	100.00	MGA94_54	786,293	8,015,000	290	DRAU	2010	0	-60
RD1013	RC	72.40	MGA94_54	786,312	8,015,026	290	DRAU	2010	0	-60

RD1014	RC	76.40	MGA94_54	786,333	8,015,024	290	DRAU	2010	0	-60
RD1015	RC	66.00	MGA94_54	786,352	8,015,046	289	DRAU	2010	0	-70
RD1016	RC	90.40	MGA94_54	786,353	8,015,028	291	DRAU	2010	0	-70
RD1017	RC	95.00	MGA94_54	786,372	8,015,041	291	DRAU	2010	0	-60
RD1018	RC	93.40	MGA94_54	786,372	8,015,028	291	DRAU	2010	0	-60
RD1019	RC	65.50	MGA94_54	786,392	8,015,044	291	DRAU	2010	0	-60
RD1020	RC	78.40	MGA94_54	786,412	8,015,046	290	DRAU	2010	0	-60
RD1021	RC	89.50	MGA94_54	786,413	8,015,034	291	DRAU	2010	0	-60
RD1022	RC	78.40	MGA94_54	786,432	8,015,047	290	DRAU	2010	0	-60
RD1023	RC	99.40	MGA94_54	786,433	8,015,030	291	DRAU	2010	0	-60
RD1026	RC	201.40	MGA94_54	786,315	8,014,962	291	DRAU	2010	0	-52
RD1027	RC	164.00	MGA94_54	786,348	8,015,000	292	DRAU	2010	5	-69
RD1028	RC	213.50	MGA94_54	786,375	8,014,970	294	DRAU	2010	356	-54
RD1029	RC	165.30	MGA94_54	786,393	8,015,004	293	DRAU	2010	356	-59
RD1032	RC	25.00	MGA94_54	786,453	8,015,080	288	DRAU	2010	0	-60
RD1033	RC	40.00	MGA94_54	786,452	8,015,070	289	DRAU	2010	0	-60
RD1034	RC	30.00	MGA94_54	786,487	8,015,076	287	DRAU	2010	0	-60
RD1035	RC	50.00	MGA94_54	786,452	8,015,060	289	DRAU	2010	7	-57
RD1036	RC	70.00	MGA94_54	786,451	8,015,051	290	DRAU	2010	0	-60
RD1037	RC	50.00	MGA94_54	786,194	8,015,015	292	DRAU	2010	0	-60
RD1038	RC	50.00	MGA94_54	786,173	8,015,019	293	DRAU	2010	0	-60
RD1039	RC	55.00	MGA94_54	786,154	8,015,021	294	DRAU	2010	0	-60

RED DAM – Significant Historical Drilling Intercepts

All intercepts are calculated using a 1.0 g/t Au cut-off grade, with a minimum down hole width of 1.0m which equates to a true width of approximately 0.64m. No top cuts have been applied, and there is a maximum of 1m of internal dilution

CRAE Holes 1987 to 1994						
Hole No:	**From (m)**	**To (m)**	**Width (m)**	**True Width (m)**	**Au g/t**	**Ag g/t**
PD87DG001	4	10	6.00	3.84	38.90	90.67
and	16	30	14.00	8.96	1.07	3.42
and	34	36	2.00	1.28	3.76	4.00
and	40	46	6.00	3.84	1.85	3.00
PD87DG002	34	38	4.00	2.56	1.35	2.50
PD87DG003	10	20	10.00	6.40	3.17	6.80
PD87DG004	16	18	2.00	1.28	7.96	55.00
PD87DG005	NSR					
PD87DG006	NSR					
PD87DG007	NSR					
PD87DG008	NSR					
PD87DG009	NSR					
PD87DG010	NSR					
PD87DG011	5	7	2.00	1.28	2.05	7.50

PD87DG012	NSR					
PD87DG013	NSR					
PD87DG014	NSR					
PD87DG015	5	6	1.00	0.64	4.10	35.00
PD87DG016	15	16	1.00	0.64	5.63	20.00
PD87DG017	10	11	1.00	0.64	1.15	3.00
PD87DG018	NSR					
PD87DG019	NSR					
PD87DG020	9	11	2.00	1.28	3.16	19.50
PD87DG021	10	12	2.00	1.28	11.10	17.50
PD87DG022	15	18	3.00	1.92	14.81	41.67
PD87DG023	3	5	2.00	1.28	3.03	5.50
PD87DG023	10	12	2.00	1.28	2.37	5.00
PD87DG024	18	19	1.00	0.64	6.85	8.00
PD87DG025	7	8	1.00	0.64	10.20	12.00
PD87DG026	12	16	4.00	2.56	24.06	29.25
PD87DG027	NSR					
PD87DG028	18	19	1.00	0.64	1.12	6.00
PD87DG029	NSR					
PD87DG030	12	15	3.00	1.92	7.47	11.00
PD87DG031	22	25	3.00	1.92	3.21	12.30
PD87DG032	10	12	2.00	1.28	1.92	1.00
PD87DG033	23	24	1.00	0.64	4.81	73.00
PD87DG034	10	14	4.00	2.56	6.25	66.50
PD87DG035	NSR					
PD87DG036	NSR					
PD87DG037	NSR					
PD87DG038	NSR					
PD87DG039	NSR					
PD87DG040	NSR					
PD87DG041	NSR					
PD87DG042	NSR					
PD87DG043	NSR					
PD87DG044	NSR					
PD87DG045	NSR					
PD87DG046	NSR					
PD87DG047	NSR					
PD87DG048	NSR					
PD87DG049	NSR					
PD89DG050	8	9	1.00	0.64	6.52	17.00
PD89DG051	11	14	3.00	1.92	12.07	52.67
PD89DG052	11	17	6.00	3.84	29.81	73.50
PD89DG053	15	16	1.00	0.64	41.80	62.00

PD89DG054	NSR					
PD89DG055	NSR					
PD89DG056	12	13	1.00	0.64	2.77	45.00
PD89DG057	21	24	3.00	1.92	11.83	10.33
PD89DG058	10	13	3.00	1.92	14.58	14.33
PD89DG059	20	21	1.00	0.64	25.15	37.00
PD89DG060	17	19	2.00	1.28	10.37	16.00
DD89DG061	17.5	19.2			2.47	17.00
DD89DG062	7.2	7.9	0.70	0.45	2.02	0.00
DD89DG062	8.7	10	1.30	0.83	2.92	6.00
DD89DG063	22.75	29.45	6.70	4.29	54.73	80.25
DD89DG064	6.9	11.2	4.30	2.75	65.78	152.81
DD89DG065	12.4	13.2	0.80	0.51	9.00	27.00
DD89DG066	NSR					
PD89DG067	9	11	2.00	1.28	2.98	17.50
PD89DG068	22	23	1.00	0.64	6.82	11.00
PD89DG069	5	7	2.00	1.28	2.96	8.00
PD89DG069	10	11	1.00	0.64	6.56	22.00
PD89DG070	9	10	1.00	0.64	22.00	10.00
PD89DG071	18	19	2.00	1.28	14.58	7.50
PD89DG072	10	12	2.00	1.28	23.47	14.50
PD89DG073	14	15	1.00	0.64	3.38	18.00
PD89DG073	17	21	4.00	2.56	9.29	7.00
PD89DG074	7	10	3.00	1.92	21.68	3.66
PD89DG075	17	20	3.00	1.92	19.14	15.00
PD89DG076	8	10	2.00	1.28	7.23	2.00
PD89DG077	16	19	3.00	1.92	10.70	11.33
PD89DG078	5	9	4.00	2.56	13.19	23.75
PD89DG079	12	15	3.00	1.92	13.43	14.67
PD89DG079	17	18	1.00	0.64	2.18	0.00
PD89DG080	7	9	2.00	1.28	19.78	14.50
PD89DG081	14	17	3.00	1.92	20.13	23.00
PD89DG081	19	21	2.00	1.28	2.41	0.00
PD89DG082	11	13	2.00	1.28	25.72	36.00
PD89DG083	16	17	1.00	0.64	17.55	20.00
PD89DG084	9	13	4.00	2.56	20.27	24.50
PD89DG085	15	19	4.00	2.56	25.83	43.75
PD89DG086	NSR					
PD89DG087	18	21	3.00	1.92	33.32	39.67
PD89DG088	8	12	4.00	2.56	20.84	9.50
PD89DG089	17	19	2.00	1.28	38.04	89.50
PD89DG090	16	18	2.00	1.28	27.80	25.50
PD89DG091	11	13	2.00	1.28	13.31	3.00

PD89DG092	19	20	1.00	0.64	30.95	210.00
PD89DG093	46	48	1.00	0.64	5.52	0.00
PD89DG094	40	42	2.00	1.28	9.80	2.00
PD89DG095	NSR					
PD89DG096	8	9	1.00	0.64	2.50	7.00
PD89DG097	16	17	1.00	0.64	10.58	9.00
RC94DG101	NSR					
RC94DG102	NSR					
RC94DG103	33	36	3.00	1.92	3.35	7.00
RC94DG104	NSR					
RC94DG105	NSR					
RC94DG106	NSR					
RC94DG107	NSR					
RC94DG108#	114	120	6.00	3.84	2.23	4.00
RC94DG108#	138	153	15.00	9.60	14.37	13.36
RC94DG109	NSR					
RC94DG110	NSR					
RC94DG111	NSR					
RC94DG112	48	51	3.00	1.92	22.20	7.00
RC94DG112	54	88	34.00	21.76	1.63	0.25
RC94DG113	81	90	11.00	7.04	6.54	1.33
RC94DG114	99	102	3.00	1.92	3.20	4.00
RC94DG115	NSR					
DD94DG116	34.6	35.5	0.90	0.58	43.11	89.00
DD94DG117	146	150	4.00	2.56	4.23	2.50
DD94DG117	156	159	3.00	1.92	1.84	7.00
DD94DG118	NSR					
DD94DG119	NSR					
RC94DG120	NSR					
DD94DG121	NSR					
DD94DG122	120	122	2.00	1.28	1.45	4.50
DD94DG122	95.1	96.1	1.00	0.64	2.21	58.50
DD94DG123	56.93	58.8	1.87	1.20	17.79	9.91
DD94DG124	80.34	80.5	0.16	0.10	11.90	3.00
DD94DG125	NSR			0.00		
GML Holes 2006						
Hole No:	**From (m)**	**To (m)**	**Width (m)**	**True Width (m)**	**Au g/t**	**Ag g/t**
RDD01	24.05	25.5	1.45	0.93	12.20	47.30
RDD01	34.85	37.3	2.45	1.57	14.32	28.45
RDD02	7.45	11.85	4.40	2.82	2.11	4.85
RDD02	18.1	19.2	1.10	0.70	10.00	11.20
RDD03	NSR					

RDD04	25.1	25.8	0.70	0.45	5.11	4.50
RDD05	16.9	18.8	1.90	1.22	18.50	32.00
RDD06	NSR					
RDD07	NSR					
Plantex Holes 2006						
Hole No:	**From (m)**	**To (m)**	**Width (m)**	**True Width (m)**	**Au g/t**	**Ag g/t**
RDP01	NSR					
RDP02	13	16	3.00	1.92	3.24	34.67
RDP03	20	21	1.00	0.64	3.85	17.00
RDP04	NSR					
RDP05	10	13	3.00	1.92	1.93	14.67
RDP06	4	7	3.00	1.92	6.68	6.67
RDP07	NSR					4.00
RDP08	7	8	1.00	0.64	1.33	6.00
RDP09	12	13	1.00	0.64	4.44	17.00
RDP10	NSR					
RDP11	37	42	5.00	3.20	7.15	18.20
RDP12	46	49	3.00	1.92	18.73	6.00
RDP13	51	52	1.00	0.64	4.34	11.00
RDP13	57	63	6.00	3.84	4.42	6.33
RDP14	NSR					
RDP15	NSR					
RDP16	NSR					
RDP17	13	16	3.00	1.92	9.75	13.67
RDP18	20	22	2.00	1.28	2.93	19.50
RDP19	15	18	3.00	1.92	2.76	30.00
RDP20	18	19	1.00	0.64	2.01	17.00
RDP21	NSR					
RDP22	17	18	1.00	0.64	2.36	7.00
RDP23	16	17	1.00	0.64	2.37	17.00
RDP24	NSR					
DRAU Holes 2010						
Hole No:	**From (m)**	**To (m)**	**Width (m)**	**True Width (m)**	**Au g/t**	**Ag g/t**
RD1000	39.7	41.9	2.2	1.41	8.01	59.4
and	44.1	47	2.9	1.86	26.14	45.46
RD1001	37.1	39.5	2.4	1.54	7.46	5.7
RD1002	32.7	33.6	0.9	0.58	15.85	29.9
RD1003	34	34.9	0.9	0.58	8.45	14
RD1004	44.3	45	0.7	0.45	25.4	57.9
RD1005	30.6	31.7	1.1	0.70	39.4	9.5
RD1006	NSR					

RD1007	36.4	37.4	1	0.64	23.5	132
RD1008	55.4	58.1	2.7	1.73	7.28	6.8
RD1009	94.4	95.2	0.8	0.51	15.45	9
RD1010	47	50	3	1.92	1.81	9.83
RD1010A	46.7	48.9	2.2	1.41	9.65	4.39
RD1011	NSR					
RD1012	NSR					
RD1013	61.4	62.55	1.15	0.74	12.85	24
RD1014	41	41.7	0.7	0.45	4.63	1.4
RD1015	49.6	53.1	3.5	2.24	36.76	48.34
RD1016	NSR					
RD1017	56.2	56.6	0.4	0.26	3.05	7.4
and	58.1	59.45	1.35	0.86	32.2	12.5
RD1018	80	81.4	1.4	0.90	20.62	5.32
RD1019	56.6	60.7	4.1	2.62	15.75	3.52
RD1020	NSR					
RD1021	NSR					
RD1022	68.95	69.4	0.45	0.29	10.25	20.4
RD1023	NSR					
RD1024	NSR					
RD1025	NSR					
RD1026	185.3	186.4	1.1	0.70	32.5	18.6
RD1027	NSR					
RD1028	200.3	200.8	0.5	0.32	11.05	12.1
RD1029	154.54	155.25	0.71	0.45	2.38	44.8
RD1030	NSR					
RD1031	NSR					
RD1032	NSR					
RD1033	NSR					
RD1034	NSR					
RD1035	NSR					
RD1036	NSR					
RD1037	NSR					
RD1038	NSR					
RD1039	NSR					

The true widths have been estimated assuming the drill holes have intersected the mineralised structure perpendicular to strike, with the dominant dip of the structure being between -80 to -85 degrees, with the majority of the holes drilled at -60 degrees.

##One-hole RC94DG108 was drilled parallel to the mineralised structure at an azimuth of 268 by CRAE to test a geophysical target and the true widths is approximately 3m

The majority of the intercepts which intersected high grade zones in the top 20m have already been mined by DRAU.

Appendix 4: Red Dam JORC 2012 TABLE 1

Section 1 Sampling Techniques and Data

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.*	Soil sampling, surface rock chips and surface geophysical surveys were all undertaken at various stages of the exploration at Red Dam, this data has been superseded by drilling and hence are not considered. Sampling included surface **costeans and trenches** that were used for interpretation but not for used for Resource estimation. Being at surface many of these are now mined out and have minimal impact currently. **Red Dam** • CRAE in 1988 completed 56 costeans sampling as 1 m rock chip lines along the trench wall on roughly 50 m line spacing • GML in 2006 completed 35 costeans at roughly 25 m spacing • JKO in 2013 completed 22 trenches over Red Dam West • The data has been superseded by drilling data and is therefore not included in this announcement **SVG RC Drilling (2025)** • Five Reverse Circulation (RC) holes for 648m were drilled at Red Dam • The RC holes were sampled at 1m intervals using a cone splitter attached to the cyclone • No composite samples were submitted • Only the mineralised area of the hole and the alteration halo adjacent to the mineralisation was assayed. Historical data and data from the recently completed diamond drilling indicates that there is no gold mineralisation in the footwall and hanging wall lithologies • Individual RC samples were collected in numbered calico bags, and then placed in large poly-weave sacks for dispatch to the laboratory in Townsville • Each laboratory submitted sample weighed between 3kg to 5 kg • Samples were submitted to Intertek Laboratories in Townsville • Backup samples for each interval were also collected and retained on site until assays results have been returned **With respect to the historical drill holes:** • Sampling of percussion, RC and diamond core are by industry standard approaches with sampling generally on 1 m intervals, some of which were composited to 2 m samples intervals were unlikely to be mineralised. • Some percussion and RC drill holes samples were selected for assaying on the basis of browner material associated with sulphides mineralisation, avoiding sampling of waste areas. Given the narrow mineralisation zone and sulphide association this selective sampling approach is considered reasonable.
	• *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.*	
	• *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay').*	
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or*	**SVG RC Drilling (2025)** • The drilling was undertaken using a DR950 Reverse Circulation Rig from AED • The hole size was 5.5 inch and a face sampling hammer was used • Surveys were taken at the base of each hole

Criteria	JORC Code explanation	Commentary
	standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	**Red Dam - Historical holes** CRA Exploration (CRAE) 1987 – 1998 • Initially percussion and progressing to RC drilling the CRAE data is the largest drilling set • Sampling intervals of 1 m were composited to generally 2 m and occasionally 3 m intervals Georgetown Mining Limited GML (2005-6) • RC 4 5/8 and 5 inch face sampling hammer sampled on 1 m intervals with a UDR650 rig • Some diamond core drilling using triple tube PQ DRAU (2009 to 2012) • Reverse Circulation drilling (RC) were 140 mm in diameter sampled on 1 m intervals • Diamond Drilling tailing RC drilling was by triple tube HQ and used for deeper sulphide intersections, samples are submitted as half core 0.5 to 1 m intervals.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.*	**SVG RC Drilling (2025)** • The samples were collected using a face sampling hammer, the samples after going through the cyclone went through a splitter, with 12.5% of the sample collected in a numbered calcio bag, the balance of the sample was collected in a green plastic bag, which will remain on site prior to environmental rehabilitation procedures • The face sampling hammer provides an uncontaminated sample and the splitter ensures that there is no sample bias in the collection of the sample **Red Dam – Historical Drilling** • Open hole drilling with some potential for smearing was initially used but from the early 1990s' drilling progressed to RC drilling as drilling methods improved across the industry. • Diamond drilling was used to target deeper sulphide mineralisation and triple tubes were used in conjunction with short runs to try and maximise recovery.
	• *Measures taken to maximise sample recovery and ensure representative nature of the samples.*	• There is no sample bias and there is no known relationship between observed sample recovery and assay grade for the SVG drilling • No previous workers have indicated an obvious relationship between recovery and grade other than that the mineralisation zone is softer and more challenging to drill. No digital recovery data is currently recovered to assess any potential relationship.
	• *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred*	• There is no sample bias and there is no relationship between observed recovery and assay grade
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to*	**SVG RC Drilling (2025)** • Geological logs were completed for all drill holes by an experienced geologist at a level to support appropriate Mineral Resource estimation

Criteria	JORC Code explanation	Commentary
	support appropriate Mineral Resource estimation, mining studies and metallurgical studies. *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* *The total length and percentage of the relevant intersections logged.*	• The lithology, weathering, oxidation colour, grainsize, texture, alteration, vein material were recorded on a paper log sheet which was then transferred to a digital log sheet for inclusion in the company's database • Logging of mineralisation and veining in the RC chips was quantitative • Representative chips form each drill hole interval were placed in numbered chip trays and the chip trays were photographed • Each 1m interval was logged **Red Dam – Historical Drilling** • Logging for geology and alteration is available for most drill holes. • Recovery of diamond core was noted though not preserved in the digital database. • CRAE & GML Diamond core was quarter core sampled • DRAU (2009 –2012) Diamond core was halved and sampled
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.*	**SVG RC Drilling (2025)** • Diamond drilling by SVG at Red Dam is detailed in an announcement made to the ASX on the 18th December 2025 **Red Dam – Historical Drilling** • CRAE & GML Diamond core was quarter core sampled • DRAU (2009 –2012) Diamond core was halved and sampled
	• *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.*	**SVG RC Drilling (2025)** • The samples were drilled dry, • The samples were collected from a splitter which was attached to the cyclone on the drill rig • 12.5% of the sample split was retained for assay, with the remaining 87.5% of the collected in large green plastic bags **Red Dam – Historical Drilling** • CRAE percussion and RC drilling used 1m sample intervals but often composited to 2 m and at times 3 m intervals when in likely waste material. • GML (2006) percussion drilling split 2 kg from a three-tier on-board riffle splitter. Selective assays undertaken used a distinctive brown colour for the mineralisation. • DRAU (2009 –2012) RC subsampling at the drill rig with a riffle splitter to 5 kg subsamples.
	• *For all sample types, the nature, quality and appropriateness of the sample preparation technique.*	**SVG RC Drilling (2025)** • The SVG drill samples were a 12.5% split from a splitter attached to the cyclone, samples typically weighed between 3 to 4 kg and the sample that was sent to an accredited laboratory for analysis.

Criteria	JORC Code explanation	Commentary
		• The samples were despatched to Intertek Laboratories in Townsville, North Queensland. The samples were dried, crushed and pulverised as per industry standard practise. • The sample preparation technique is appropriate for the style of mineralisation being analysed • The samples were pulverised to -75 microns and analysed for gold by fire assay (FA50/OE) and also for multi elements using the 4A/MS methodology **Red Dam – Historical Drilling** • Sample preparation was by commercial laboratories that changed which each operating company. • Though not described sample preparation is assumed to have used industry standard practices of the day.
	• *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.*	**SVG RC Drilling (2025)** • One to three duplicate samples were submitted per RC hole and submitted to Intertek for analysis along with the original sample • A Blank and two standards were also submitted with each sample batch • Intertek also used their own standards and ran duplicate samples on SVG's submitted samples duplicates • No Duplicate samples were submitted for the core holes so no comparisons can be made, lab duplicates and standards returned results that fall within industry standards for the type and style of mineralisation reported **Red Dam – Historical Drilling** • Riffle split of RC samples should have produced acceptable presentation of the splits. • There is no record if processes were adopted for diamond core splitting to avoid bias. Given the broken ground structural bias between core halves is unlikely. There are no records of spear percussion sampling
	• *Whether sample sizes are appropriate to the grain size of the material being sampled.*	**SVG RC Drilling (2025)** • The RC laboratory submitted samples which are a 12.5% split of the entire samples and weighed between 3 to 4kgs, this is considered appropriate by the CP • The sample size is appropriate considering the grain size of the material, as well as the style of mineralisation being analysed. • Subsampling sizes are within industry practice and considered acceptable
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.*	**SVG RC Drilling (2025)** • The method employed to assay SVG's samples is industry standard and considered appropriate for the style of deposit and elements being assayed • Sample preparation and assaying was by Intertek in Townsville which is an ISO/IEC 17025 accredited laboratory • Samples were assayed for gold using the Au FA50/OE methodology and for multi-element analysis using the MS/4A method, these methodologies are industry standard • The method employed is industry standard and considered appropriate for the style of deposit and elements being assayed.

Criteria	JORC Code explanation	Commentary
		Red Dam – Historical Drilling • CRAE samples were prepared and assayed at Classic Laboratories (Analabs) in Townsville. Au assays were by fire assay and ASS finish and ICPMS for other geochemistry. • GML samples were prepared and assayed by SGS Townville using fire assay for Au (FAA505) and ICP (ICP21R) for Ag, As, Cu, Fe, Pb, Zn, Bi and Sb (also S for diamond core samples). ALS was used for check analyses with similar fire assay methods. • DRAU (2009 to 2012) used ALS in Townsville as the primary Laboratory and Genalysis for check sample work. Analysis was at ALS Townsville by Fire Assay (FA25) for Au and method AR01 for Ag, As, Cu, Fe, Pb and Zn
	• *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.*	• No geophysical tools were used.
	• *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established*	**SVG RC Drilling (2025)** • Standards and blanks submitted by the laboratory came, back within industry standards. **Red Dam – Historical Drilling** • At Red Dam GML repeated analyses from SGS at ALS randomly at about 1 in 20 samples with 24 samples. In additional some check sample duplicates were taken by spear sampling the RC field residue.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.*	• All assay data received including significant intercepts are reviewed by at least 2 appropriately qualified persons for validation purposes. All reported significant intercepts are verified by at least 2 appropriately qualified persons • At Red Dam initial discovery and resource definition channel and drill sampling by CRAE has been followed up with confirmation drilling by both GML and DRAU.
	• *The use of twinned holes.*	• No holes were twinned by the five RC holes
	• *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.*	• SVG has collated and created a digital database of all exploration completed at the project which contains all of the historical drill hole data

Criteria	JORC Code explanation	Commentary
	• *Discuss any adjustment to assay data.*	• No adjustment of assay data was considered necessary.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.*	**SVG RC Drilling (2025)** • All drill hole locations were surveyed using a hand held GPS with a +/- 5m accuracy. • The coordinate system used is Geocentric Datum of Australia (GDA202) Map Grid of Australia (MGA) zone 54 • A table of drill hole parameters is included as Table 1 in the document. • A drill hole location map has also been included as Figure 2 in the document **Red Dam – Historical Drilling** • CRAE drilling and costeans were laid out by tape and compass and surveyed post drilling by theodolite and EDM survey by Terrasearch Ltd using a local grid and tided into AMG coordinates and later converted to MGA coordinates. • GML drilling and surface topography (1:1000 airborne mapping) were surveyed by Ausnorth Consultants in 2006 when an MGA network was established along with resurvey of some historic drilling. Subsequent drilling by GML was surveyed by differential GPS. • DRAU drilling was surveyed by Ausnorth Consultants • Surface topography for all deposits with mining were surveyed by Ausnorth Consultants pre and post mining. • There is no description of down hole surveys for all drilling phases. • At **Red Dam** the majority of holes are orientated at or near 60˚ and were presumably setup or measured at collar from the drill rig. Some deeper diamond holes have small variations of survey from 40 to 80 m at around 30 m intervals, suggesting single shot camera surveys.
	• *Specification of the grid system used.*	• All data has been converted to MGA 94 (Zone 54). Elevation values are in AHD RL • All historical data has been converted to MGA 94 (Zone 54). Elevation values are in AHD RL. All data has been converted to MGA 94 (Zone 54). Elevation values are in AHD RL
	• *Quality and adequacy of topographic control.*	• The Quality of the topographic control data is reliant on public domain topographic data. • GPS readings with a +-5m accuracy were used to survey in the drill holes
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.*	**SVG – Exploration drill hole spacing** • Due to the exploratory nature of the drilling, spacing varied between 40m to 120m between holes (see drill hole map included as Figure 2 in the document) . **Red Dam – Drill hole spacing** • Resource definition drilling sections spaced at

Criteria	JORC Code explanation	Commentary
		• 10 m at Red Dam to a depth of 30 m below surface and 30 m in deeper areas
	• *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.*	• An Inferred resource has been reported for Red Dam, the details of which are included in the report. These results may be utilised to update this resource in 2026 • The drilling is of sufficient density and the geology has the appropriate continuity to be used to upgrade the Resource estimate • Drill hole spacing will support a higher classification than Inferred Mineral Resource.
	• *Whether sample compositing has been applied.*	• No sample compositing has been carried out.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.*	• Where possible the drill holes were orientated to intersect the mineralised target perpendicular to strike • The holes were designed to intersect the mineralisation perpendicular to strike and at 90 degrees to the dip to obtain true intercept thicknesses
	• *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Drilling orientations are considered appropriate to the mineralisation type with no bias observed as a result of the drill orientation. • At this stage no sampling bias is considered to have been introduced in the sampling undertaken to date • At Red Dam most drilling is at 60˚ north or south into a near vertical east-west mineralised structure.
Sample security	• *The measures taken to ensure sample security.*	• The chain of custody is managed by the project geologist who generally dispatches the sample bags directly from site to the lab by an authorised company representative • No third party was involved with the handling of the samples, with a company representative delivering the samples to the Townsville Laboratory • The chain of custody by the three previous exploration companies that completed drilling is not documented and largely completed where sample security was not an industry consideration
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• SVG's Exploration manager visited the project site during the he drilling programme and reviewed sampling methodologies and data capture with the project geologists overseeing the drilling programme. • In 2008 L Davis of Veronica Webster Pty Ltd prepared a due diligence report for Deutsche Rohstoff AG for Georgetown projects including the Red Dam, Electric Light deposits and resources

Section 2: Reporting Exploration Results

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.*	• The Red Dam Prospect lies within ML 30203 and EPM 9158 – Mt Campbell. This EPM and ML are part of the 17 EPMs, 17 MLs and 1 MDL which comprise Savannah Goldfield's Etheridge Project • The EPM and ML are held by Kempton Minerals Pty Ltd, a 100% owned subsidiary of Savannah Goldfields Ltd • The tenements are in good standing • For all the tenements which comprise the Etheridge Project refer to the tenement table in the company's Annual Report dated 20 December 2024 • The tenements are overlapped by the Ewamian People #3 (QUD6018/2001) native title determination. Negotiations with Ewamian People who are the determined Native Title claimant are well underway and are not expected to impact future development and production. Savannah has a current Native Title Compensation Agreement and a CHMA with the determined Native Title group for all activities within EPM 9158 and ML 30203 • CCA's have recently been finalised and executed with the relevant landholders
	• *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The tenements are 100% owned by a subsidiary of SVG, and there are no impediments to operating in this area
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties*	• Precursor work was undertaken by the BMR • The majority of the drilling and resource definition work was undertaken by CRA Exploration (1987 – 1998) and included soil sampling, ground magnetics, IP and Genie EM surveys, costeaning and drilling (percussion, RC and diamond). • Triumph Resources NL (1998-2004) followed by Georgetown Mining Limited (GML) undertook reinterpretation, resource and mining studies between 1998 and 2008. • GML completed a second phase of drilling in 2005-6 along with supporting air and ground survey work and further geophysical and soil sampling programmes. • Red Dam was mined by DRAU in 2010-2011 and work since this time has focussed on the extensions along strike and down dip at Red Dam • Work has comprised further drilling sampling and geophysical surveys. • Plentex (2007 – 2008) undertook data review and mining and resource studies. • Deutsche Rohstoff Australia Pty Ltd (DRAU) completed: ➢ At Red Dam additional trenching in 2009 on 25 m spacing,

Criteria	JORC Code explanation	Commentary
		➢ RC drilling with some diamond HQ tails testing deeper areas and mining and resource studies. ➢ Mining occurred between 2010 and 2011 of both oxide resources. ➢ Completed a small costean program
Geology	• *Deposit type, geological setting and style of mineralisation.*	• The deposit is located within the northern part of the Georgetown inlier, which is made up of crystalline basement or early to middle Proterozoic rocks. • The deposit occurs within the Etheridge Goldfield which contains numerous mesothermal veins and lenses of gold and sulphide mineralisation typical of Siluro-Devonian age. • Red Dam is a high-grade gold deposit, characterized by a narrow, sub-vertical structure running east-west over a 1,600m extent. It is divided into three distinct segments and has a higher sulphide content and elevated density. • The mineralised shear at Red Dam strikes East West and dips steeply to the South at between 80 to 90 degrees • The sulphide mineralisation which is associated with the gold mineralisation predominantly comprises galena – arsenopyrite and sphalerite and is contained within a narrow (between 1.3 to 2.0m) wide shear zone
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.*	• All the drill hole information is listed in the GDA Z54 format • The data is included in the document in Table 1 and Appendix 2 • Historical drill hole locations and gold and silver assay results are included in Appendix 4 and the drill hole locations presented in Figure 2 within the body of the release
	• *If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.*	

Criteria	JORC Code explanation	Commentary
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• No capping of high grades was performed. No aggregation of data was performed. • No metal equivalents are reported • The intercepts reported were calculated using a 1.0 g/t Au COG, no internal dilution was used on the SVG holes drilled in 2025, however a maximum of 1m of internal dilution, (1m interval <1.0g/t Au) was used to calculate the historical intercepts but only on rare occasions.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.*	• The apparent thickness of each intercept has been reported • The holes drilled were at -60 degrees, the mineralised zone was mapped as predominantly dipping at -80 to -90 and the holes would have intersected the mineralised zone perpendicular to strike • Each hole was sited on the hanging wall side of the mineralised shear • The historical holes were predominantly drilled at either -60 or -70 degrees • The mineralisation is generally near vertical and thin. Drilling is generally undertaken perpendicular to the view strike. The majority of the drilling is angled -70 or at -60º and hence although at some angle the drilling orientation is generally as optimal as is practicable. • Shallow vertical holes were drilled by the earlier explorers
	• *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• Estimates of the apparent thickness and actual thicknesses have been reported
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• A plan of the drill hole locations and a table listing the coordinates of the drill holes, their depths, dip and azimuth is included in the document, (Figure 2 Table 2 and historical hole parameters and assay results are included in Appendix 4)
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• Balance reporting of Exploration Results has been presented in this document

Criteria	JORC Code explanation	Commentary
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• The project includes drill hole data collected by previous companies including surface geochemical data and drill hole data. Most of this data has been captured by SVG in their GIS database • There is no additional exploration data that is considered to be material to this report • Oxide mining by DRAU (2010 to 2011) included the processing of Red Dam oxide material. DRAU mined 23 kt @ 13.6 g/t Au of ore and approximately 471 kt of waste. • Little oxide remains, with the resource being comprised of mostly sulphide mineralisation. • The resource is within the existing mining lease with related environmental, rehabilitation, water and operational reports.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	• Planned further work will include possible additional drilling to test for down dip extensions to the Red Dam mineralised shear zone. • The mineral resource estimate will be updated based on the new assay information • Metallurgical testwork
	• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	• Additional drilling will be planned once an updated resource has been estimated and this will be announced to the market prior to the recommencement of any drilling